

# Design and Performance Analyses of the DLR Robotic Manipulator Arm for the e.deorbit Mission

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Knowledge for Tomorrow

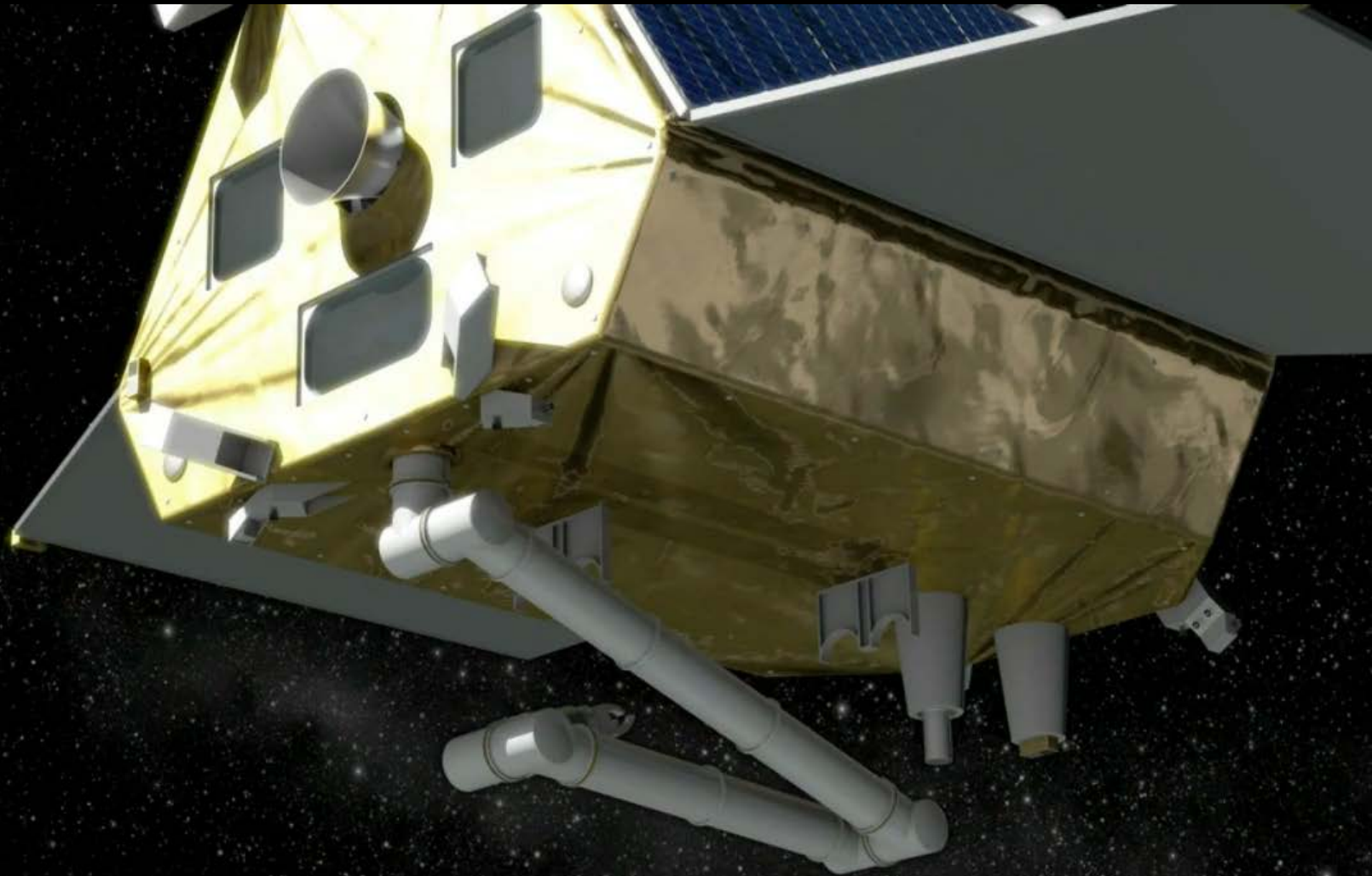




Note: Artist's impression; size of debris exaggerated as compared to the Earth

Source: ESA







Source: Youtube (edited)



# Challenges of Robotic Spacecraft for OOS and ADR

- In general: complex free-floating contact operations in **close-proximity**
- **Unintended contact** can lead to unsuccessful capture: upon contact capture needs to be assured
- **uncertain environment** (target not prepared for servicing)
- Free-floating dynamics: manipulator has **direct physical feedback** on its floating base: GNC stabilization



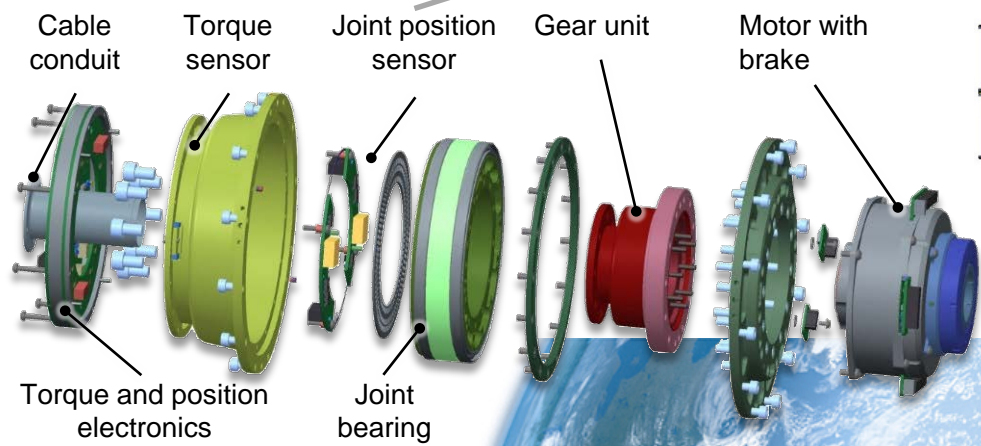
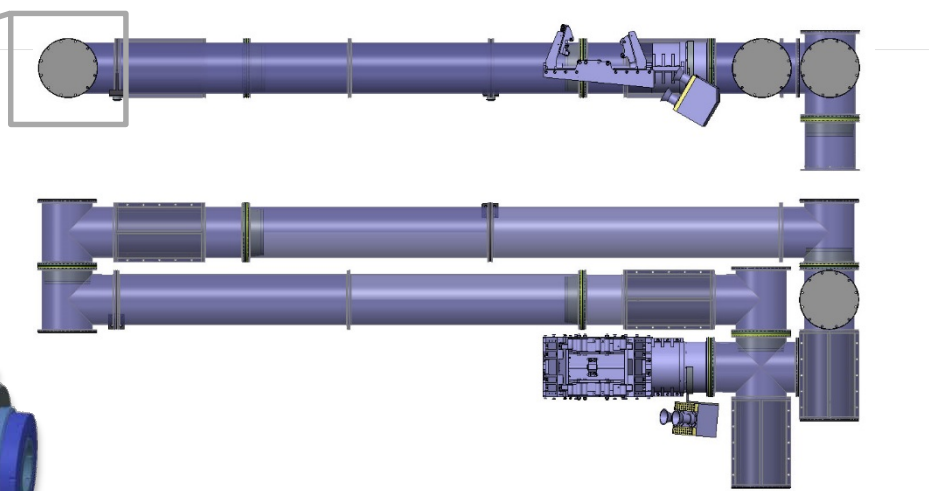
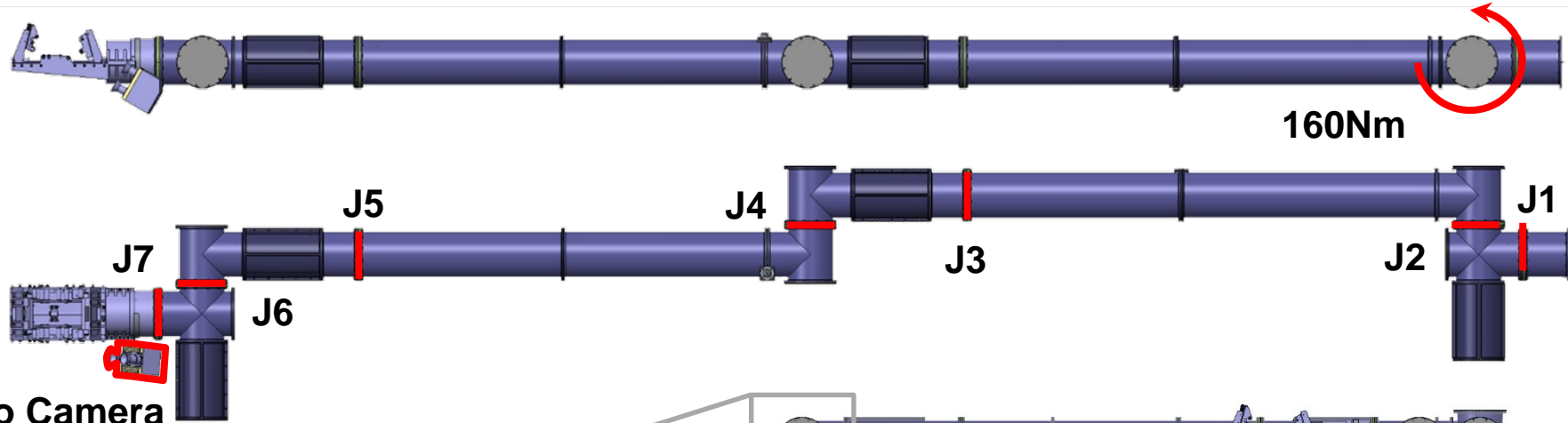
# e.deorbit - Phase B1 Baseline Capture Concept





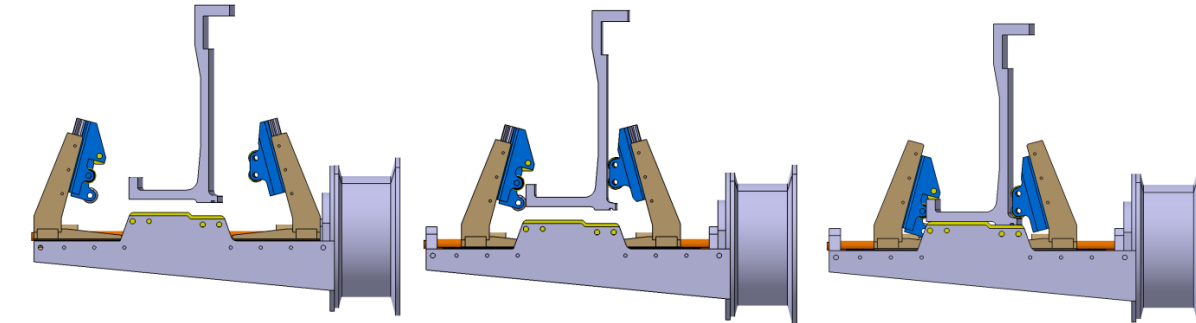
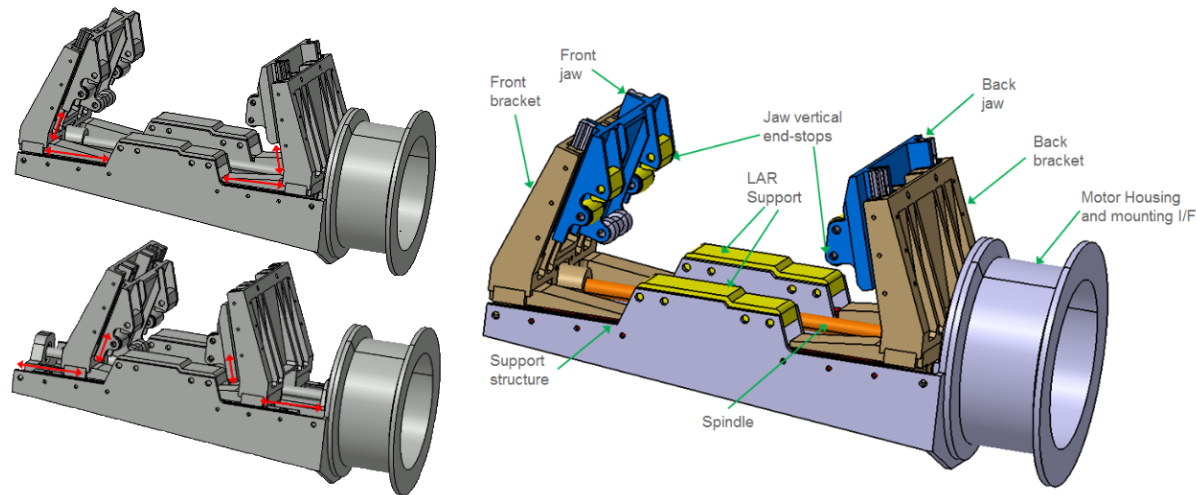
# Arm Technology

4.3m



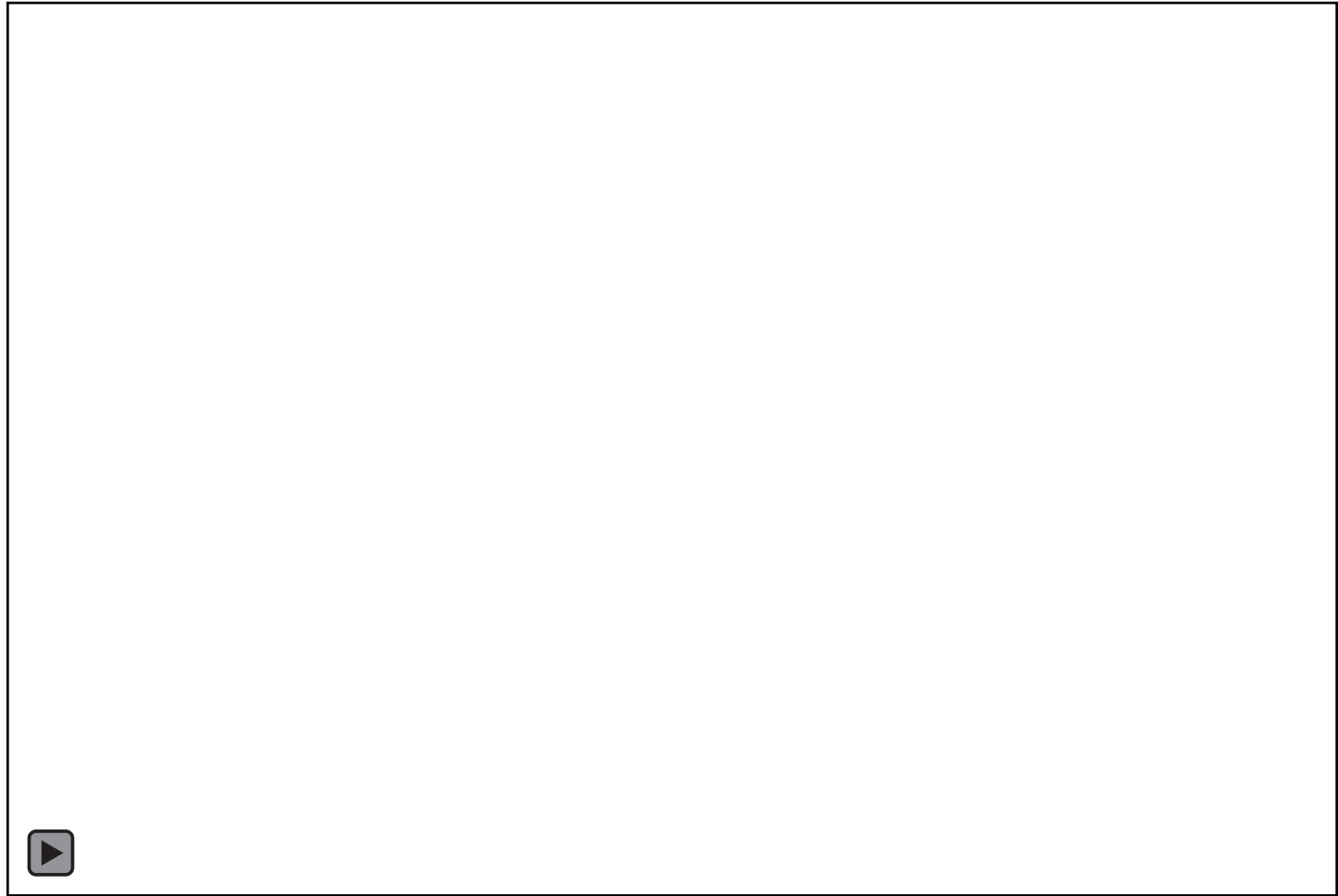
# Gripper (OHB)

- Two spindle-driven brackets
- Movable, spring-driven, inclined grip jaws on each side
- Contact points only on dedicated rolls
- Inclined, movable brackets: horizontal force increases vertical force
- Full form closure with Ariane launch adapter ring



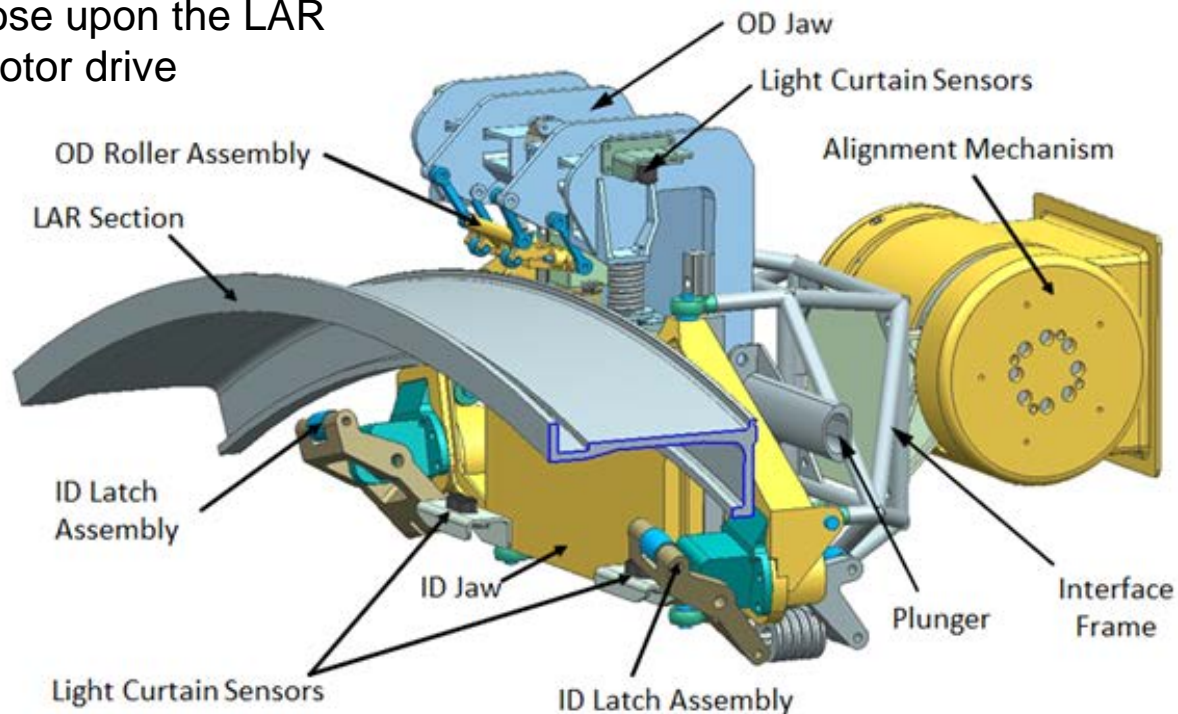


# Gripper (OHB): Grasping Process



## Clamp (MDA)

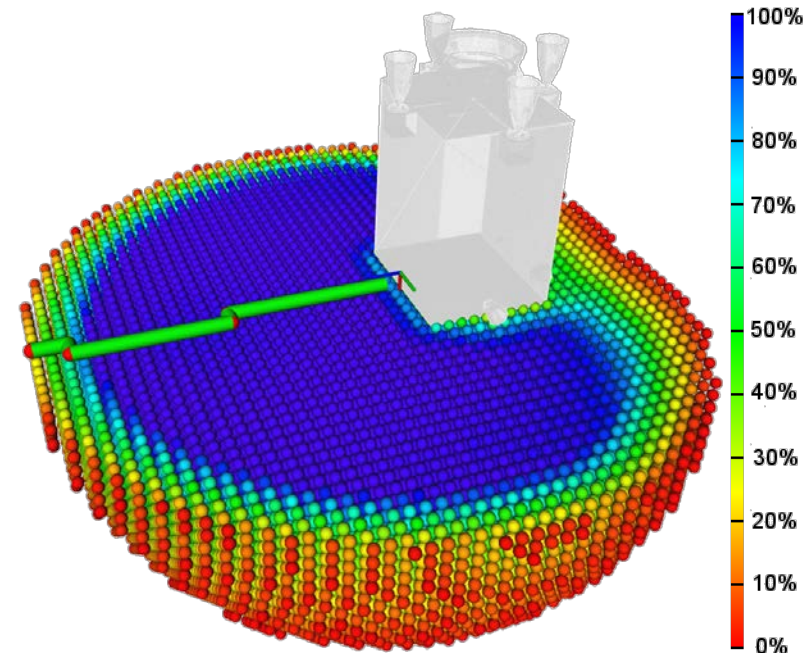
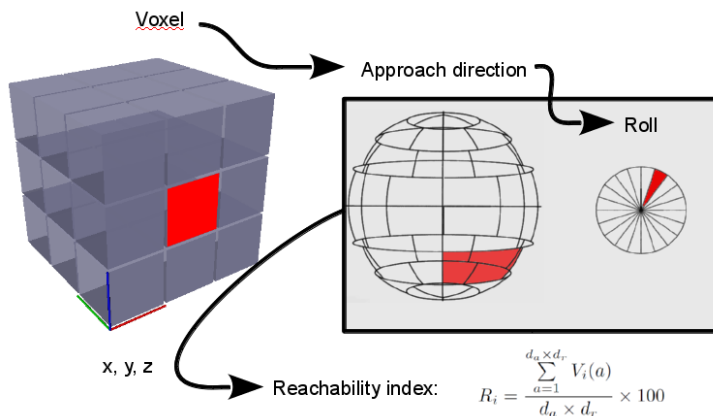
- Achieve stiff force closure between spacecraft
- Alignment mechanism for adjusting de-orbit thrust
- Light curtain to determine LAR in capture envelope
- Spring-loaded latch close upon the LAR
- Jaws fully closed by motor drive





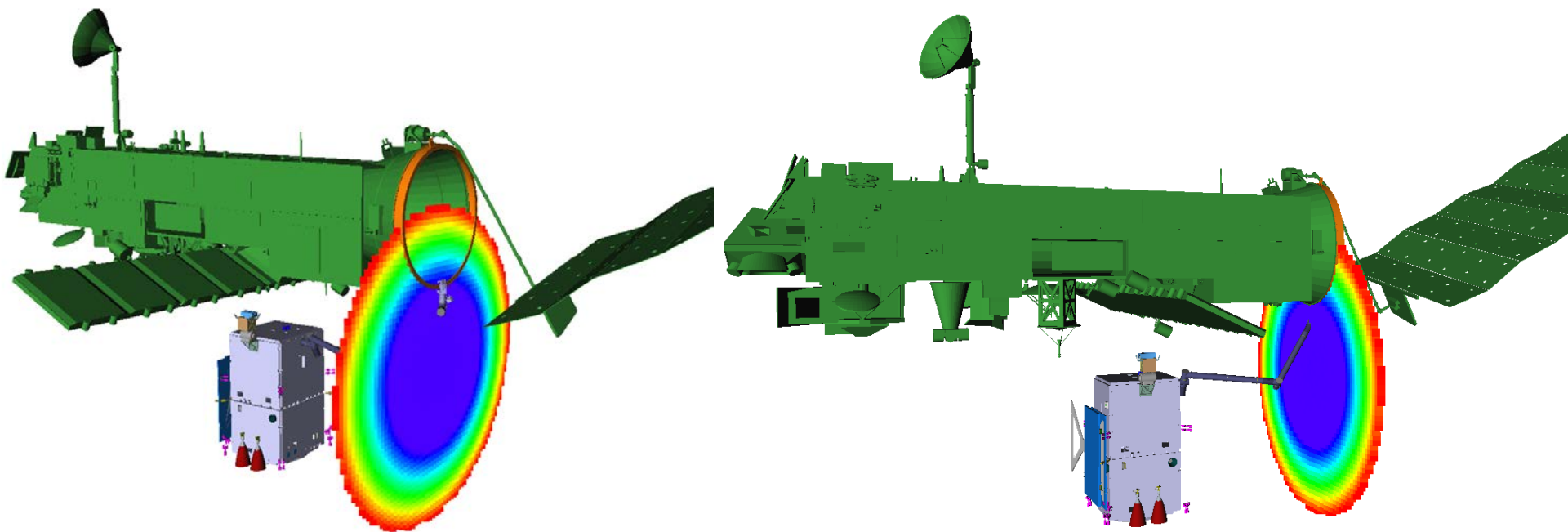
# Workspace Analysis

- Capability map – quantification of possible discretized directions in subspace
- Euclidean space is discretized into voxels and orientations (RPY)
- Color intensity identifies feasible end-effector poses
- Direct insight into workspace of the robot
- Used for validation of kinematics
- Accounts for self-collision



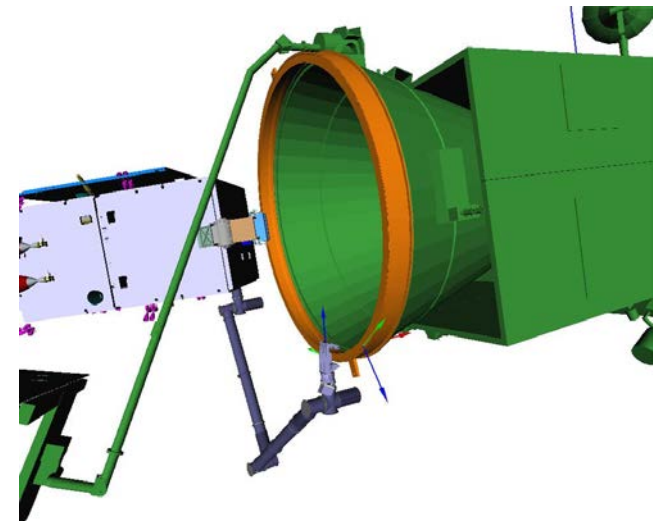
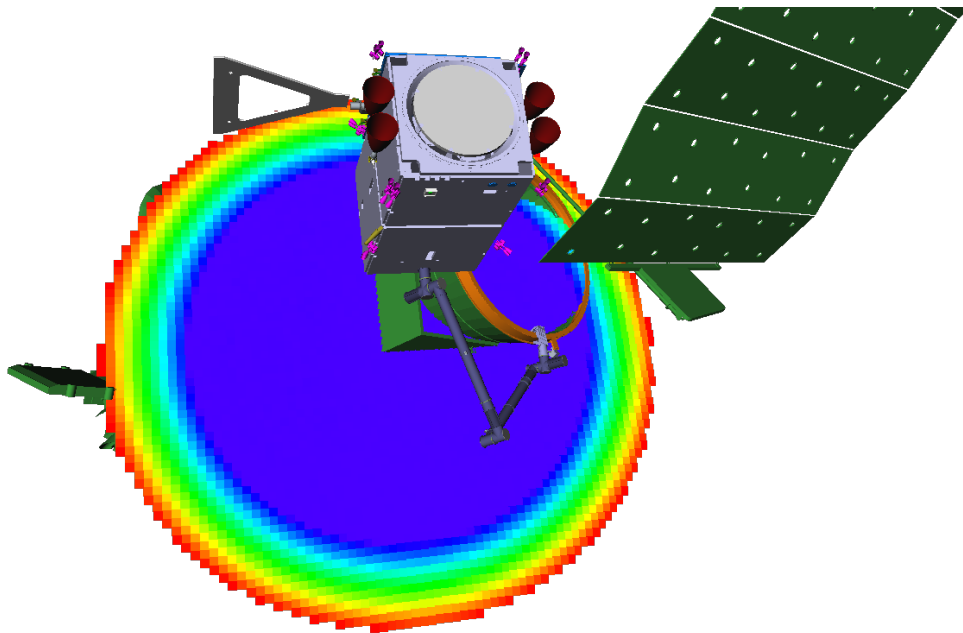
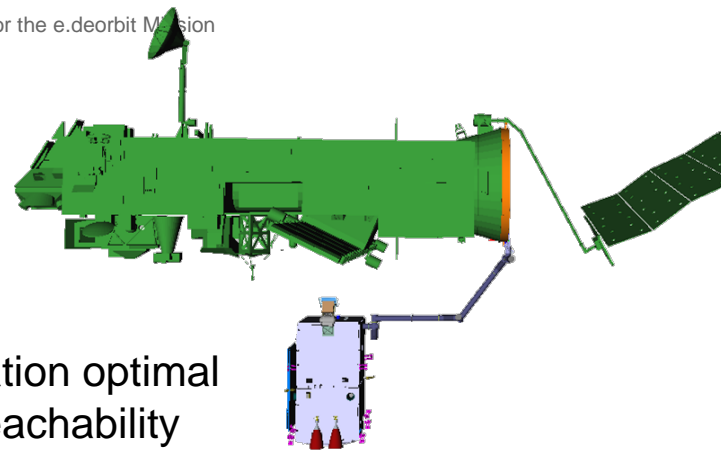
# Workspace Analysis: Capture

- Capture configuration at arm delivery point (satellites CoG's are aligned)
- Good reachability robustness in case of unexpected drift



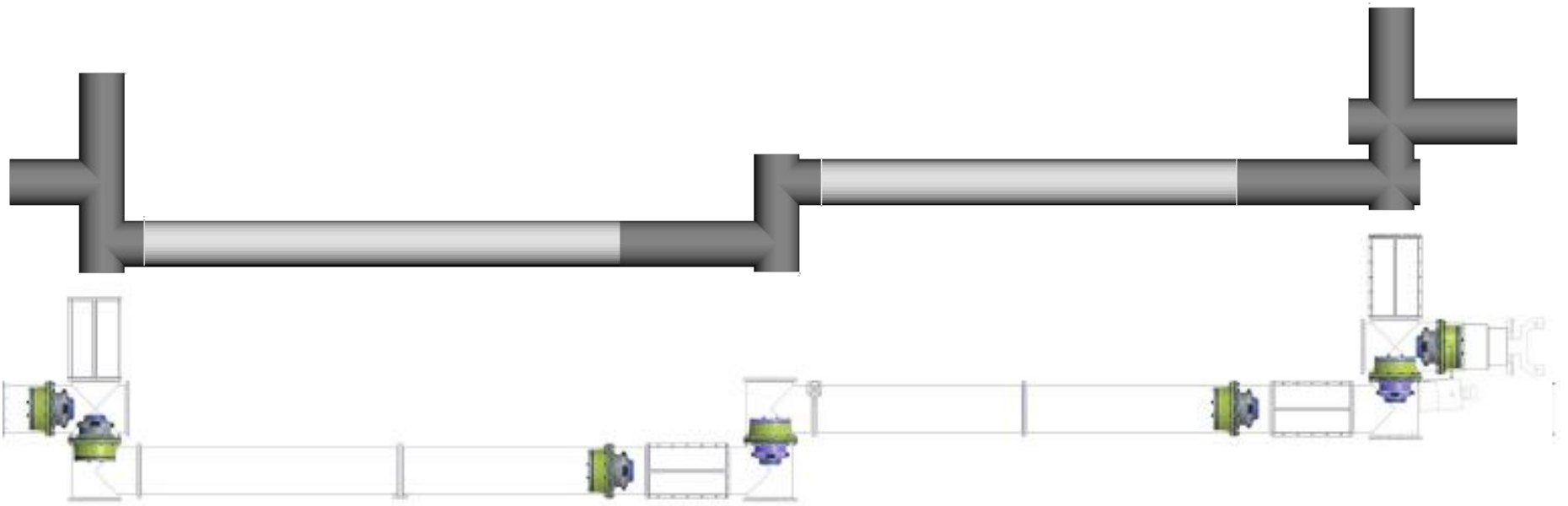
# Workspace Analysis: Clamping

- Clamping position analysis: 90deg clamp configuration optimal considering possible grasp point, safe trajectory, reachability
- Some distance required between grasp point and clamp point due to reachability and to allow better elbow placement (pointing away from potential collisions)



# Arm Flexibility

- Multi-body simulation in Simulink/SpaceDyn and SIMPACK with free-floating target, chaser and attached manipulator
- Dynamic modes and frequencies of manipulator assembly and stack
- Impacts of arm structural flexibility on accuracy and control approach





# Arm Flexibility: Grasped 1<sup>st</sup> Mode



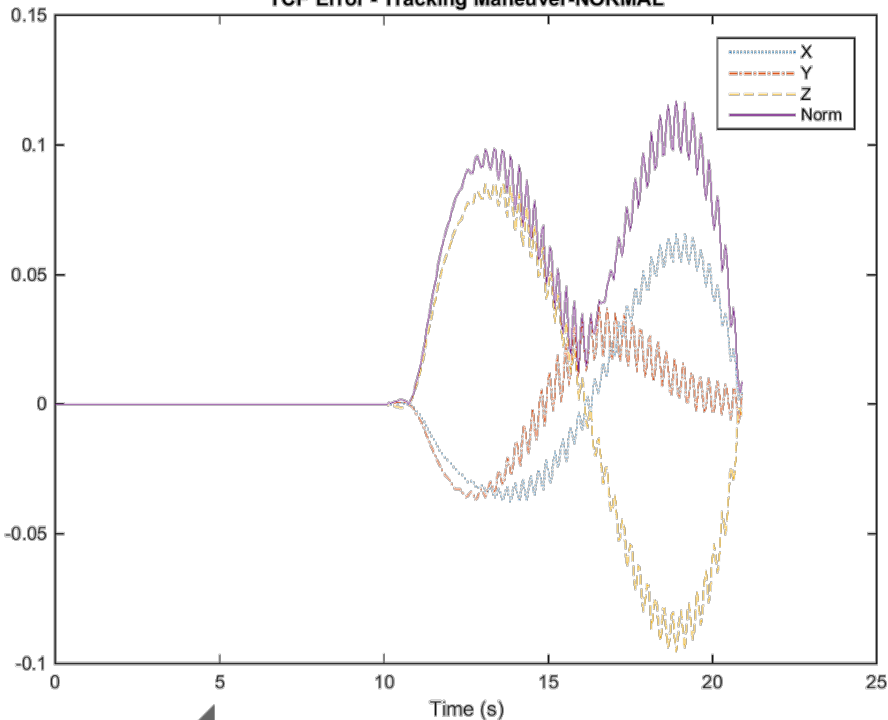
# Arm Flexibility: Docking 1<sup>st</sup> Mode



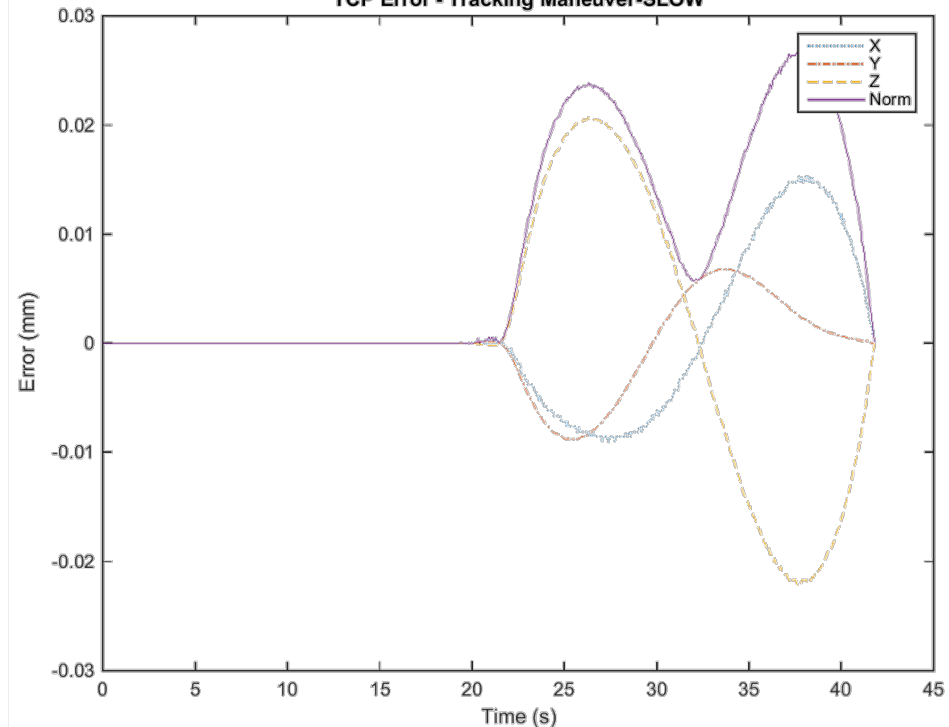
# Arm Flexibility: Induced TCP Error for Capture

- Arm capture maneuver, speed normal (up to 6deg/s, 10s maneuver time) and slow (up to 3 deg/s, 20s maneuver time)
- Resulting error: 0.1mm (normal) and 0,02mm (slow)

TCP Error - Tracking Maneuver-NORMAL



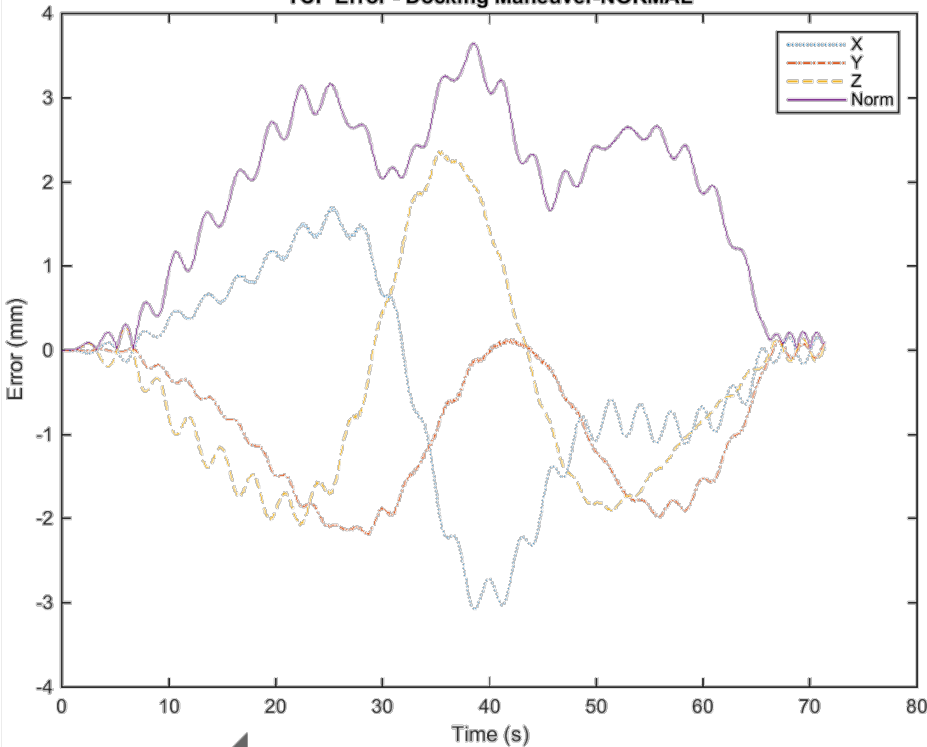
TCP Error - Tracking Maneuver-SLOW



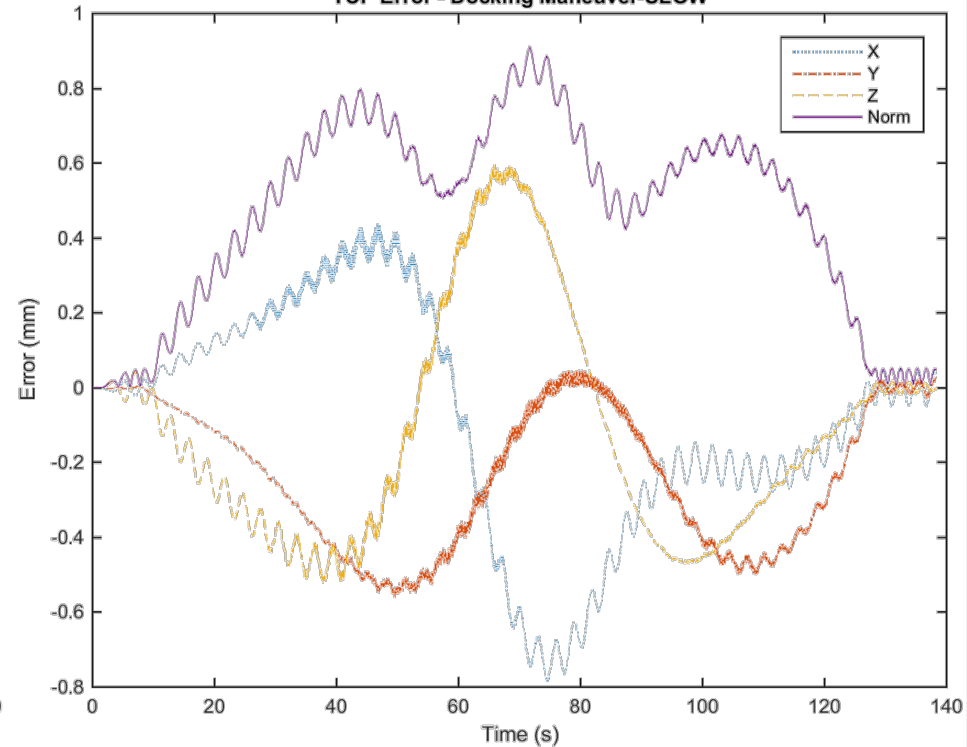
# Arm Flexibility: Induced TCP Error for Docking

- Docking maneuver, speed normal (up to 5deg/s, 50s maneuver time) and slow (up to 2.5 deg/s, 100s maneuver time)
- Resulting error: 3.5mm (normal) and 1mm (slow)

TCP Error - Docking Maneuver-NORMAL



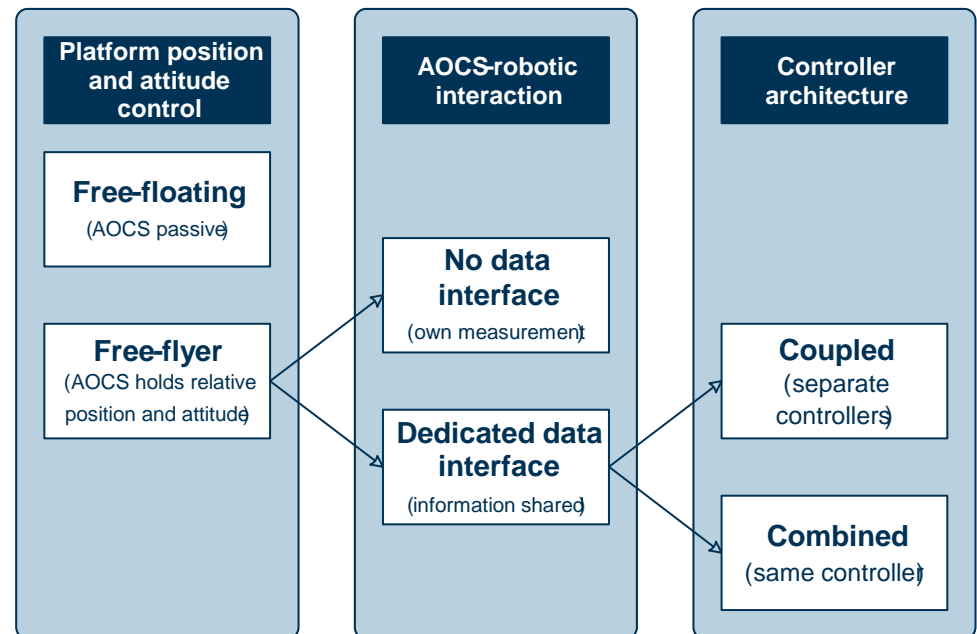
TCP Error - Docking Maneuver-SLOW





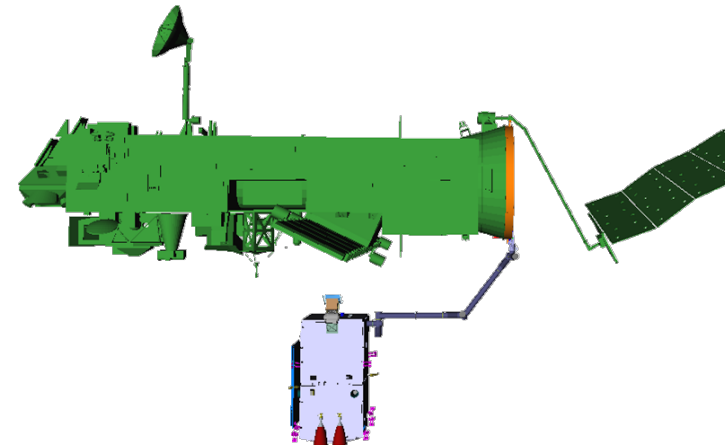
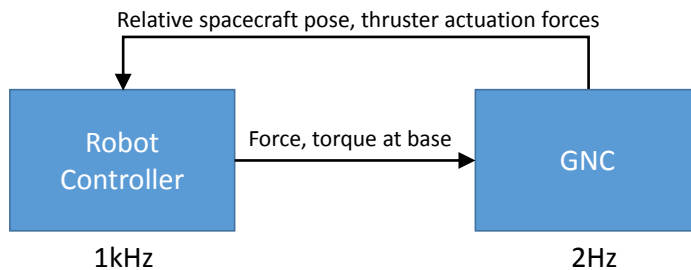
# Controller Interaction: Free-Floating vs. Free-Flyer

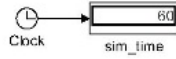
- Space robot: Free-flyer: two controllers (robot control and GNC) simultaneously act on the same system and could challenge each other
- Open loop (no direct information shared) vs. Closed loop (direct information shared)
- Coupled (two distinct controllers) vs. Combined (one mighty controller) approach
- Potential problems: different sampling rate (1kHz vs. 1-10Hz) and bandwidths, delays and stability



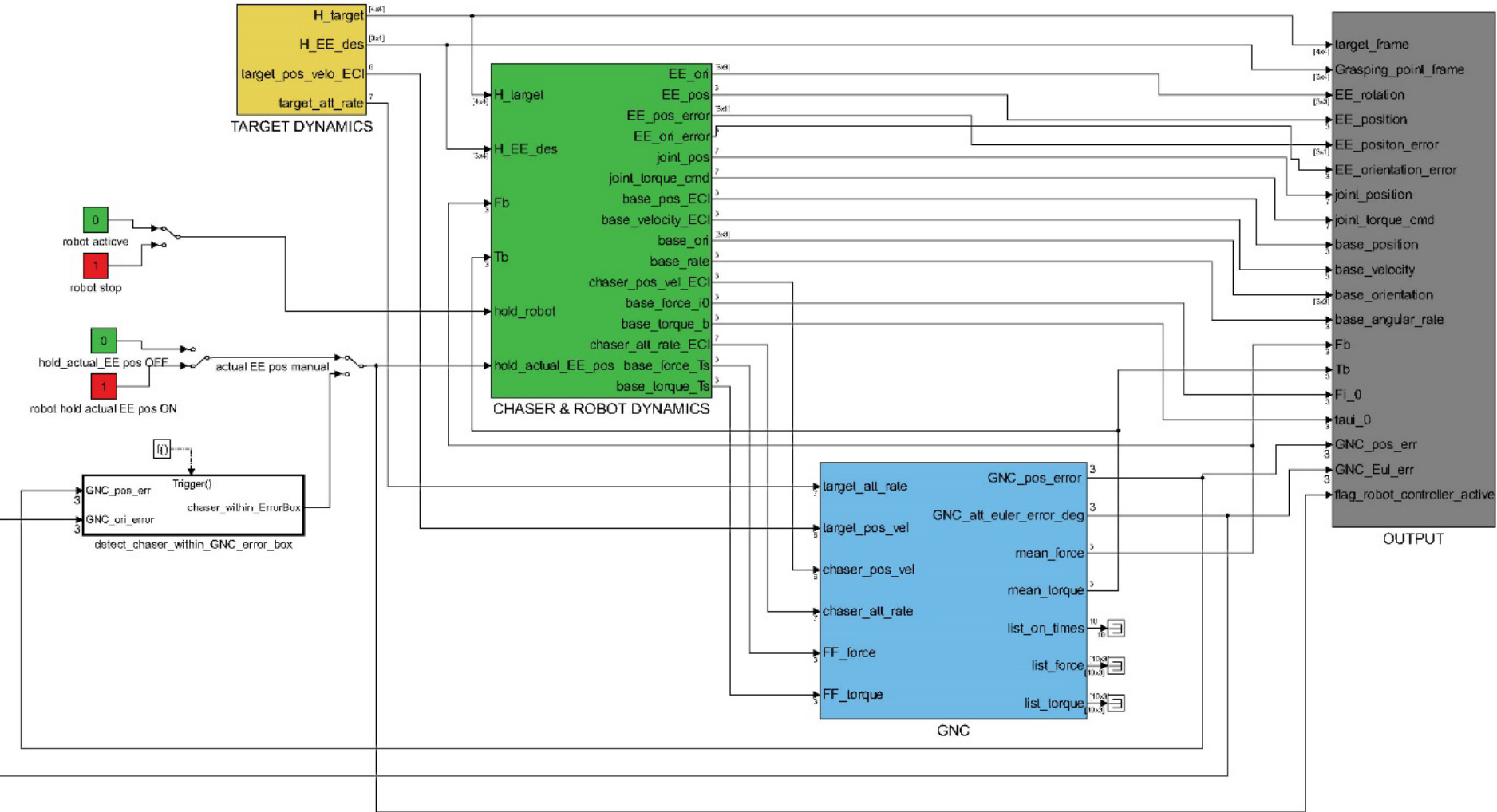
# Controller Interaction

- From GNC to robotic controller
  - Thruster actuation forces
  - Satellites relative pose and derivative (from relative navigation sensors)
  - Inertial pose and derivative (w.r.t. orbit position, for computing centrifugal forces)
- From robotic controller to GNC
  - Forces and torques acting on base
  - Robot CoM w.r.t. base (for global CoM and inertia update)

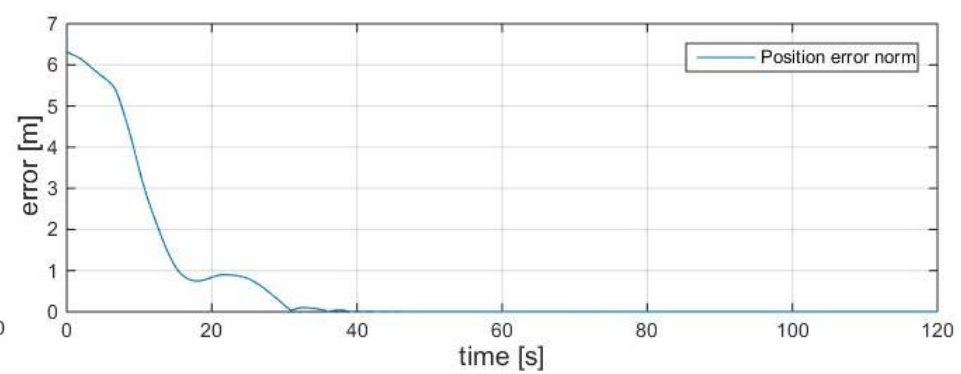
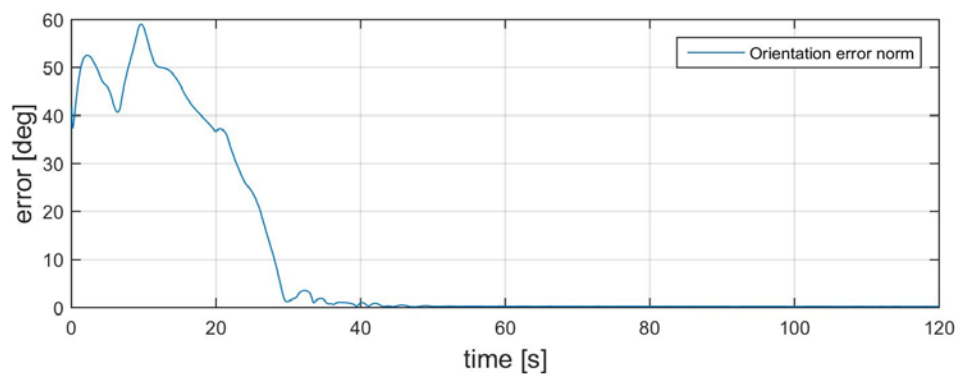
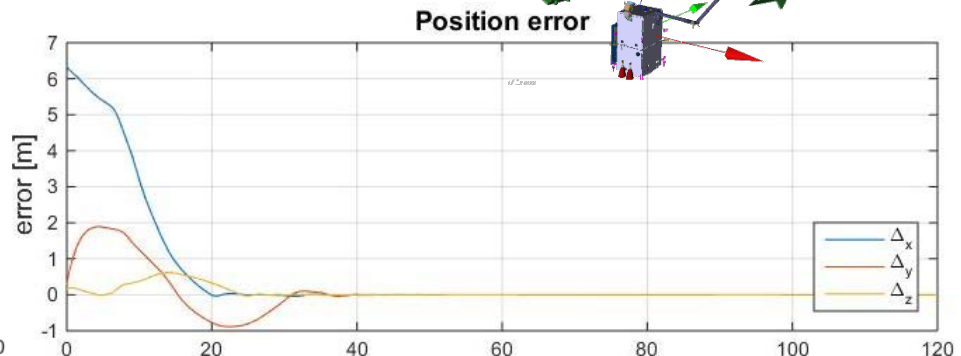
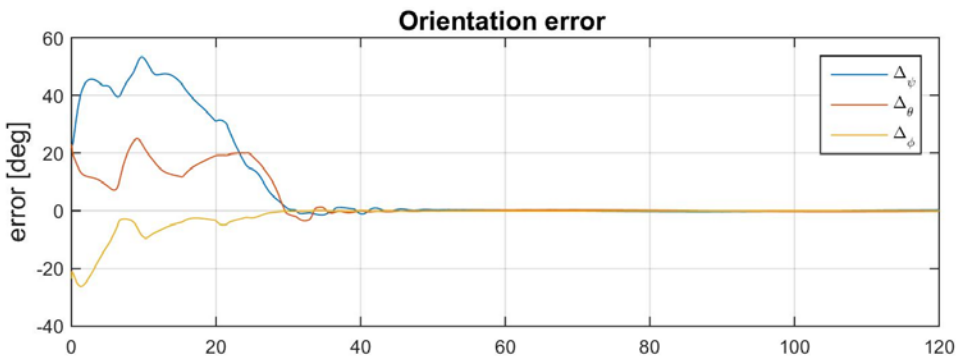
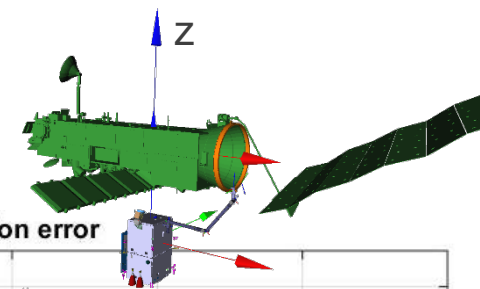




Dynamics and control for a free-floating robot

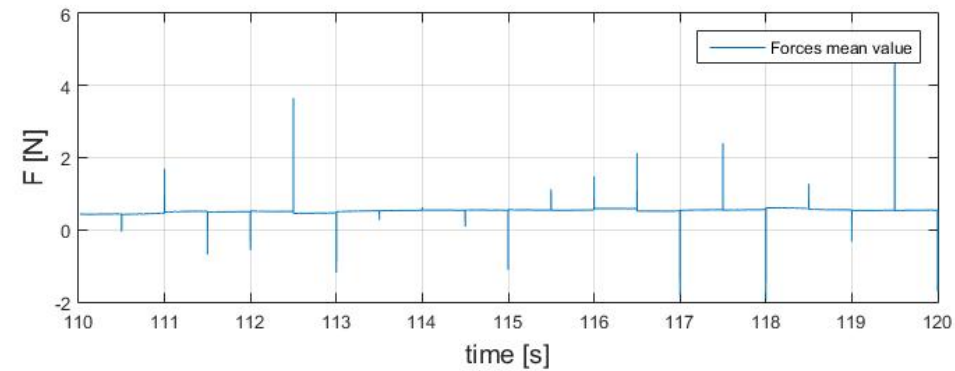
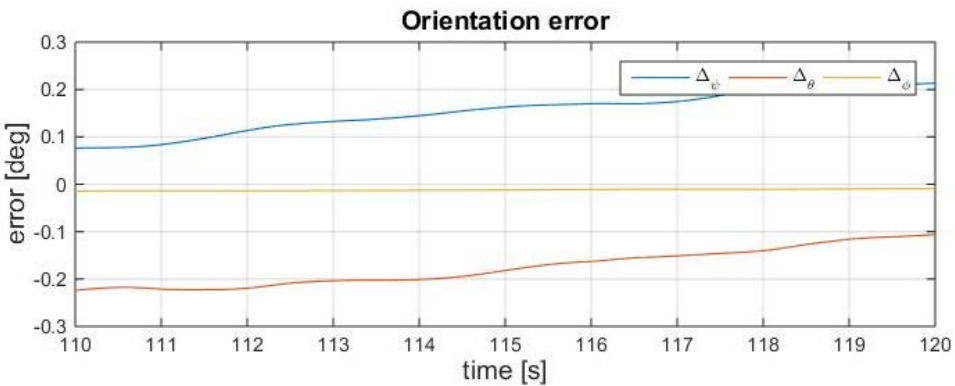
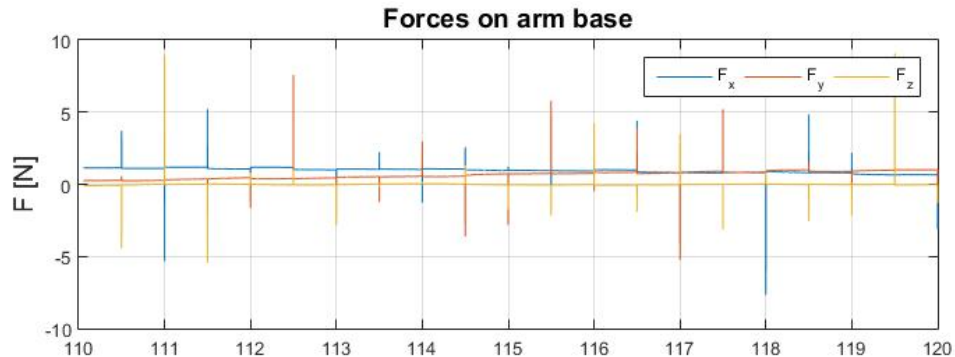
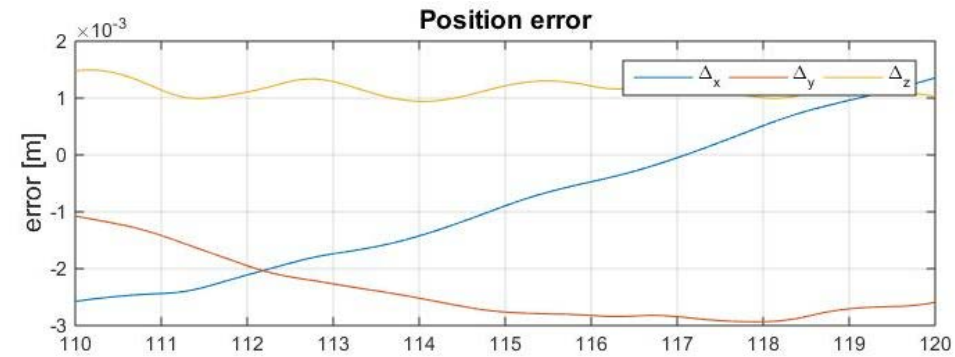


# Controller Results – Z-Rot, TCP

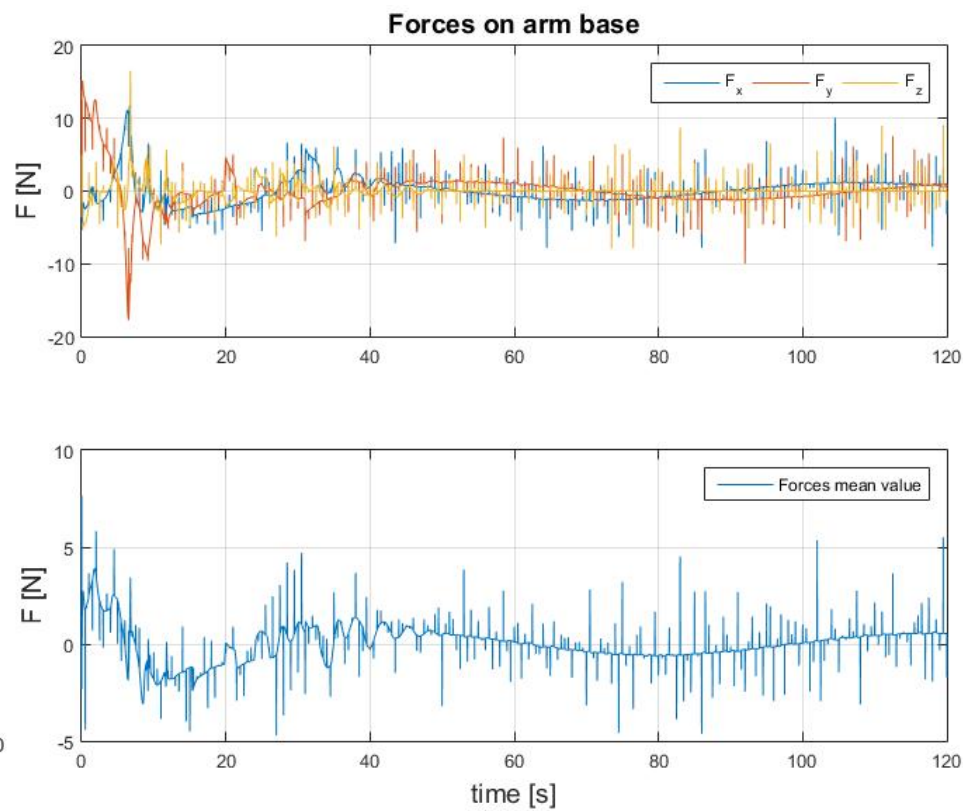
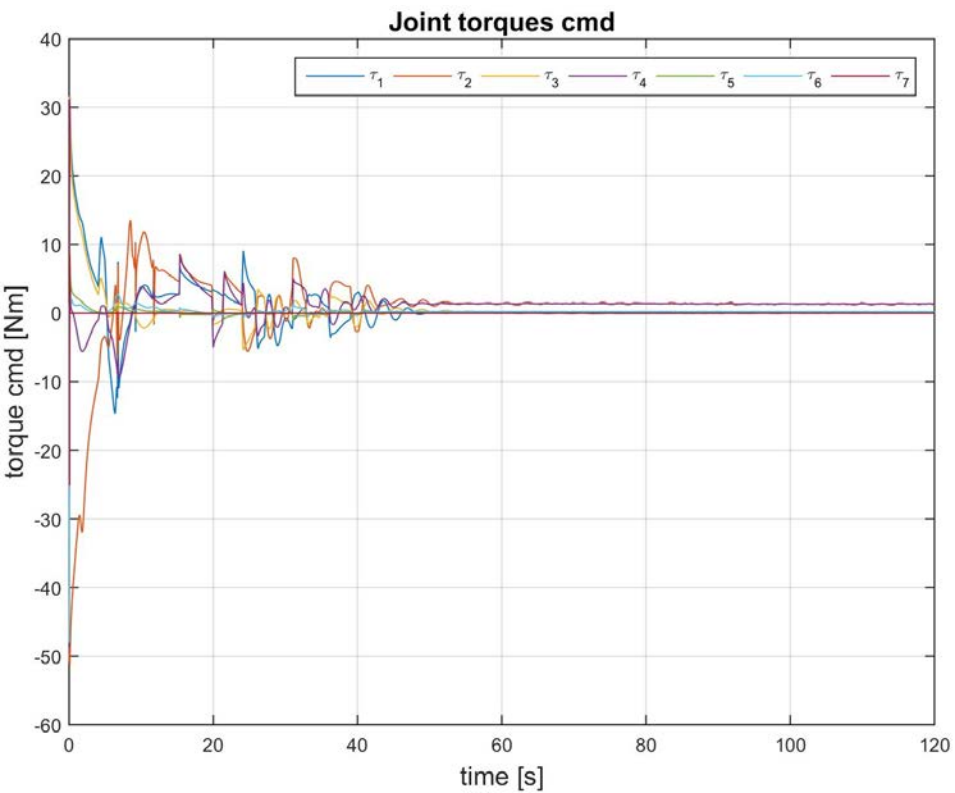




# Controller Results – Z-Rot, TCP Zoom-In

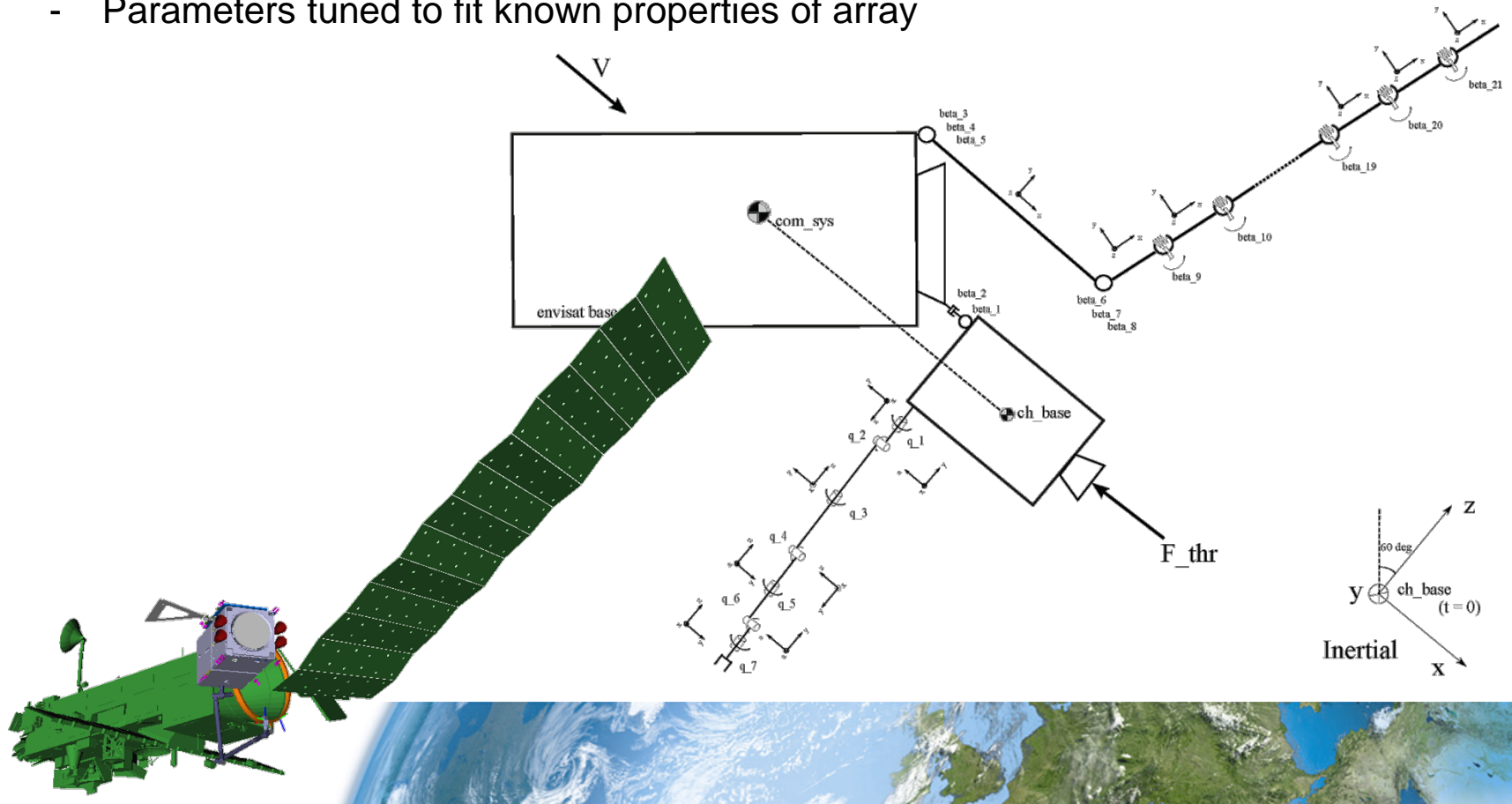


# Controller Results – Z-Rot, Arm



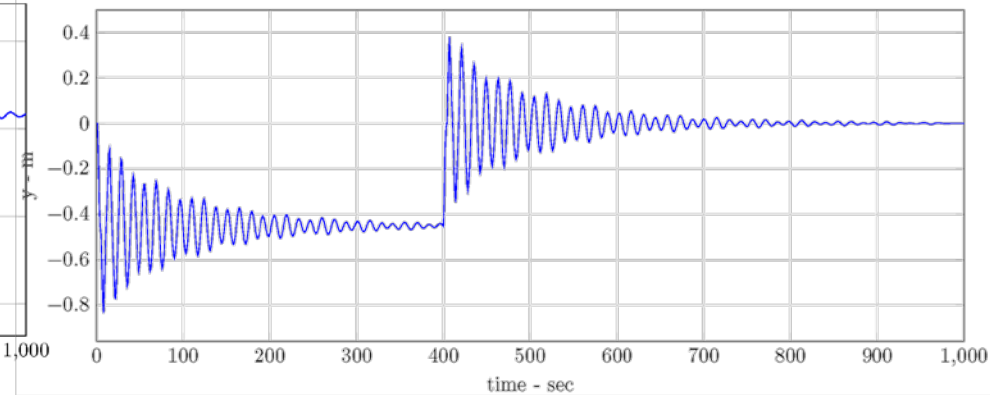
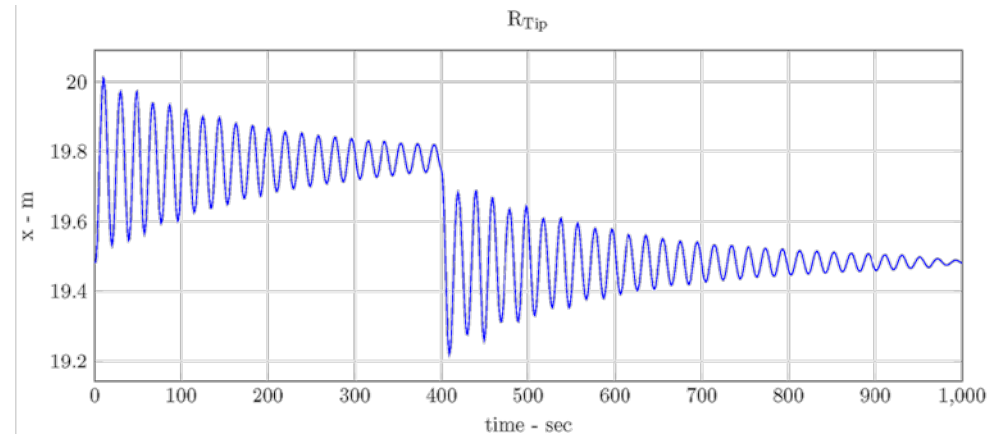
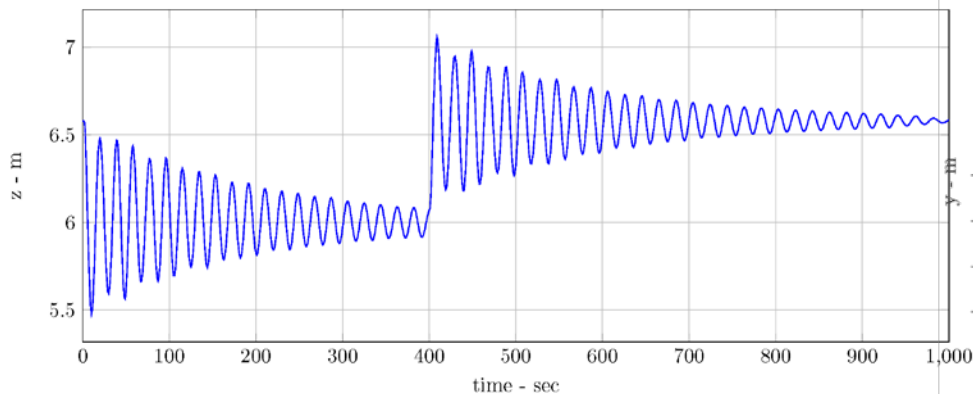
# De-Orbit: Solar Array Behavior

- Multi-body dynamics model in Matlab/Simulink environment using the SpaceDyn library and SIMPACK for verification
- Solar array modelled as rigid panel segments conected by flexible joints
- Parameters tuned to fit known properties of array



# Solar Array Dynamics – Solar Array Tip (90deg Clamp)

- Solar array tip position relative to platform COG for 90deg clamping position
- Less movement compared with 180deg clamp

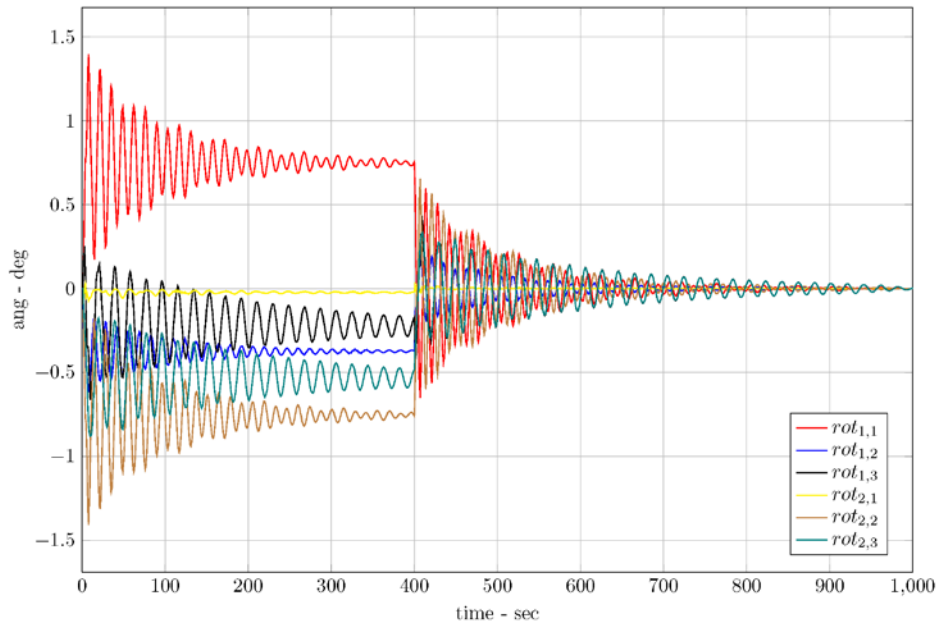




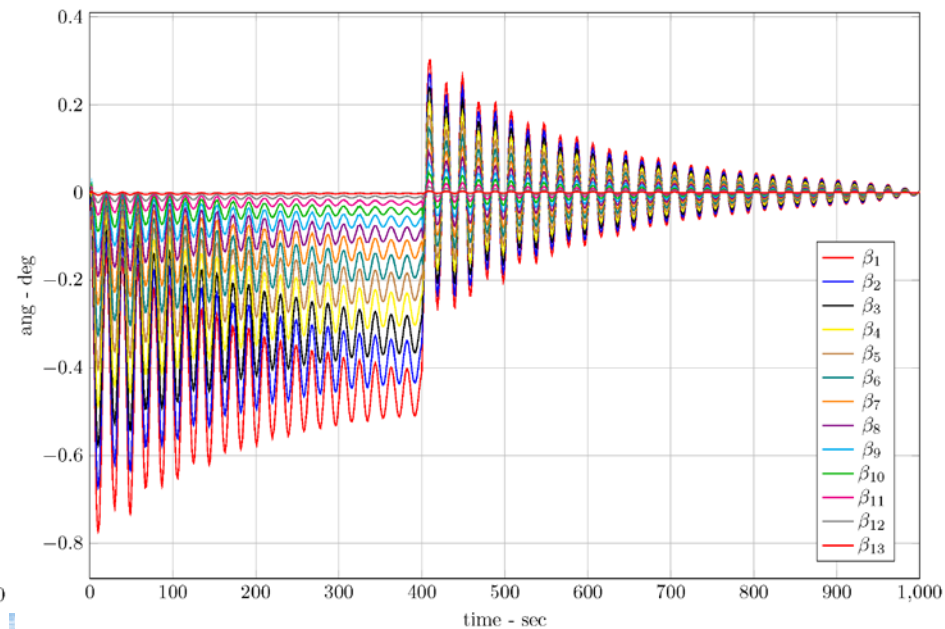
# Solar Array Dynamics – Boom and Array Joints (90deg Clamp)

- Rotation angle of boom (left) and solar array (right) joints for 90deg clamping position
- Less rotation compared with 180deg clamp (1.5deg vs. 0.8deg)

Rotation of Spherical Joints of SP Boom



Rotation of Envisat's Solar Panel Sections



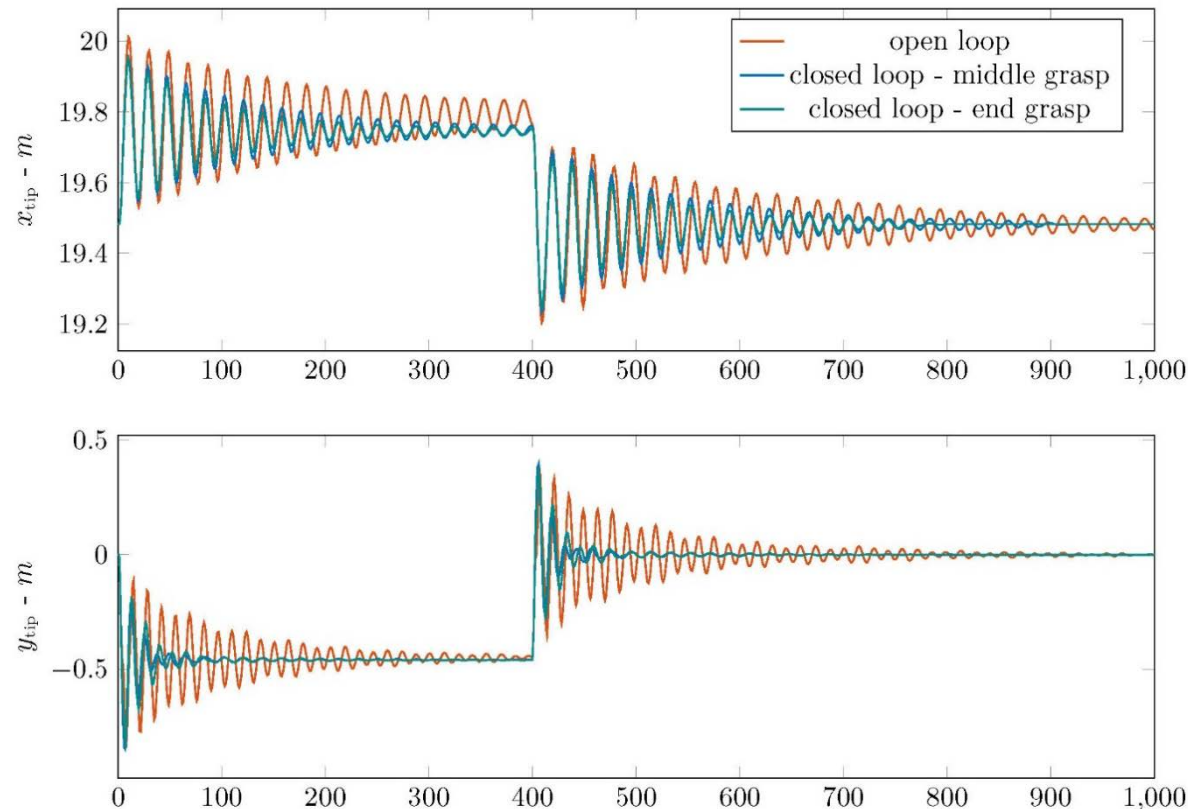


# e.deorbit - Analysis of De-Orbit Maneuver for 180deg clamping position



# Solar Array Dynamics – Solar Array Tip (Damped, 90deg Clamp)

- Solar array tip position relative to platform COG for 90deg clamping position
- Robot arm is grasping at the solar array boom (middle and end) and passively damping its motion (600Nm/rad)
- Better timely behavior, absolute peak is not damped significantly
- **Can improve de-orbit pointing accuracy but does not decrease chance of breaking**



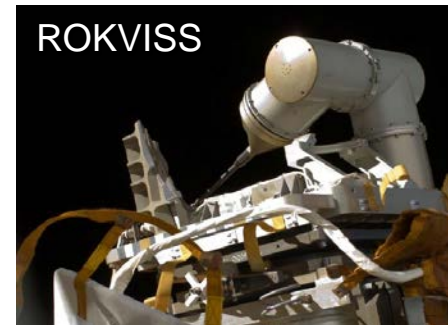
Thank you!





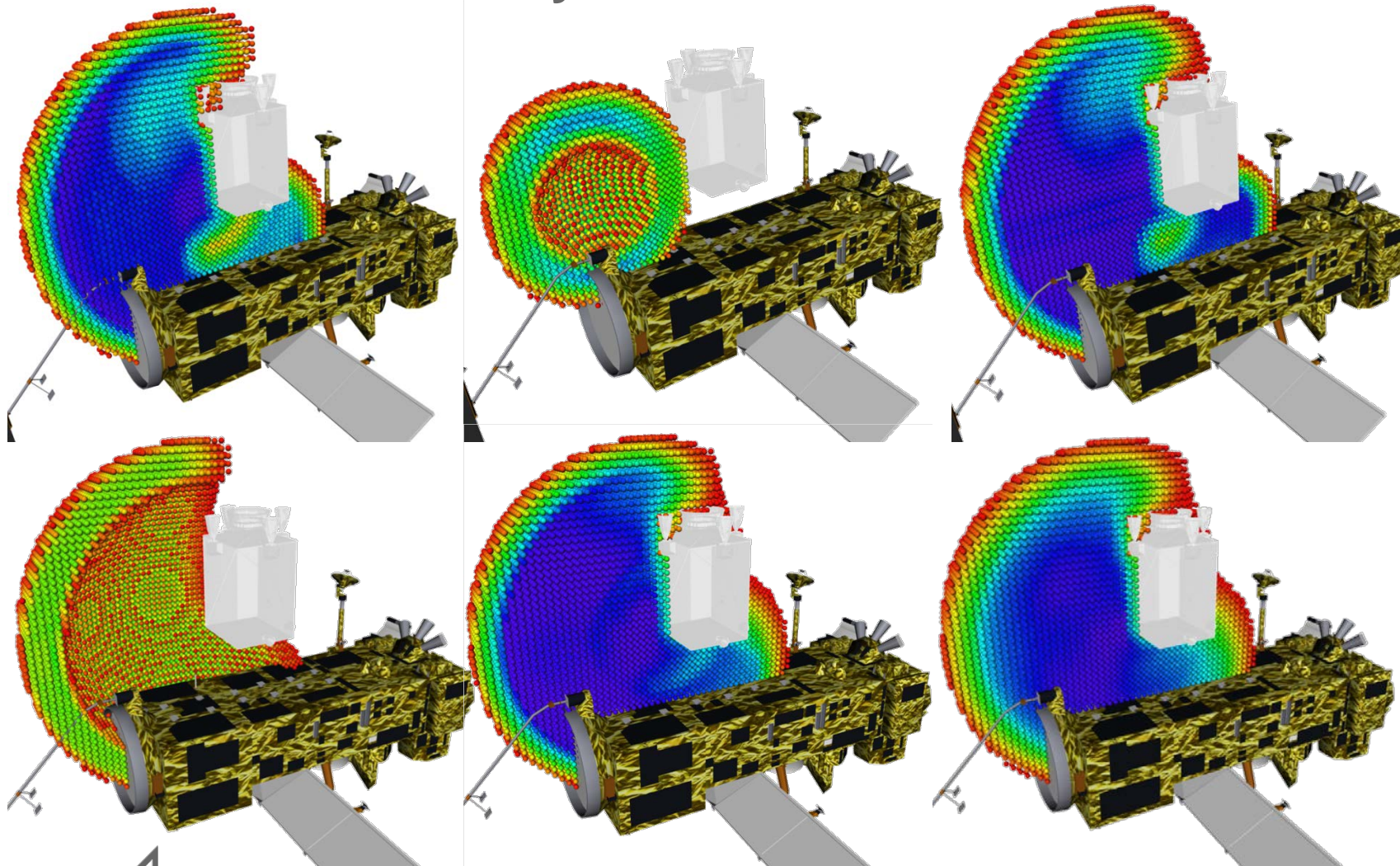
# Introduction – Space Robotics

- Future and already deployed robot applications in space:
  - **In-space robotic assembly (ISRA):** Shuttle Arms
  - **EVA assistance:** Robonaut, DLR's Justin, small satellites for inspection
  - **Robotic exploration:** MER's
  - **On-orbit servicing (OOS)** for prolonging lifetime of operational satellites, repair & refuel (RRM), extend or upgrade functionality (Hubble)
    - OOS for **active debris removal** from LEO or re-orbiting into graveyard orbit in GEO (DEOS)
  - **Dexterous manipulators** play essential role robotic manipulation in space – based on DLR's **7-DoF lightweight robot (LWR)** → Rokviss (middle) and 7-DoF space manipulator (bottom) with impedance control concept





# Workspace Analysis – Joint Failure



# Mechatronic Arm Positioning Accuracy

- Following aspects were included in the accuracy analysis:
- Motor-side joint position sensor (motor commutation sensor) resolution, relative accuracy, and absolute accuracy
- Harmonic Drive gearbox friction, stiffness, and backlash
- Output bearing friction and stiffness
- Harness disturbance torque
- Structural manufacturing inaccuracies and thermal effects (worst-case assumptions)
- Joint deadzone measurements
- Different relevant arm configurations

Parameter	Position control	Impedance Control
Absolute	14mm, 1deg	29mm, 7deg
Relative	0.5mm, 0.02deg	6.3mm



## Arm Worst-Case Error Budget

- Overall positioning error (including mechatronics, flexibility and tracking accuracy) is lower than required positioning accuracy by gripper

Parameter	Position	Orientation
Gripper Req.	15mm	5deg
Max. Error	9mm	0,3deg



# Solar Array Dynamics – Will it break?

- Carbon strength  $\sigma_{(flex, long)} > 1000 \text{MPa}$
- $D = 0.06 \text{m}$

$$\sigma_{max} = \frac{k\alpha_{max}D}{2I} \quad I = \frac{\pi(D^4 - d^4)}{64}$$

Inner diameter d [m]	$\sigma_{max}$ [MPa]
0.01	1.81
0.02	1.81
0.03	1.83
0.04	1.93
0.05	2.2

- Surprisingly - not a problem!

