

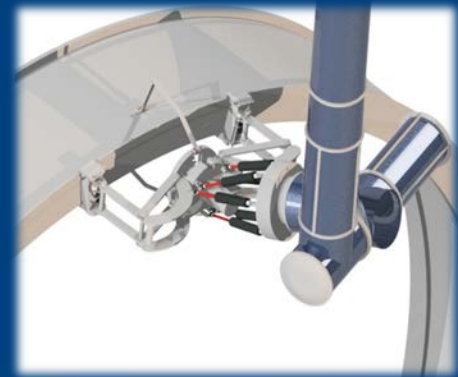


# Predator

## Short Project Presentation

ESTEC

24 October 2017



# **Contents of the Presentation**

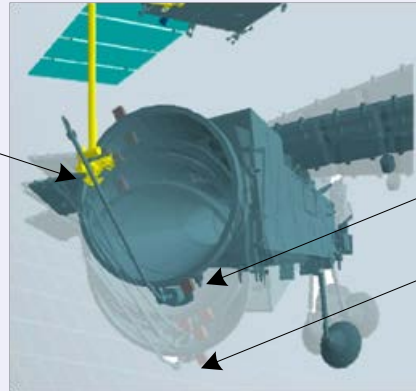
**LAR Motion Study and Videos**

**Stewart Platform study for Gripper isolation  
from DLR robot and Videos**



# LAR Motion Study : What is the expected range of motion and the timing?

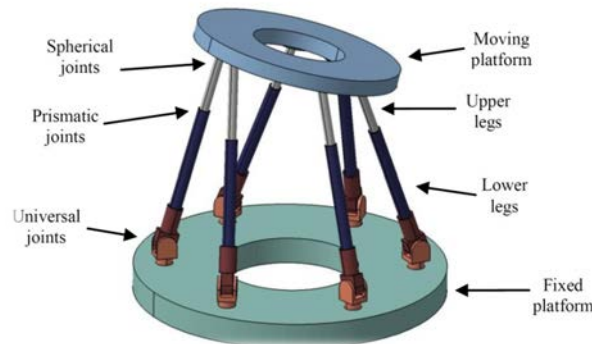
PREDATOR Gripper



Upper limit of oscillation

Lower limit of oscillation

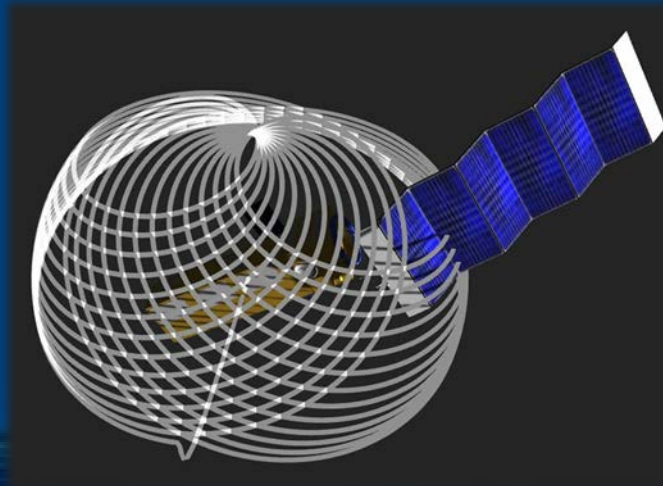
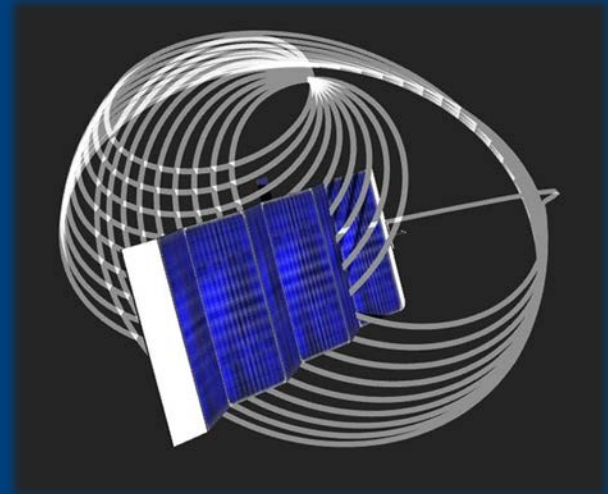
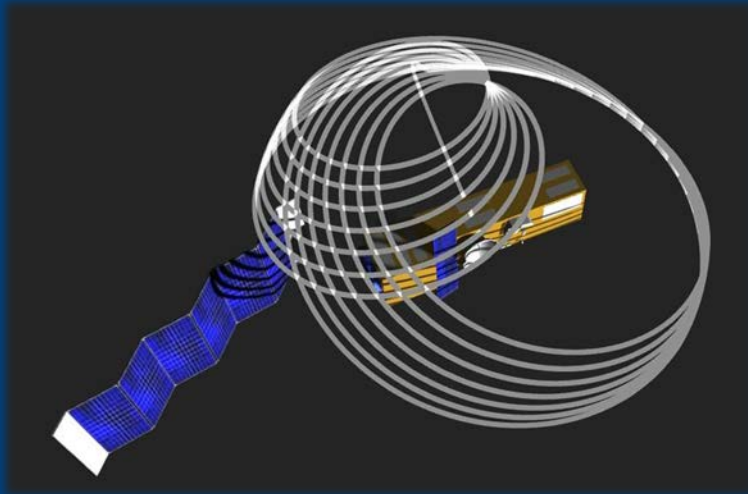
## Stewart Platform : Can it be used to isolate the gripper from the DLR arm?



# LAR Motion Study Examples

## An Impossible to Catch Scenario Example 1/2

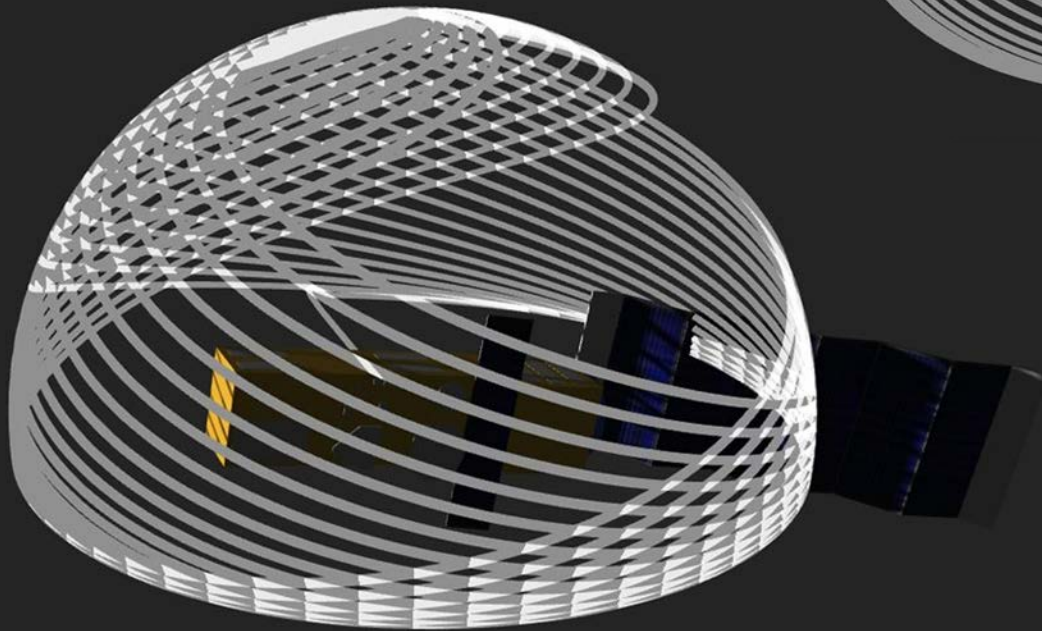
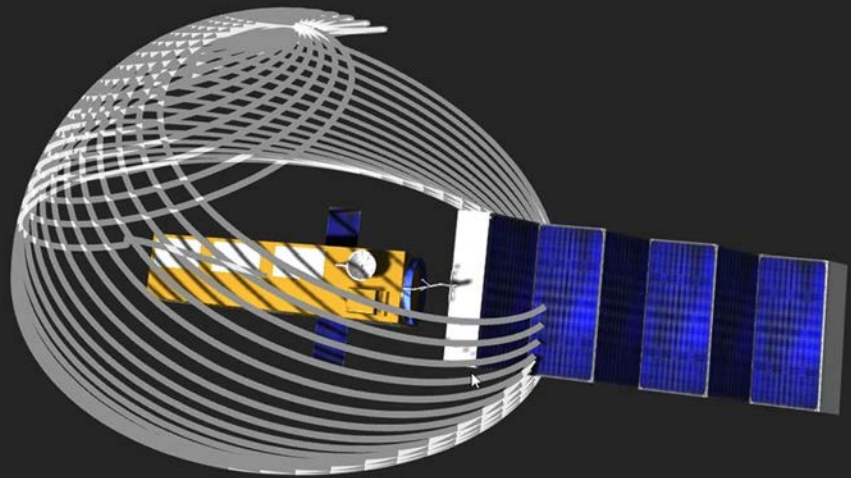
During this simulation the satellite (ENVISAT) is moving in a way that does not allow the chaser to approach it safely.



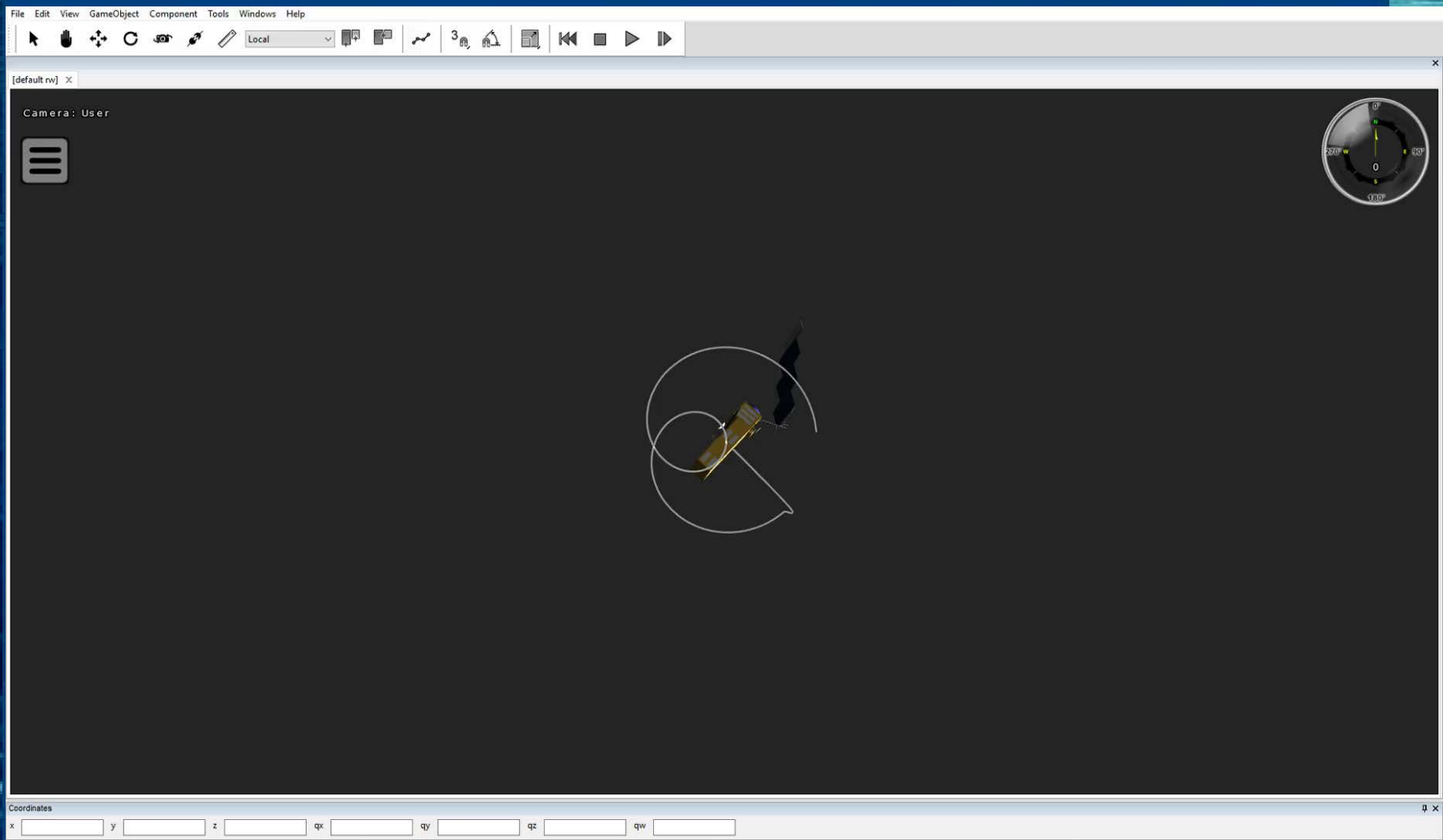
# LAR Motion Study

## Example 2/2

This scenario is similar to the scenario 1 presented by B1 Phase Final Report page 9-41 and it is clear that the chaser cannot approach safely the target satellite (ENVISAT)

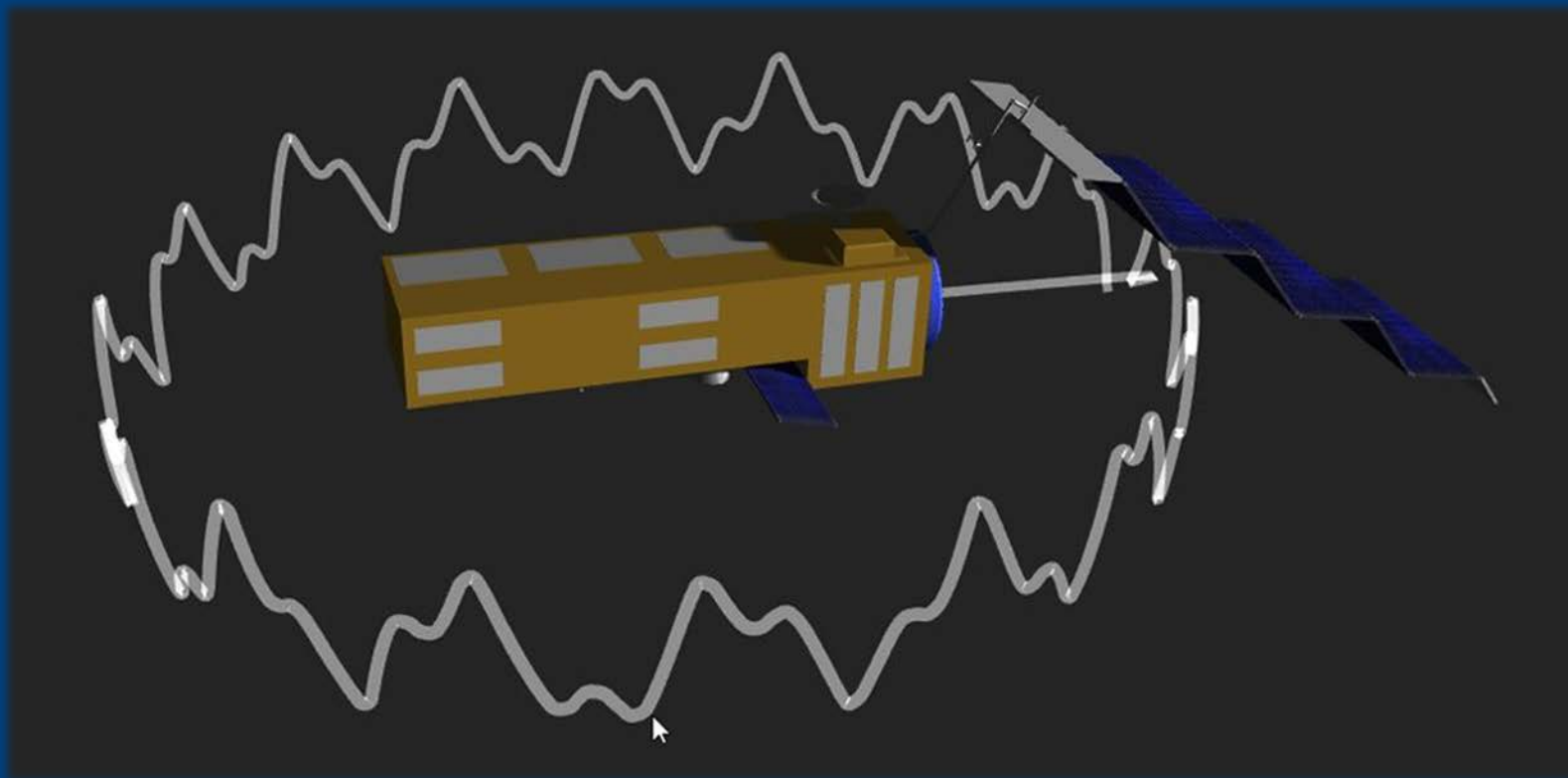


A whole hemisphere is covered by the marker on z-axis of ENVISAT body frame



# LAR Motion Study

## A Possible to Catch Scenario 1/4

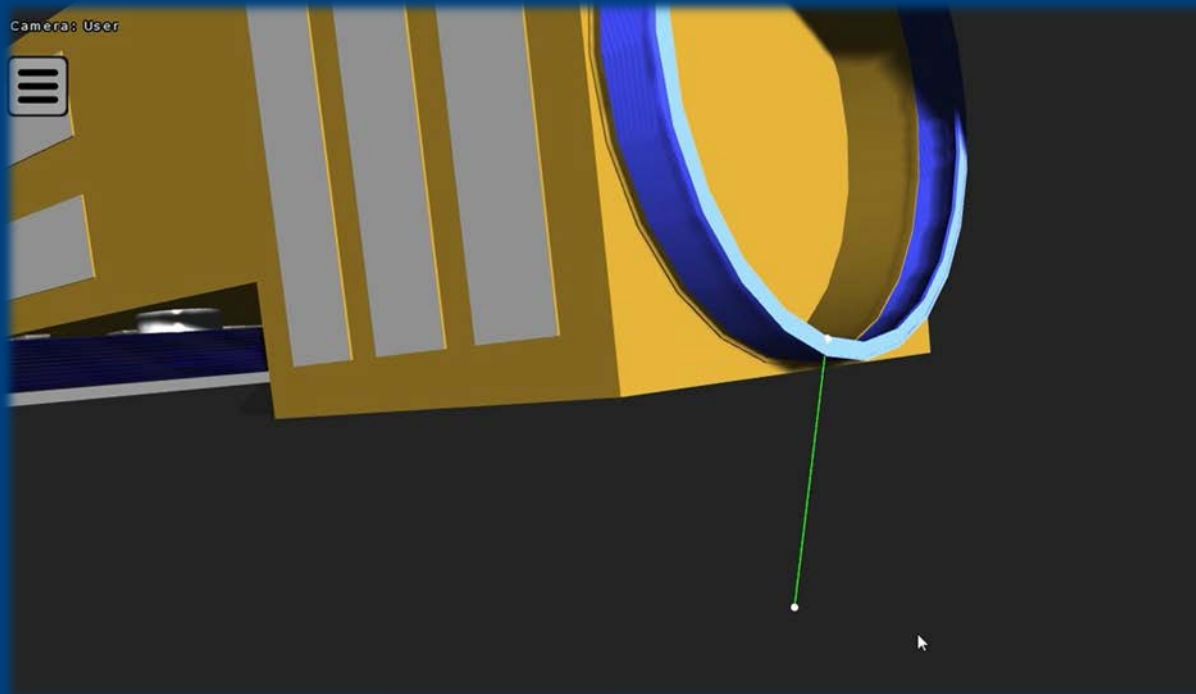


Overall view of the tumbling motion (Scenario 3 of B1 phase Final Report)



# LAR Motion Study

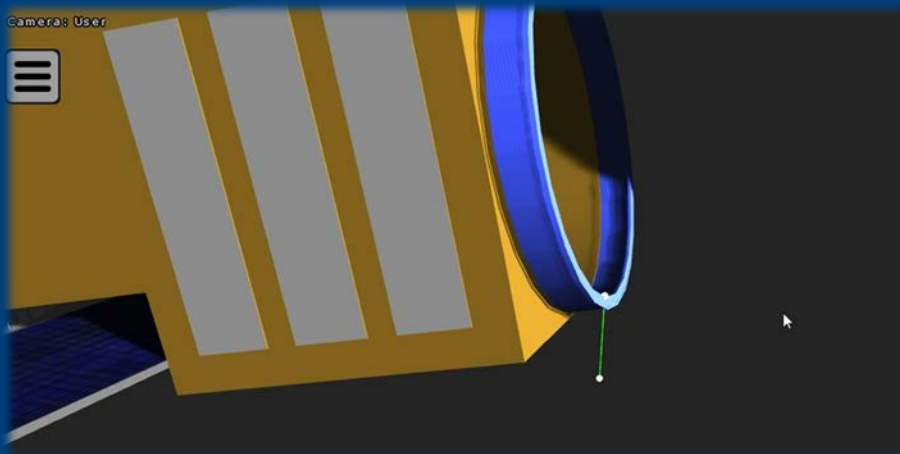
## Simulation 2/4



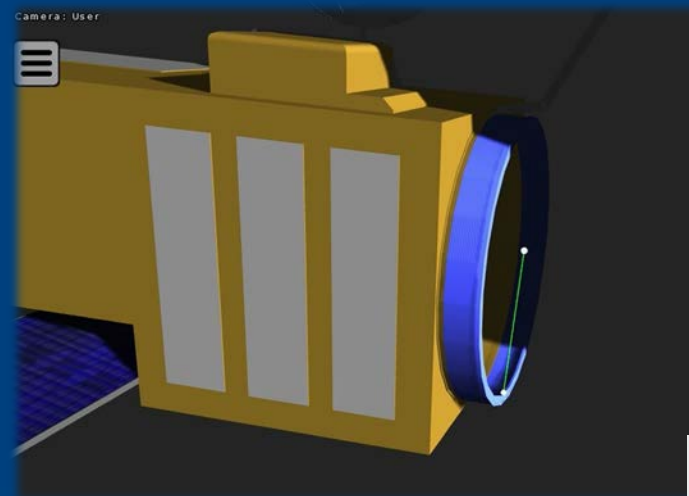
A slow oscillation of a very small amplitude is observed, if the spin (z) axis of the chaser is synchronized with ENVISAT

# LAR Motion Study

## A Possible to Catch Scenario 3/4



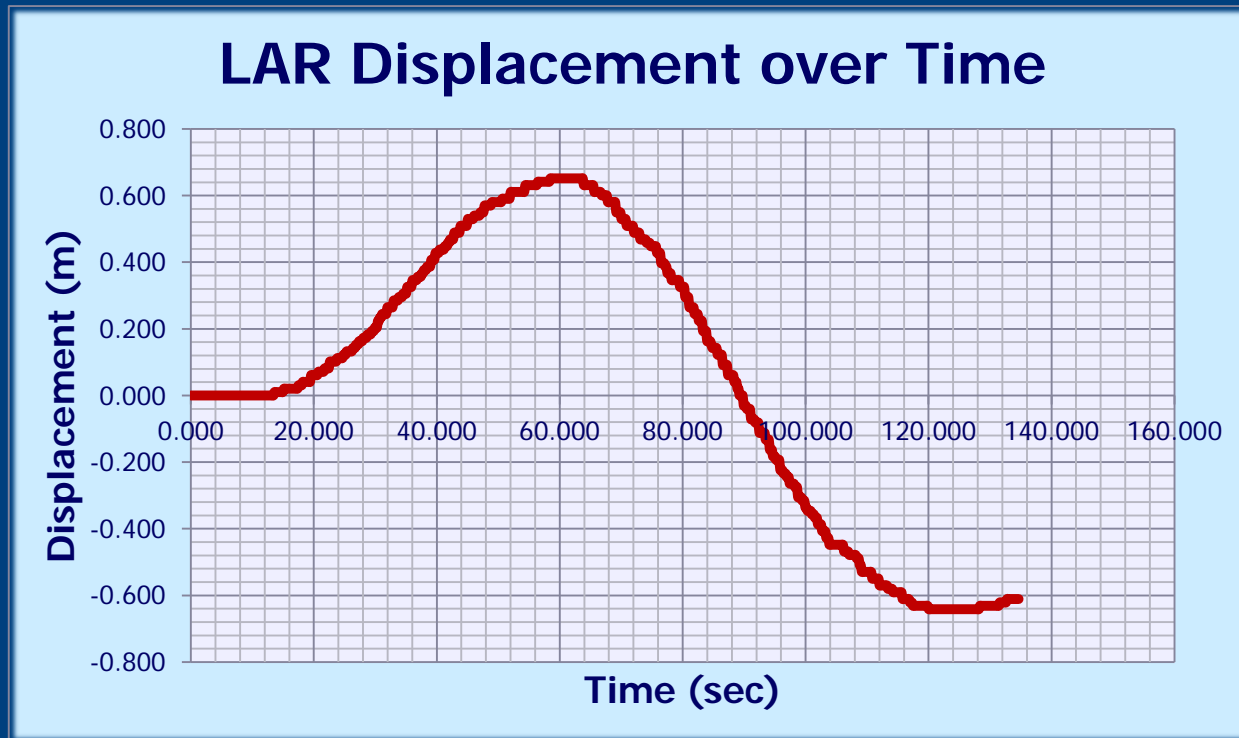
Two positions of slow oscillation.  
The displacement is sufficient for a safe grab.



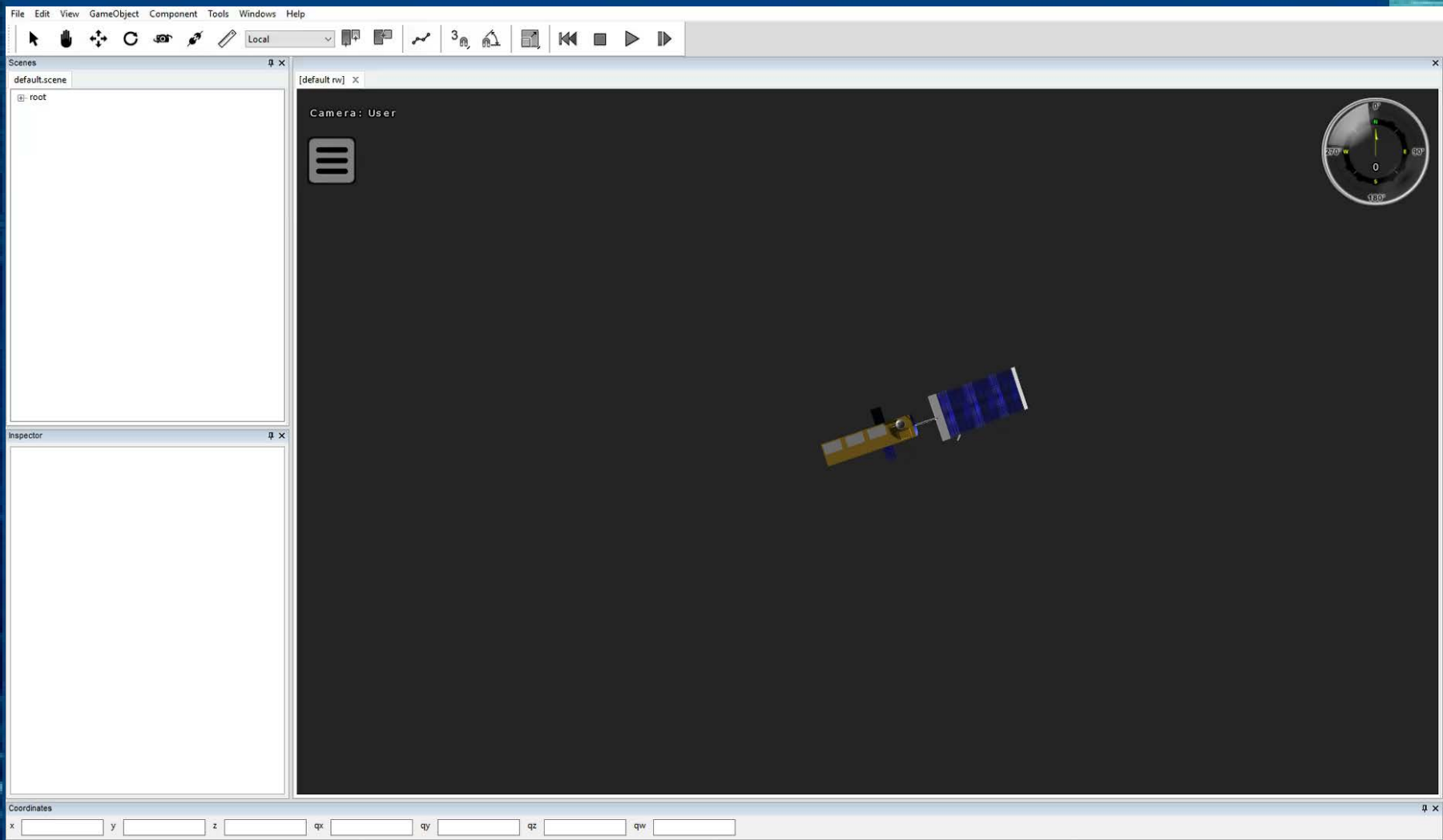


# LAR Motion Study

## Simulation 4/4



For the time interval (00:50 - 03:02) of this simulation, there are time periods of several seconds in which the LAR is idle, or it displaces itself for a few cm (minimum and maximum of the graph)

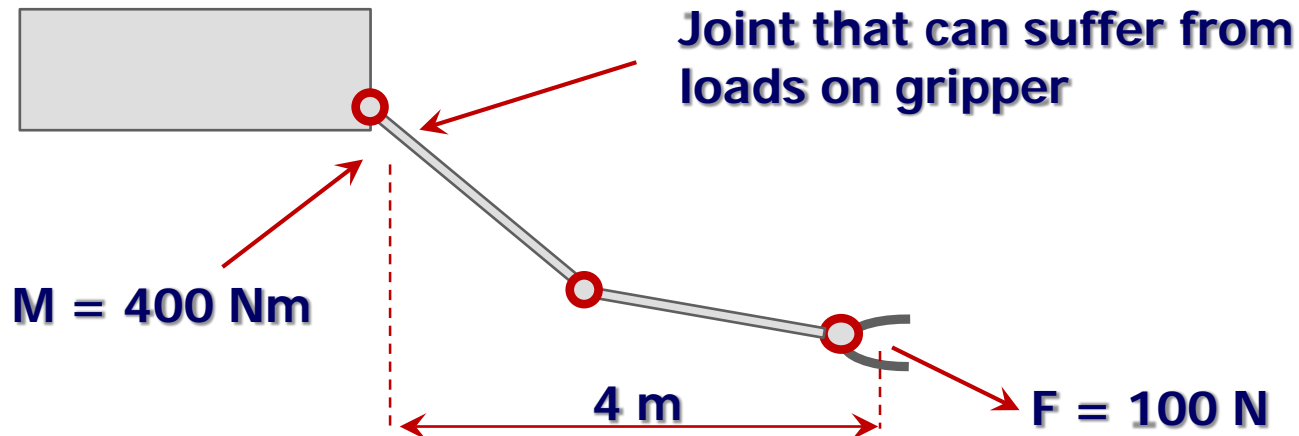


# Stewart Platform study for Gripper isolation

## The Problem

### DLR ARM

Very long structure with substantial moment of inertia and limited max torque on joints

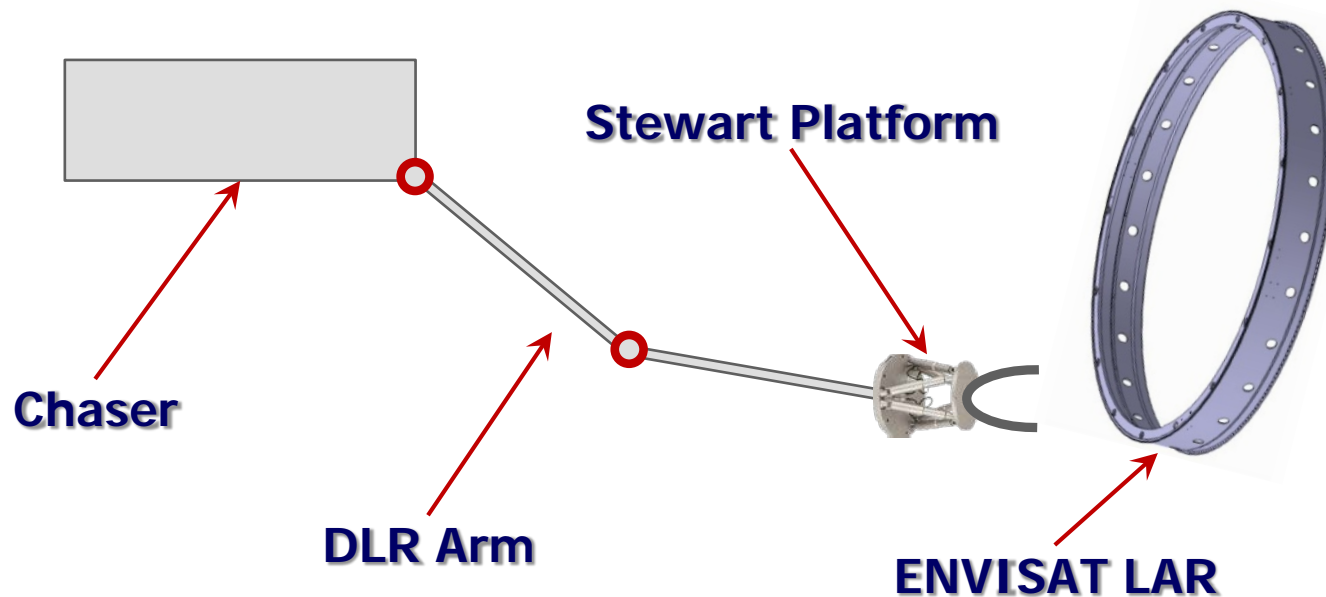


# Stewart Platform

## The Solution

### Stewart Platform

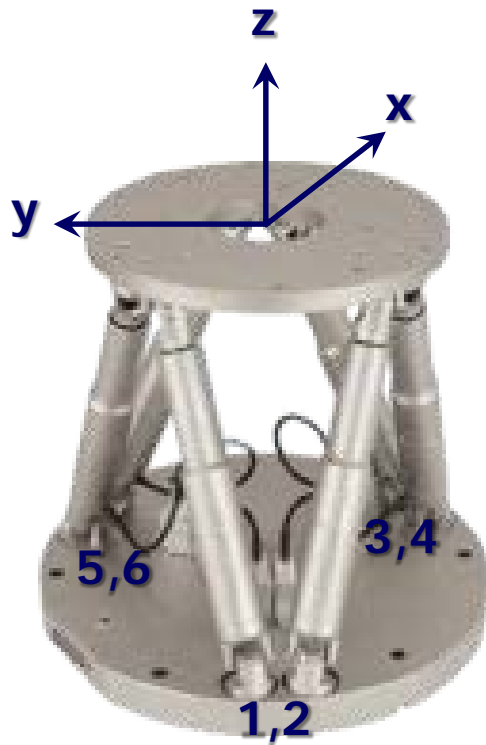
A variable impedance 6-DOF wrist



# Stewart Platform

Can be driven either with Direct Kinematics

## Direct Kinematics



$$\begin{bmatrix} F_1 & F_4 \\ F_2 & F_5 \\ F_3 & F_6 \end{bmatrix}$$

Given Forces  
along legs 1,...,6



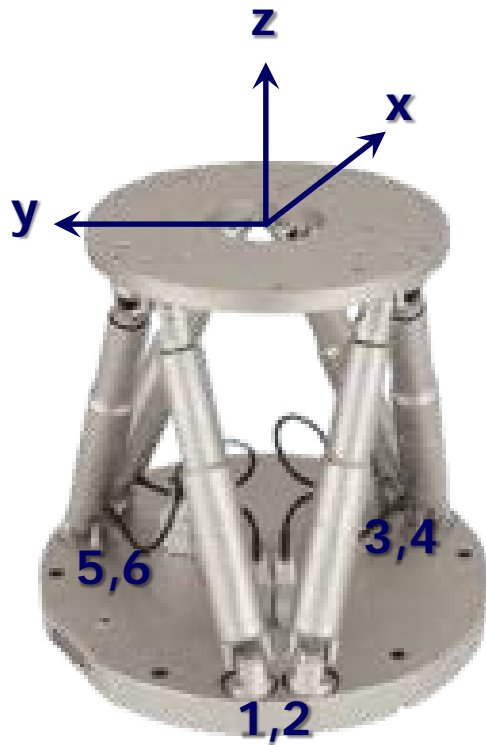
$$\begin{bmatrix} F_x & M_x \\ F_y & M_y \\ F_z & M_z \end{bmatrix}$$

Produced Forces  
and Torques  
along x, y, z axes

# Stewart Platform

Or with Inverse Kinematics

**Inverse Kinematics**



$$\begin{matrix} F_x & M_x \\ F_y & M_y \\ F_z & M_z \end{matrix}$$

Given Forces and  
Torques along x,  
y, z axes



$$\begin{vmatrix} F_1 & F_4 \\ F_2 & F_5 \\ F_3 & F_6 \end{vmatrix}$$

Produced Forces  
along legs 1,...,6

# Stewart Platform



**Pre-prototype built for  
concept verification and  
control loop tuning**

**Specifications :**

**Workspace : 100 x 100 x 100  
mm, 40° rotation**

**Speed : 30mm/sec**

**Max force: 30N, all directions**

**Max torque : 2 Nm, all  
directions**

**Mass: 7 kg**

**Power: 18W**



# Stewart Platform





**End of Presentation**