

# APPLICABILITY OF COBRA CONCEPT TO DETUMBLING SPACE DEBRIS OBJECTS

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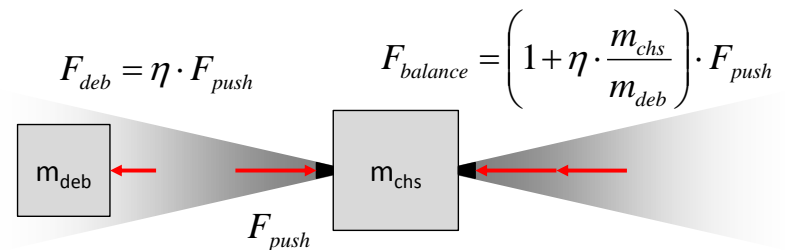
DIEGO ESCORIAL OLMOS, GMV

# INTRODUCTION

- COBRA overview
- COBRA context
- Plume modeling
- Despinning control strategies
- Envisat & PROBA 2 test cases
- Simulation

# COBRA OVERVIEW

- Momentum exchange between chaser and target through plume impingement
  - Chaser fires thruster in direction of target
  - (Part of) plume intercepted by target
  - Plume pressure generates force and torque on target
- COBRA initially developed for orbit modification
  - Found to be expensive in terms of  $\Delta V$ , **but:**
  - Rotation state modification feasible and fairly cheap
- COBRA concept requires no additional payload apart from what is already present for performing rendezvous
  - At least one thruster needs to point in the direction of the relative sensors



# COBRA CONTEXT: DEBRIS REMOVAL

- Removal options
  - Removal of tiny & small debris not practical
  - Removal of large objects removes potential sources of fragments in case of collision
- Conclusion: remove large objects
- Recent interest in removing Envisat in particular
- Trial mission could focus on smaller target, such as PROBA2

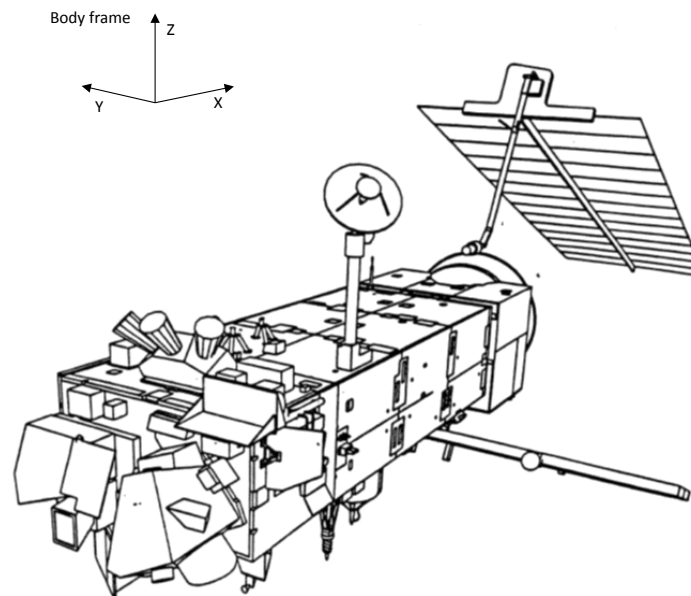
Type	Characteristics	Hazard
Tiny	Not tracked, <1 cm	Shielding exists, damage to satellites may occur
Small	Not tracked, diameter 1 – 10 cm, 98% of lethal objects, ~400.000 objects in LEO	Too small to track and avoid, too heavy to shield against
Medium	Tracked, diameter >10 cm, <2 kg, 2% of lethal objects, ~24.000 objects in LEO, > 99% of mass (incl. large objects)	Avoidance manoeuvres performed most often for this category
Large	Tracked, >2 kg, <1% of lethal objects, > 99% of mass (incl. medium objects)	Primary source of new small debris, 99% of collision area and mass

# ENVISAT

- An ADR mission is being studied to de-orbit Envisat
  - Robotic arm concept requires risky and expensive ( $\Delta V$ ) synchronization manoeuvre
- Detumble Envisat using plume impingement
  - Reduce risk of collision by easing / removing need for attitude synchronization
  - Synchronization  $\Delta V \sim 20$  m/s
  - S.K.  $\Delta V \sim 2.2$  m/s/min

## Envisat rotation state

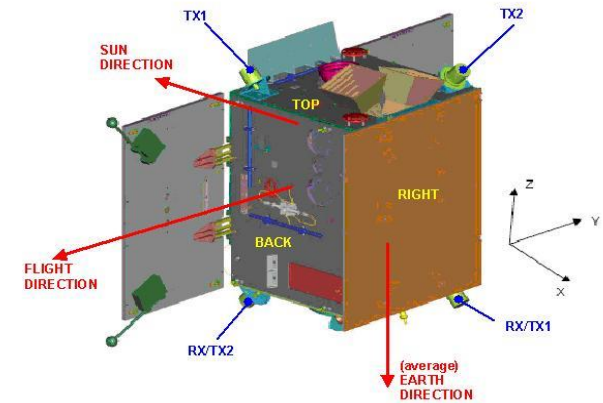
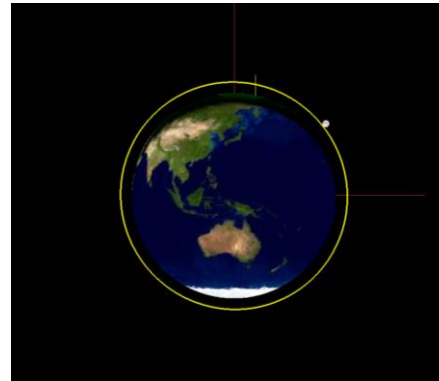
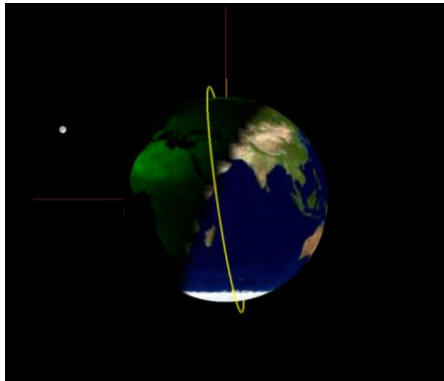
- Spin rate of  $3.5$  °/s, around body z-axis
  - Possibly around y-axis or intermediate axis
- Spin rate of  $5$  °/s around y-axis assumed for simulation



# PROBA2

## ■ Mission characteristics, PROBA 2:

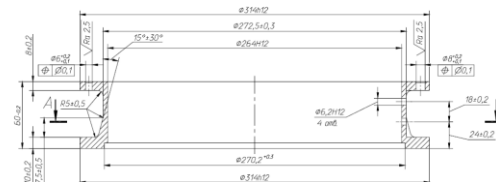
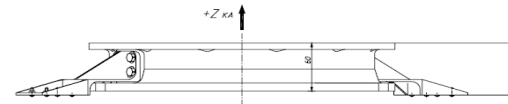
- Orbit: SSO, 718 km, inclination 98.285°, eccentricity 0.0013
- LTAN: 6:24 AM
- Payload: Optical (main) + 17 technological demonstrators
- Launch: 02.11.2009 (auxiliary to SMOS)
- Launcher: Rocket



## ■ Physical characteristics

- Mass: 124.8 kg

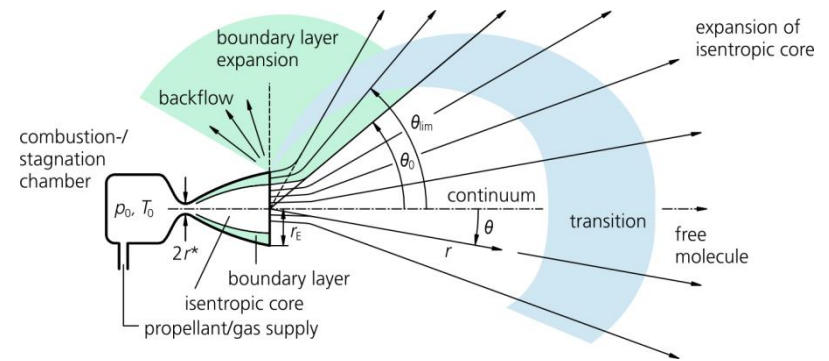
COG (mm)	X	Y	Z
	-16.1	-5.8	381.4
MOI (kg m <sup>2</sup> )	X	Y	Z
X	13.42	0.27	-0.29
Y	0.27	11.60	-0.52
Z	-0.29	-0.52	10.06



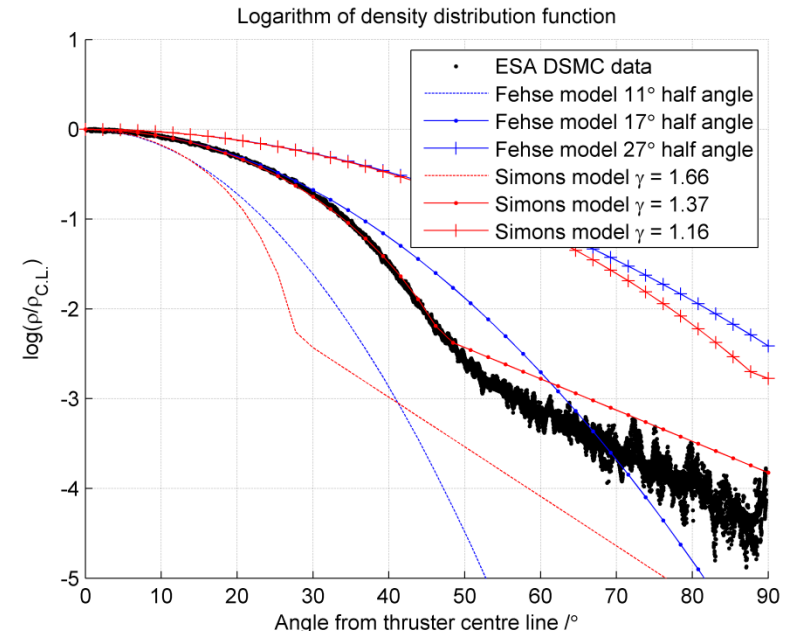
- Deployed dimensions: 0.590x1.603x0.790 m

# PLUME MODELING

- Plume model based on work by G. A. Simons
  - High-power cosine law in isentropic core
  - Exponential decay in boundary layer
  - Analytical & fast model
- Verification and parameter settings
  - ESA DSMC data available for 1 N thruster
  - Analysis of experimental data in literature ongoing
- Interaction with target assumed to occur in free molecular flow regime
  - Transition is estimated to occur (Flow “freezes”) at about 0.3 m to about 2 m

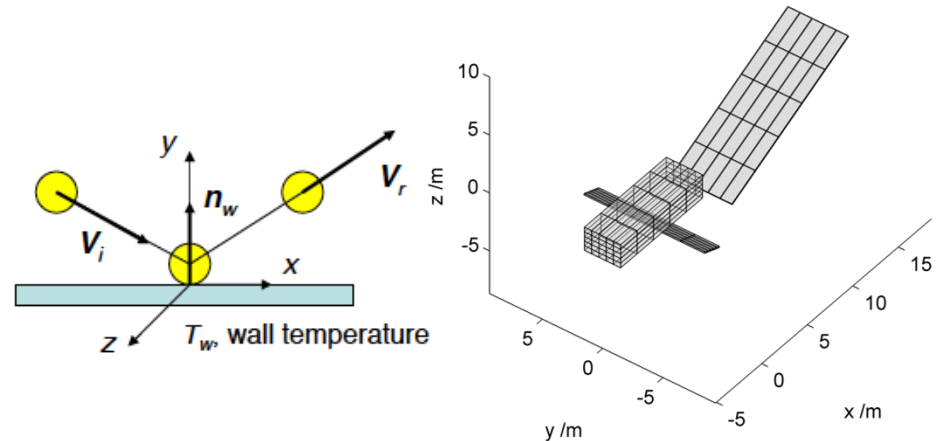


From: Dettleff, Georg and Grabe, Martin (2011) Basics of Plume Impingement Analysis for Small Chemical and Cold Gas Thrusters. In: RTO Educational Notes Models and Computational Methods for Rarefied Flows. RTO/NATO. pp. 1-40. ISBN 978-92-837-0129-3



# SURFACE INTERACTION

- Simplifying assumptions made for speeding up calculations
  - Few special functions to limit number of function evaluations
  - Coarse, low detail model of target
- Assumptions
  - Simplify Schaaf & Chambré model
    - Collisions of gas molecules assumed Maxwellian
  - Thermal motion negligible compared to flow velocity (hypersonic flow) (in reality up to 20%)
  - Zero wall temperature (in reality flow velocity up to 20% of incoming flow velocity)

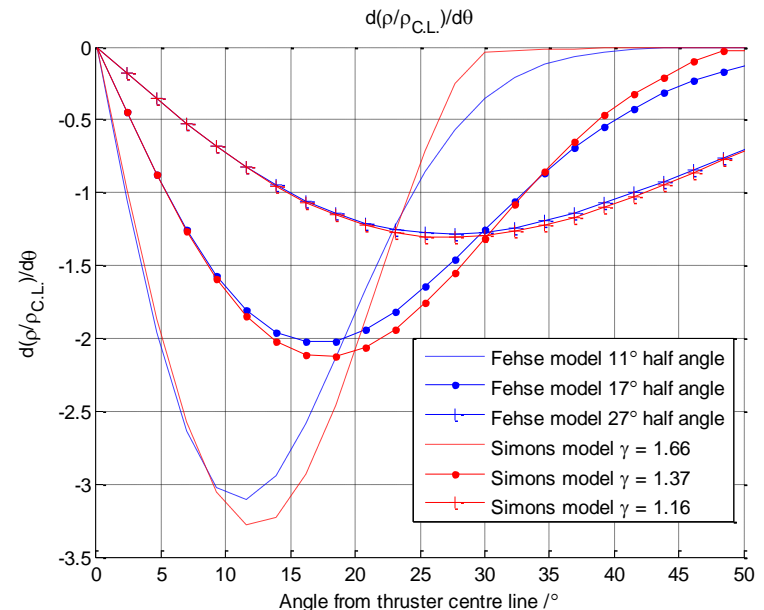
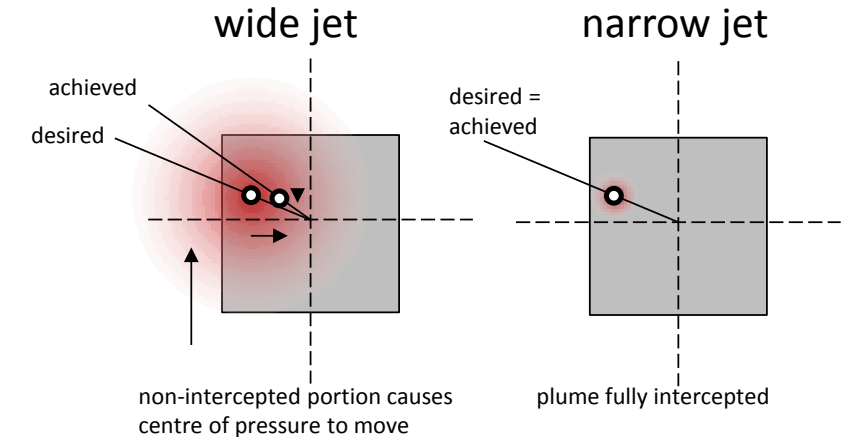


- Simplifying assumptions reduce fidelity but reduce computation time
  - Full model should be used to check results
  - Still, force components will be present in the direction of panel normal and direction of incoming flow



# EFFECT OF PLUME OPENING ANGLE ON CONTROLLABILITY

- Narrower plume desirable
  - Larger operating distance possible (larger portion of jet intercepted)
  - Torque depends on
    - Dynamic pressure variation (depending on  $d\rho/d\theta$ ) so the narrower the plume, the higher the torque
    - Part of plume intercepted
  - Narrow plume behaves more like force application at single point instead of over an area
    - Less “unexpected” behaviour if a single force application point is used in control model



# CONTROL STRATEGY

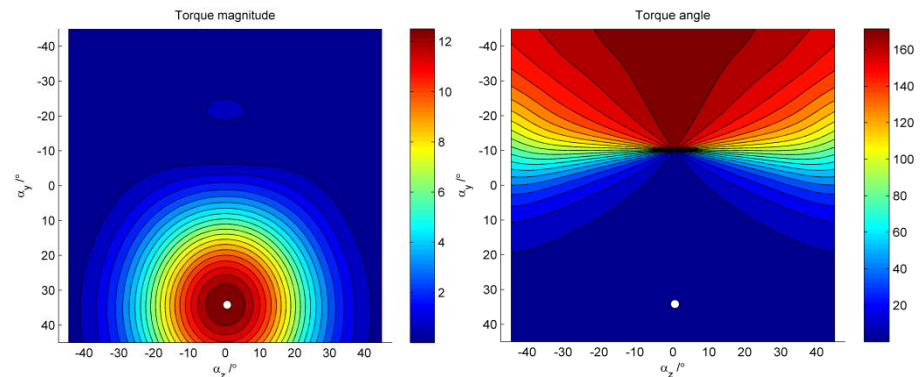
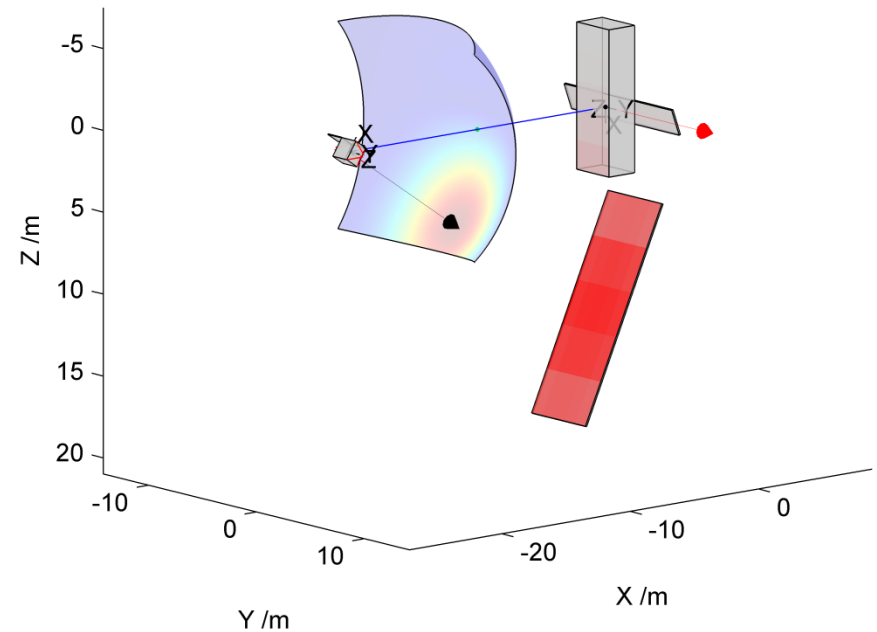
## ■ Two effects

- Target object asymmetry
  - chaser imparts torque on target even if gas jet is directed at centre of mass
- Gas jet pointing away from centre of mass
  - pressure distribution is non-symmetrical with respect to centre of mass (even if target is symmetric)

## ■ Envisat panel causes large asymmetry

## ■ Control strategy

- Based on pointing and switching
- Can control two axes at a time



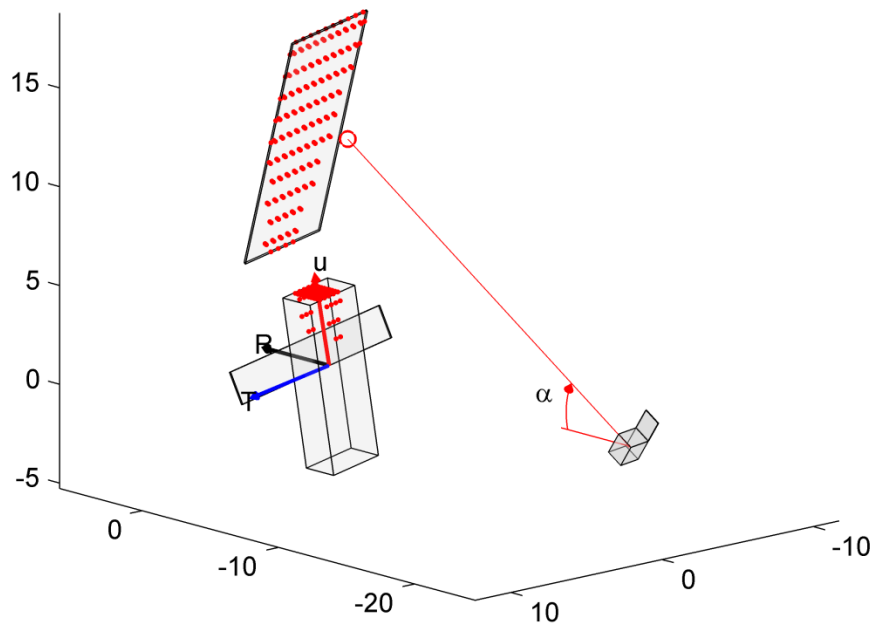
# CONTROL STRATEGY 1

## Direction calculation

- Step 1: desired torque on target is computed based on target angular momentum
- Step 2: direction  $u$  of force application is calculated
  - Perpendicular to torque and direction to target
- Step 3: off-centre angle  $\alpha$  is calculated based on target shape
  - i.e., a sufficiently large portion of plume must be intercepted

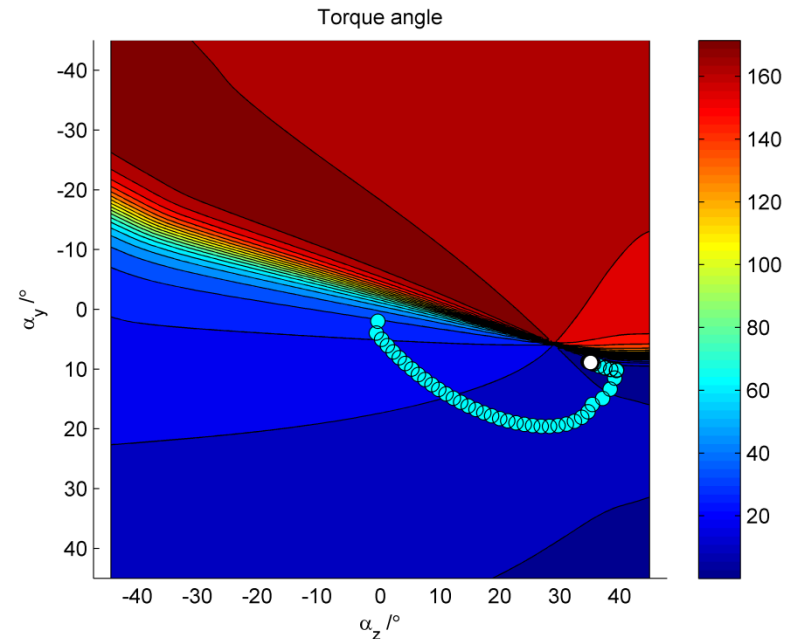
## Switching calculation

- Check whether desired torque is close to perpendicular to direction to target (threshold)

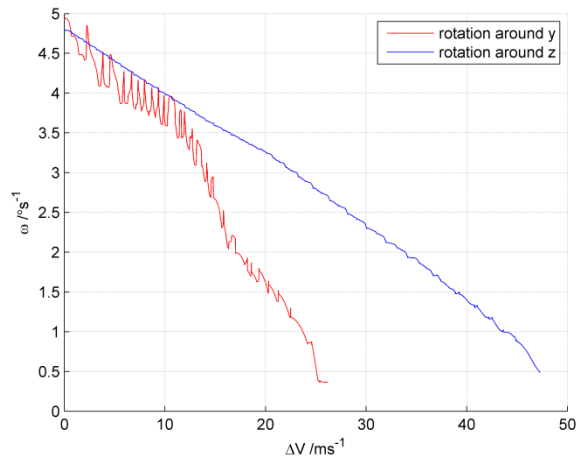


# CONTROL STRATEGY 2

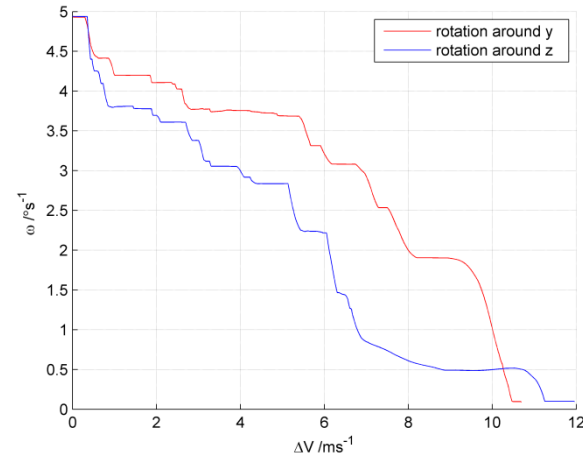
- Find maximum torque for correct torque direction
- Simplified plume impingement model
- Calculate torque and derivatives for current direction
  - Torque angle + magnitude + first & second derivative
  - 7 evaluations of plume impingement model
- If torque angle is not correct, step towards correct angle
- If torque angle is correct, step towards maximum
- One step allowed per simulation time step



# SIMULATION RESULTS

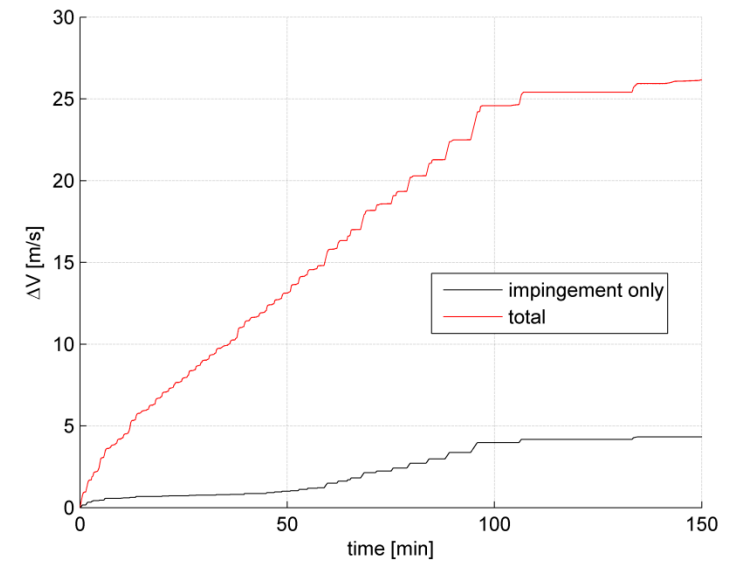
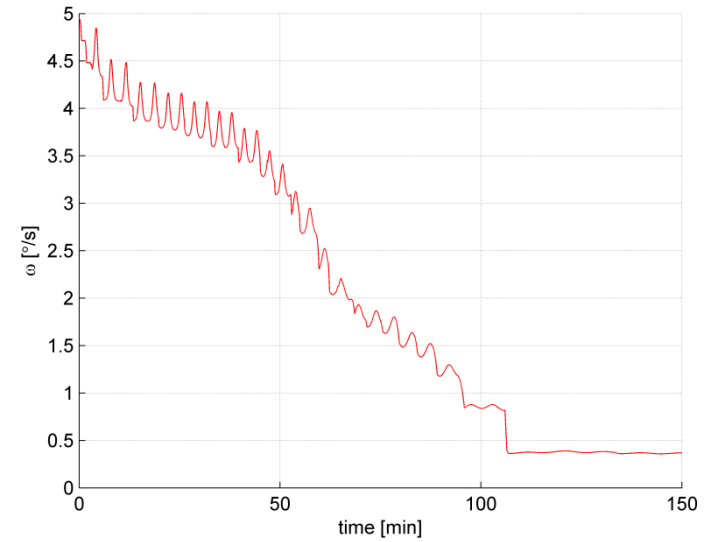
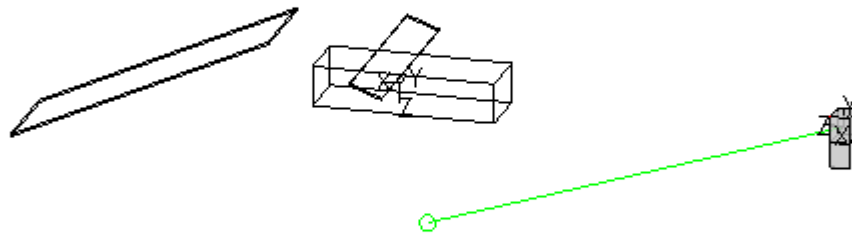


- Envisat detumbling using strategy 1
  - Distance 23 m, 5N thruster
- Duration 100 – 150 minutes
- $\Delta V$  25 – 48 m/s depending on rotation conditions



- PROBA2 detumbling using strategy 2
  - Distance 6 m, 1N thruster
- Duration about 20 minutes
- $\Delta V$  10– 13 m/s depending on rotation conditions

# COBRA DETUMBLING



# CONCLUSION

- COBRA de-tumbling satellites is promising technique for de-tumbling space debris objects.
  - No additional equipment on chaser apart from equipment already there for performing rendezvous with the object
- Improved models
  - Improved plume model
  - more realistic (albeit highly simplified) model of surface interaction of plume exhaust gases with surface of target object
- Simulations have shown that de-tumbling by means of plume impingements is possible
  - Even if target object is in unfavourable rotation state
  - Even for satellites that do not have pronounced asymmetrical shape



# Thank you

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