

Part-to-part and lot-to-lot variability study of TID effects in bipolar linear devices

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- **Definition of Radiation Design Margin (RDM) requirements for Radiation Verification Testing (RVT) on flight lots under Total Ionizing Dose (TID)**
- **Critical for linear bipolar devices**
 - Likely to show part-to-part and lot-to-lot variation in TID sensitivity
- **Investigation on the within-one-lot and inter-lot variability on three different references**
 - Experimental characterizations
 - Data analysis
- **One-sided tolerance limit (K_{TL}) method is usually considered for TID testing**
 - Applied to our test data
 - Compared to a Maximum Likelihood Ratio (MLR) method which is investigated and provides an interesting accuracy

- **Three different references were irradiated**
 - ▶ Three lots were tested for each reference
 - ▶ 30 devices were irradiated for each lot

- **Cobalt 60 TID test**
 - ▶ Dose rate 210 rad/h
 - ▶ GAMRAY facility (TRAD – Labège, France)

Device	Part number	Manufacturer	Lots
LM124AWG	5962R9950401VZA	Texas Instruments	0539A 1136A 1306A
AD584SH	5962R3812801VGA	Analog Devices	0125A 0226A
AD584SH	5962-3812801VGA	Analog Devices	1052A
TL1431ACZ	-	ST Microelectronics	GE245074 GE334152 GE337030

Op. Amp.

Volt. Ref.

- **Radiation hardness assurance standards**

- ▶ **Intra-lot variability taken into account with the 3-sigma approach**
 - Over a test sample, the electronic device parameter drift considered for the worst-case analysis is mean ± 3 sigma
- ▶ **Inter-lot variability taken into account with periodic testing**
 - RVT periodicity depends on space project prime-contractor

- **In most of the cases, the 3-sigma approach is representative enough and well adapted (when the associated risk is accepted) to take into account the intra-lot variability for a space project**

- ▶ **This study focuses on the few other cases...**
 - In this presentation, 3 worst-cases (1 per tested reference) are shown
- ▶ **Investigate the application of another statistical methodology (MLR) that could be applied when a higher confidence level is required**

- **First level analysis**

- ▶ 3-sigma approach
- ▶ $K_{TL} = 2.742$ for $n = 5$ (C=90, P=90) [1]



Experimental mean 'm'

$$m = \frac{1}{n} \sum_{i=1}^n x_i$$

$$s = \sqrt{\frac{1}{n-1} \sum_{i=1}^n (x_i - m)^2}$$

Standard deviation 's'



- **Second level analysis**

- ▶ Maximum Likelihood Ratio
- ▶ Test data fitted to a normal law

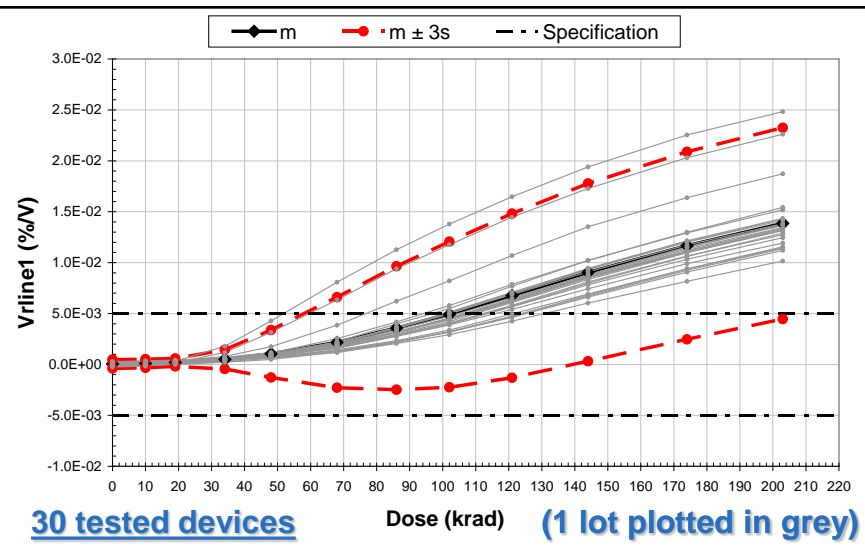
$$f_{nm}(x, \mu, \sigma) = \frac{1}{\sigma\sqrt{2\pi}} \exp\left[-\frac{1}{2}\left(\frac{x - \mu}{\sigma}\right)^2\right]$$

Normal law (2 parameters μ and σ)

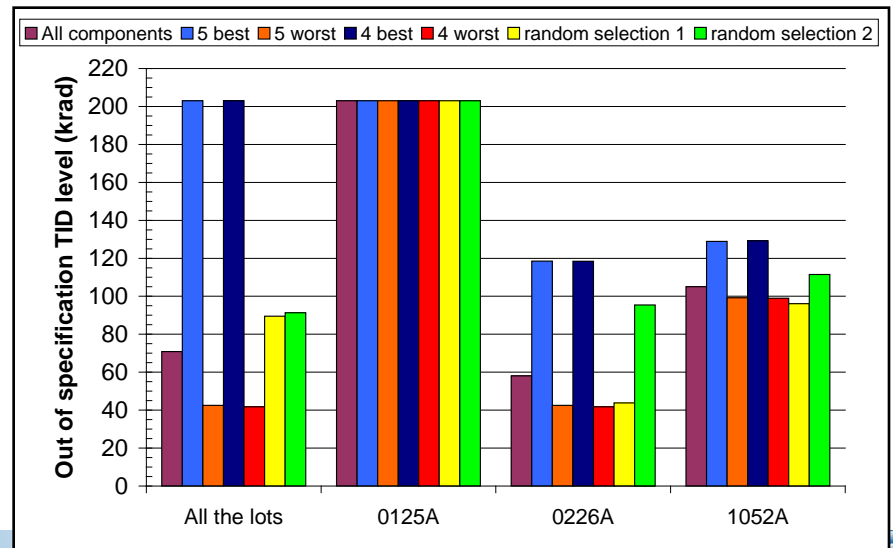
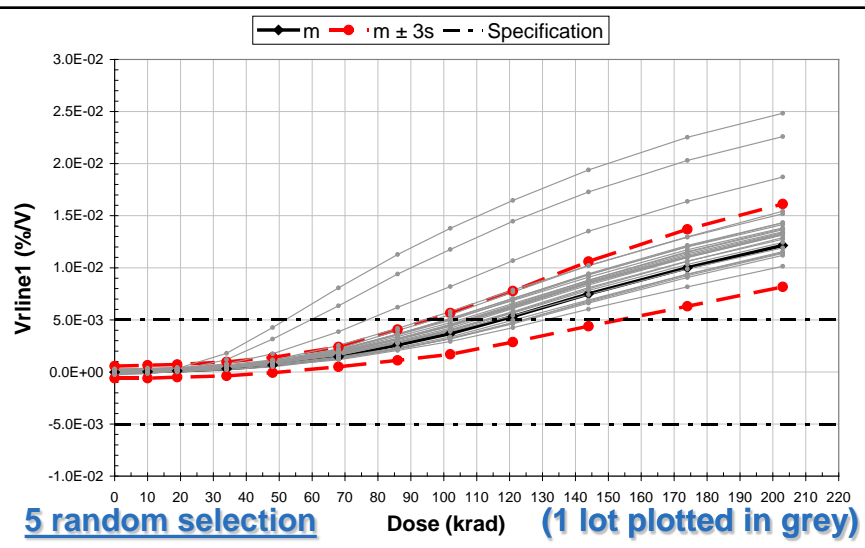


- **2-level analysis based on the use of experimental parameters 'm' and 's' as defined above, as well as statistical parameters 'μ' and 'σ'**

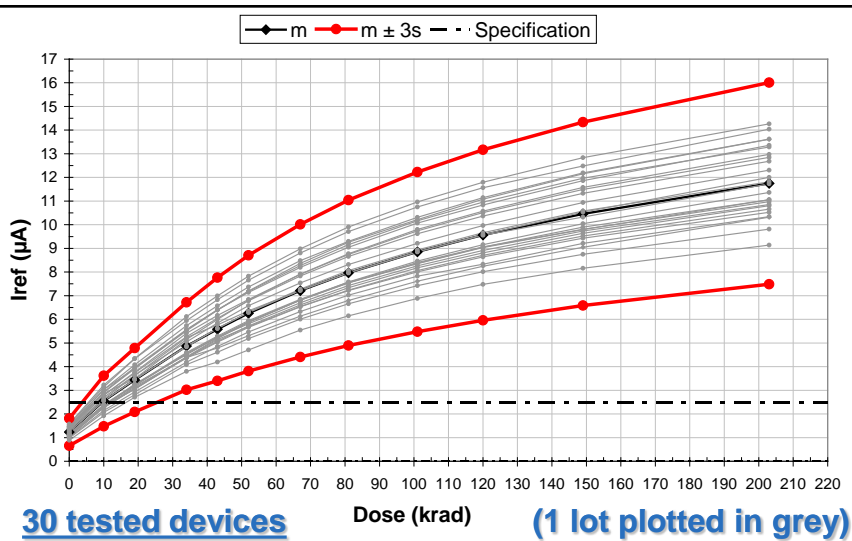
■ **AD584SH Vrline1 (%V) lot 0226A**



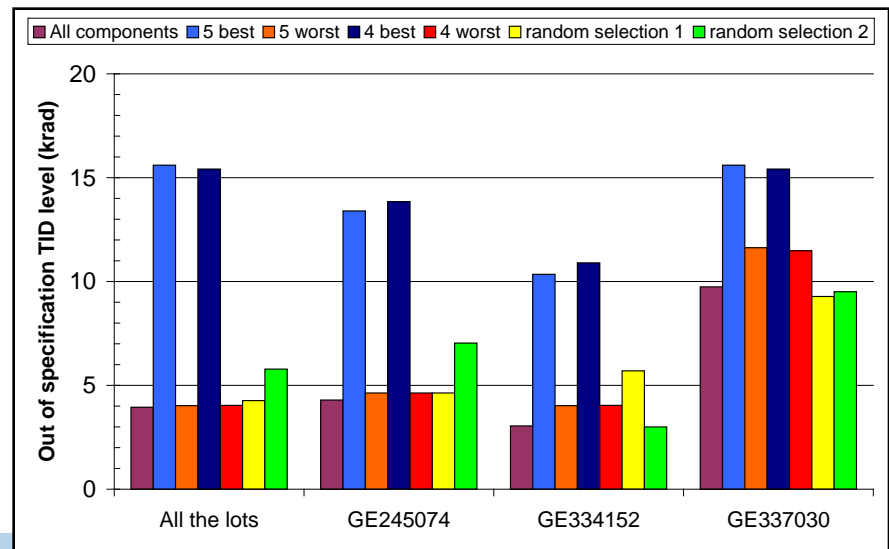
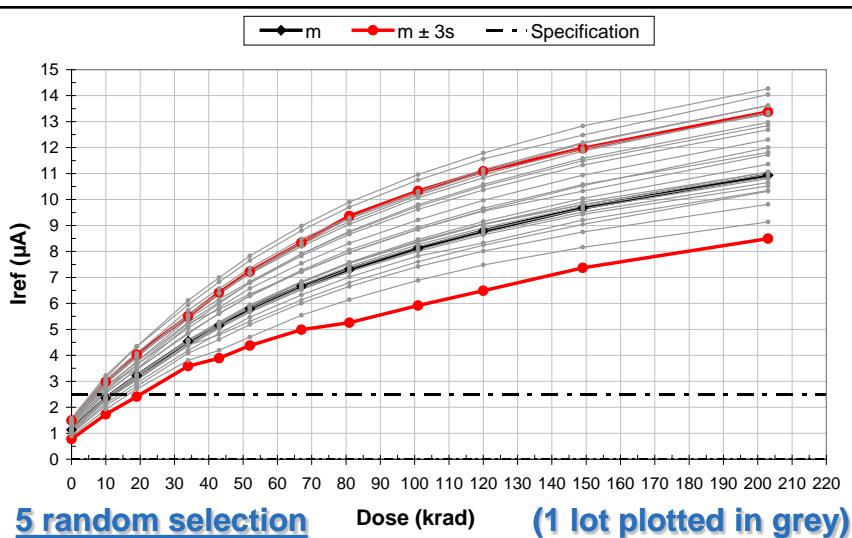
- Mean ± 3 sigma calculated over the 30 tested devices
- Mean ± 3 sigma calculated over 5 randomly selected devices
- Estimated lot behaviour for different subgroups
 - Out-of-specification TID level based on m+3s limit
 - All devices, 5 best or worst, 4 best or worst, random selections



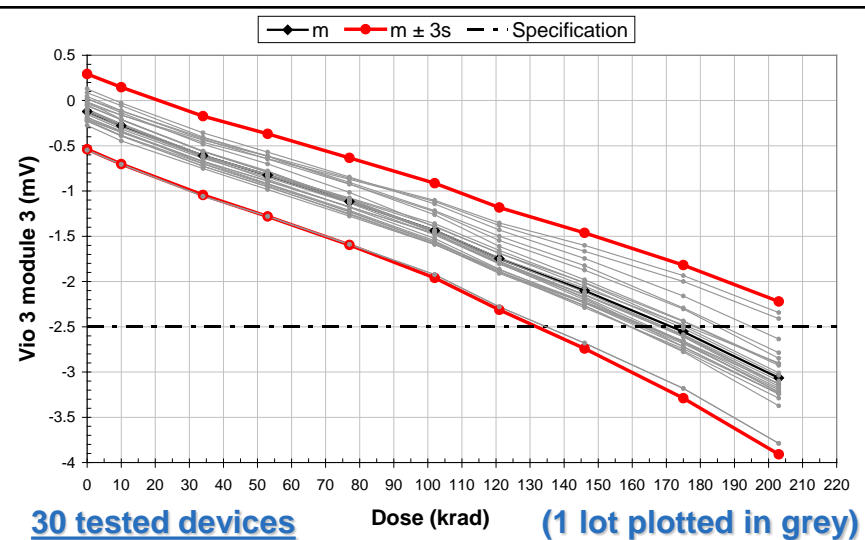
■ **TL1431ACZ Iref (µA) lot GE334152**



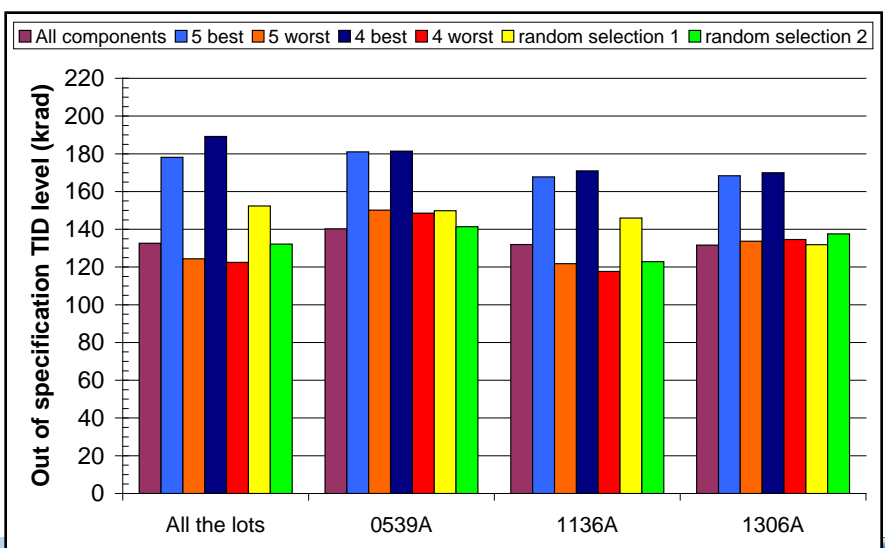
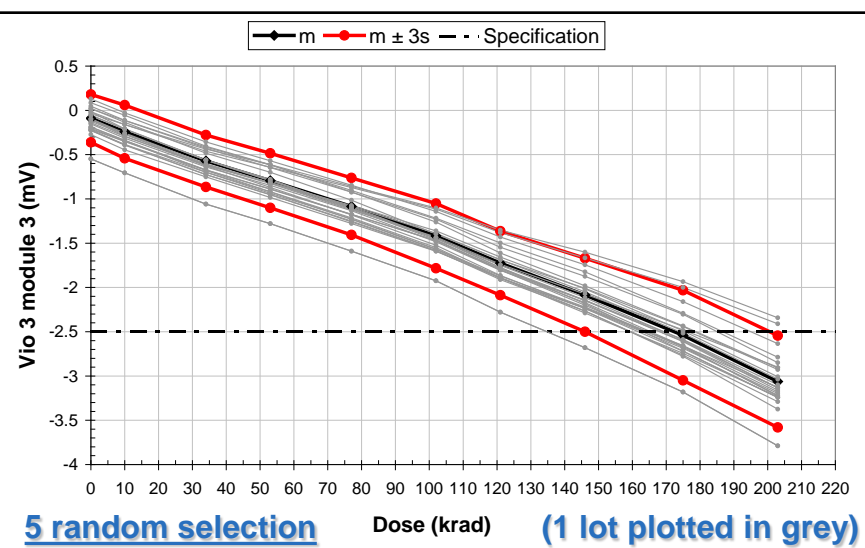
- Mean ± 3 sigma calculated over the 30 tested devices
- Mean ± 3 sigma calculated over 5 randomly selected devices
- Estimated lot behaviour for different subgroups
 - Out-of-specification TID level based on m+3s limit
 - All devices, 5 best or worst, 4 best or worst, random selections



■ **LM124AWG Vio3 module 3 (mV) lot 1136A**



- Mean ± 3 sigma calculated over the 30 tested devices
- Mean ± 3 sigma calculated over 5 randomly selected devices
- Estimated lot behaviour for different subgroups
 - Out-of-specification TID level based on m+3s limit
 - All devices, 5 best or worst, 4 best or worst, random selections



Second level analysis

- Normal law parameters optimized with max. likelihood

▶ **Likelihood formula**

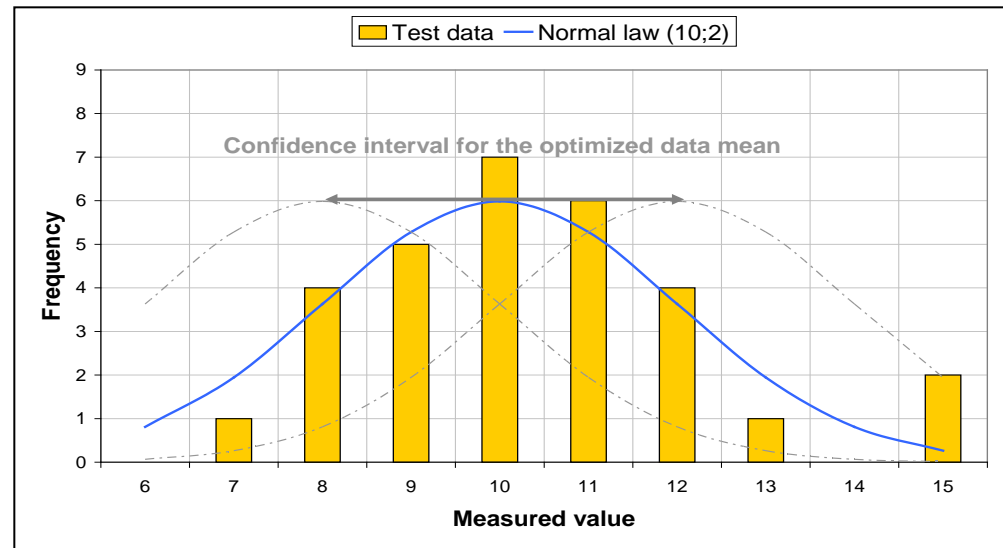
$$L = \prod_{i=1}^n f(x_i, \mu, \sigma) \longrightarrow L_{\max} = \max(L)$$
Maximum likelihood

- The maximum likelihood is also used to define a confidence interval for the normal law parameters

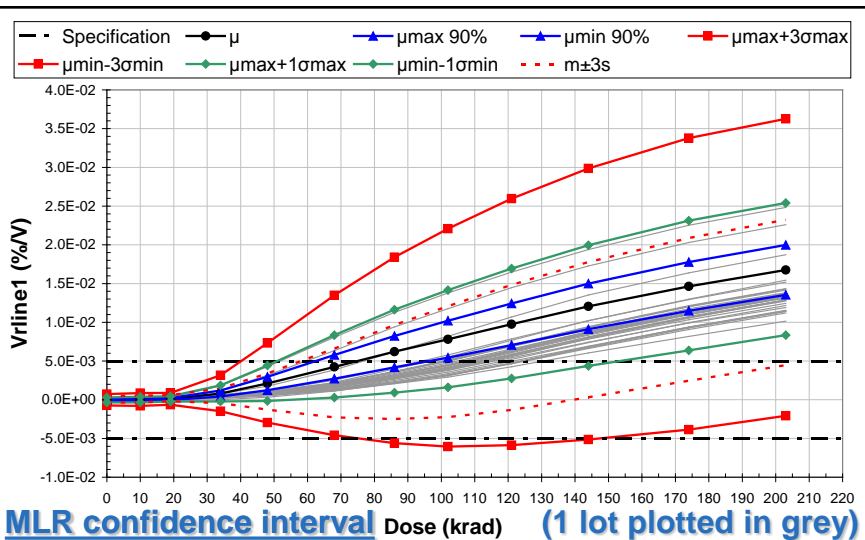
$$\ln\left(\frac{L}{L_{\max}}\right) \geq -\frac{1}{2} \chi^2(1-\alpha, 2)$$

▶ **Confidence interval formula
(maximum likelihood log-ratio)**

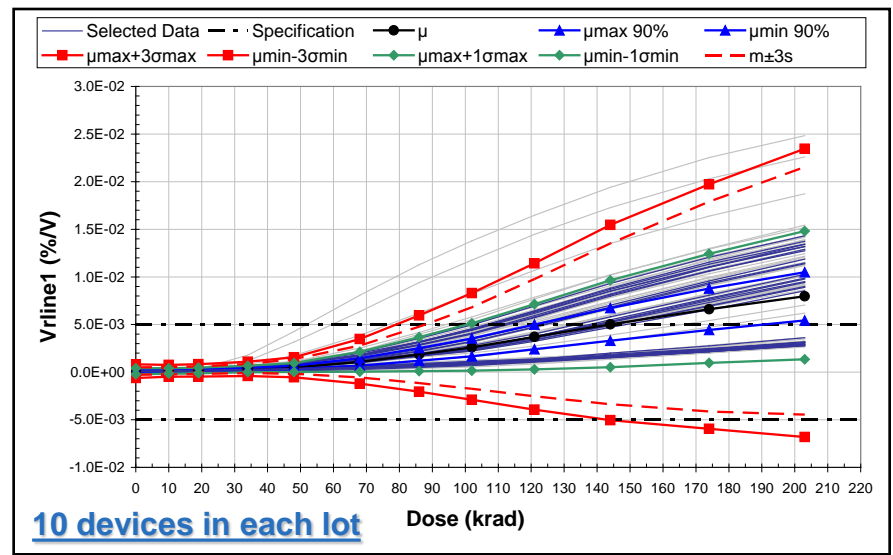
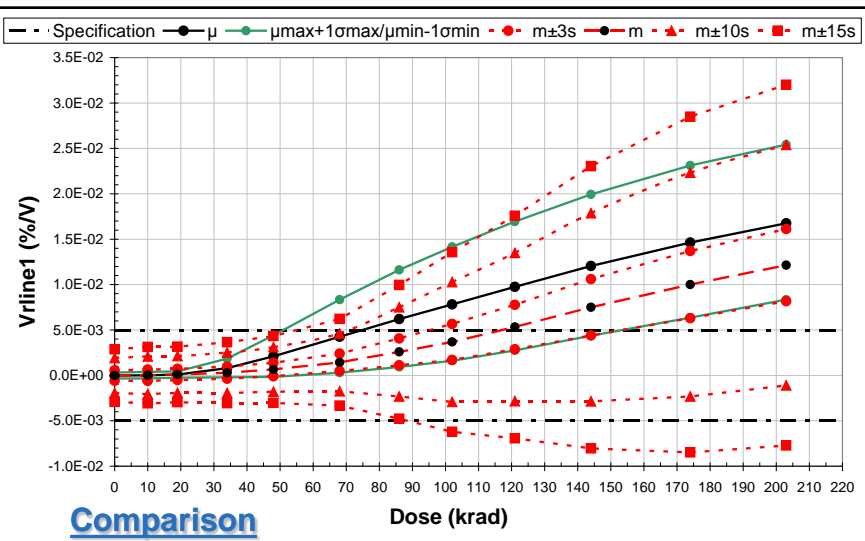
Representation of the normal fit confidence interval calculation (frequency plotted as a function of the measured value for the electrical parameter)



■ **AD584SH Vrline1 (%V) lot 0226A**



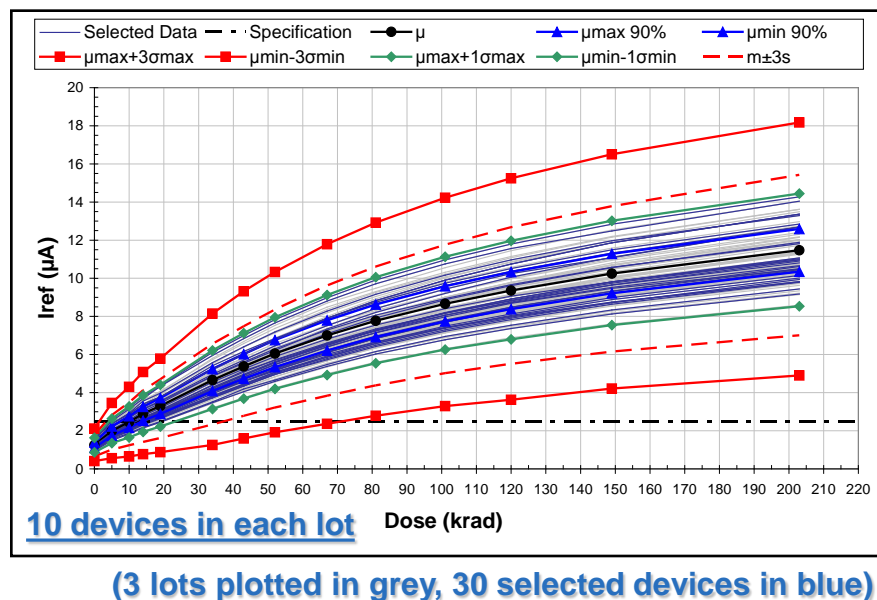
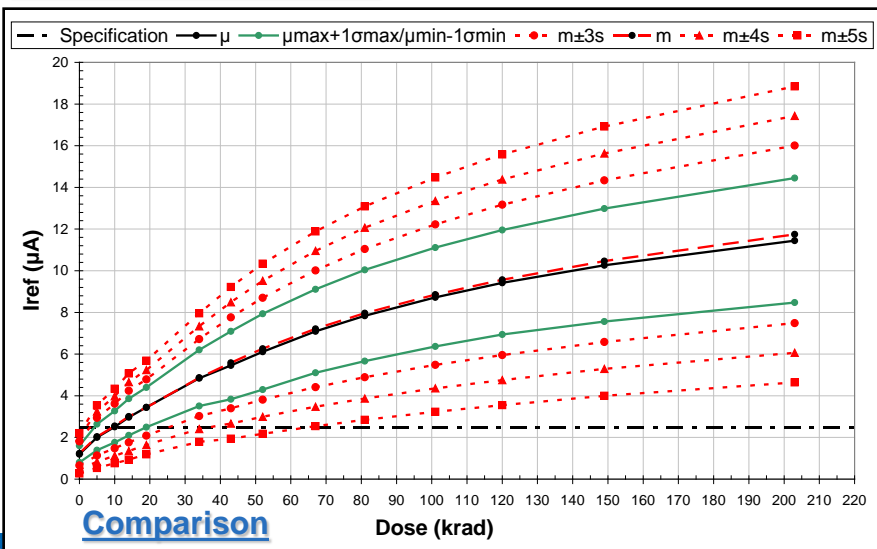
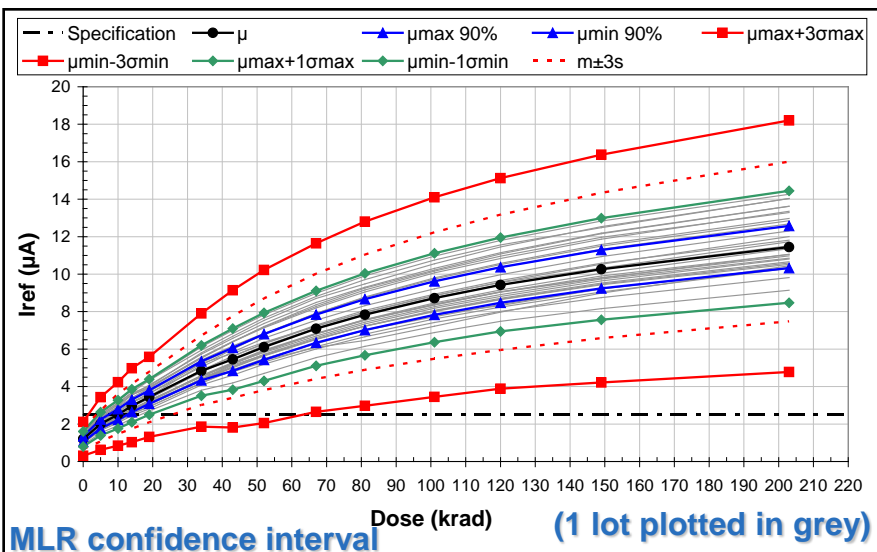
- Max. Likelihood Ratio method with the 30 devices in one lot
- Comparison of MLR confidence interval and 3-sigma calculation with 5 devices
 - Number of sigma to cover the confidence interval delimited by « 90% + 1σ » (green curves)
- MLR method, 10 devices selected in each one of the 3 tested lots
 - To take into account the inter-lot variability



(3 lots plotted in grey, 30 selected devices in blue)

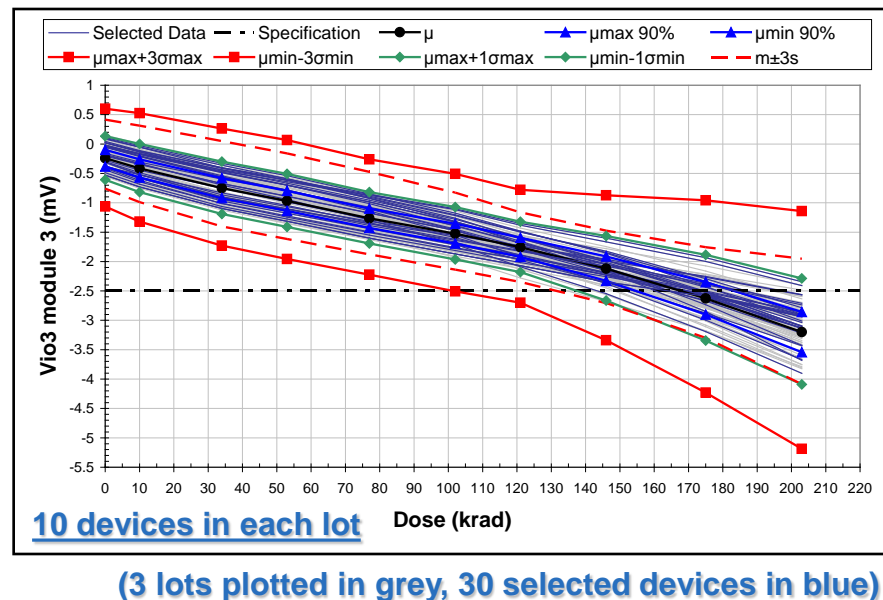
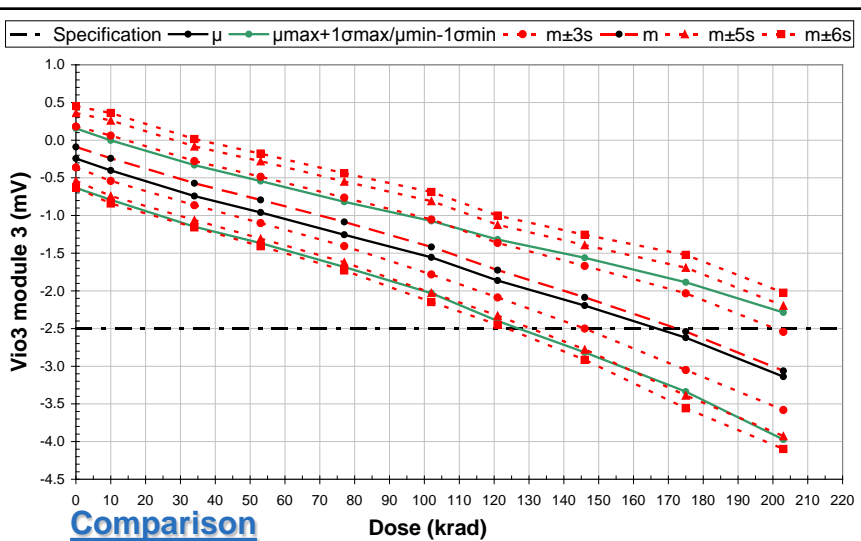
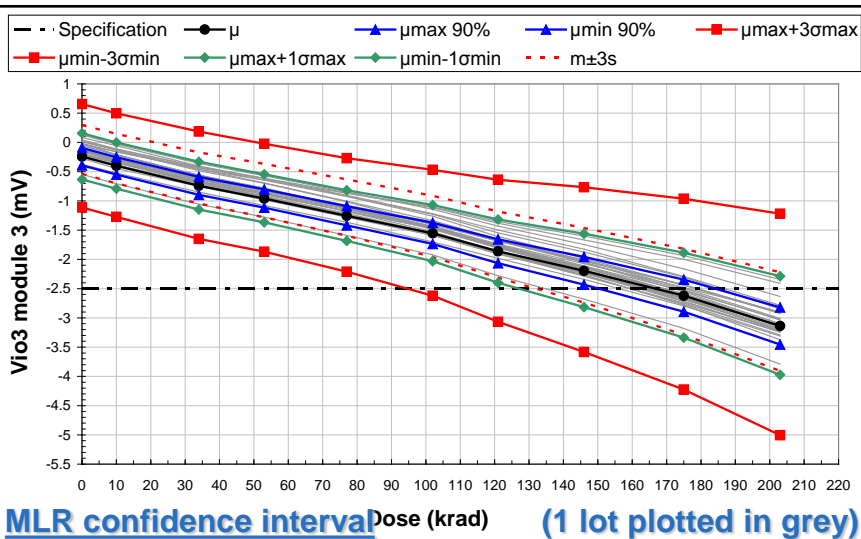
■ **TL1431ACZ Iref (μA) lot GE334152**

- **Max. Likelihood Ratio method with the 30 devices in one lot**
- **Comparison of MLR confidence interval and 3-sigma calculation with 5 devices**
 - Number of sigma to cover the confidence interval delimited by « 90% + 1σ »
- **MLR method, 10 devices selected in each one of the 3 tested lots**
 - To take into account the inter-lot variability



■ **LM124AWG Vio3 module 3 (mV) lot 1136A**

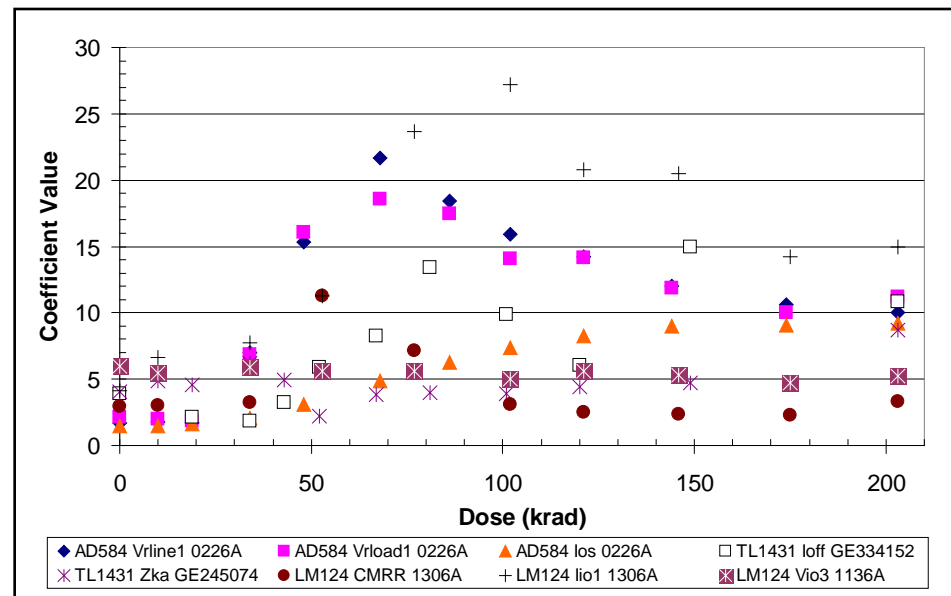
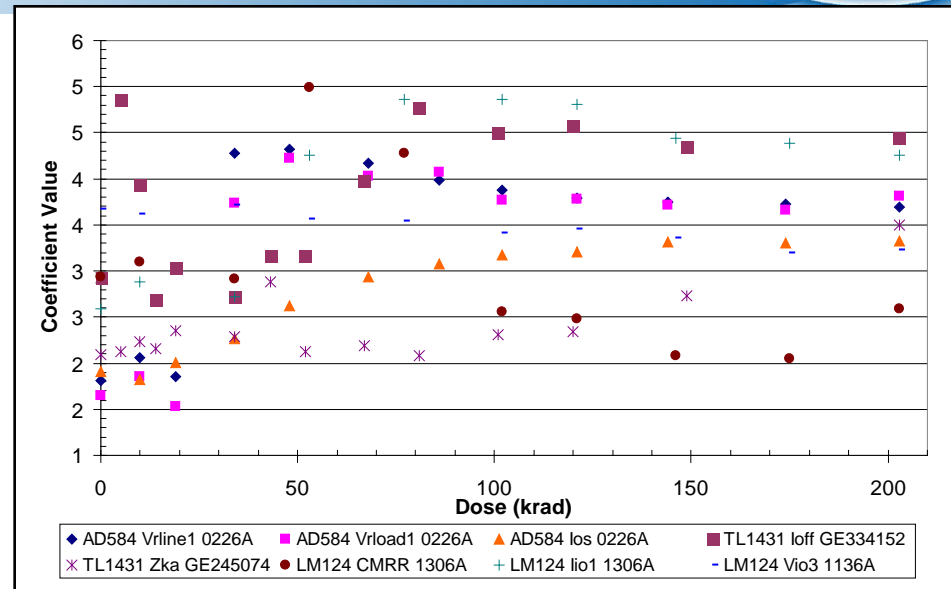
- **Max. Likelihood Ratio method with the 30 devices in one lot**
- **Comparison of MLR confidence interval and 3-sigma calculation with 5 devices**
 - Number of sigma to cover the confidence interval delimited by « 90% + 1σ »
- **MLR method, 10 devices selected in each one of the 3 tested lots**
 - To take into account the inter-lot variability



- **Multiplication factor applied to sigma 's' at each TID step to cover the confidence interval delimited by « 90% + 1σ » from MLR calculation**
 - 30 device lot (top graph)
 - 5 device random selection (bottom graph)

- **Indication of the accuracy with the MLR method corresponding to $K_{TL} = 5$ ($P > 0.999$ for $C = 90$)**

- **The impact of the lot/selection homogeneity in terms of degradation can be observed**
 - **AD584 Vrline1 exhibits atypical devices**
 - Larger margin required to cover the lot behaviour
 - **LM124 Vio3 more homogeneous**
 - Smaller margin required to cover the lot behaviour



- **TID testing was performed on 3 lots for 3 bipolar device references**
 - Analysis of the lot-to-lot and within-one-lot variability

- **Data analysis objectives**
 - Characterize the lot coverage based on 5-device sample size for TID testing
 - Propose and evaluate a Maximum Likelihood Ratio (MLR) method based on the use of confidence intervals

- **MLR is an accurate way to estimate the lot behaviour**
 - Large sample size needed (30 devices)
 - Use of a confidence interval on the mean μ of the electrical parameter measurement

- **Can be applied to data groups composed with different lots**
 - Increase the sample size, better calculation accuracy
 - Takes into account the lot-to-lot variability

- **Perspective**
 - Cost problem related to the large needed sample size
 - Adaptation of the MLR method to smaller sample sizes but keeping similar accuracy

- [1] **MILITARY HANDBOOK, Ionizing Dose and Neutron Hardness Assurance Guidelines for Microcircuits and Semiconductor Devices, MIL-HDBK-814, 08 February 1994.**
- [2] **R. L. Pease, 'Total ionizing dose effects in bipolar devices and circuits', IEEE Transactions on Nuclear Science, vol. 50, no. 3, pp. 539–551, Jun. 2003.**
- [3] **A. Namenson and I. Arimura, 'A Logical Methodology for Determining Electrical End Points for Multi-Lot and Multi-Parameter Data', IEEE Transactions on Nuclear Science, vol. 34, no. 6, pp. 1726–1729, Dec. 1987.**
- [4] **I. Arimura and A. I. Namenson, 'Hardness Assurance Statistical Methodology for Semiconductor Devices', IEEE Transactions on Nuclear Science, vol. 30, no. 6, pp. 4322–4325, Dec. 1983.**
- [5] **R. Ladbury, J. L. Gorelick, and S. S. McClure, 'Statistical Model Selection for TID Hardness Assurance', IEEE Transactions on Nuclear Science, vol. 56, no. 6, pp. 3354–3360, Dec. 2009.**
- [6] **R. Ladbury and J. L. Gorelick, 'Statistical methods for large flight lots and ultra-high reliability applications', IEEE Transactions on Nuclear Science, vol. 52, no. 6, pp. 2630–2637, Dec. 2005.**
- [7] **R. Ladbury, 'Statistical Techniques for Analyzing Process or "Similarity" Data in TID Hardness Assurance', IEEE Transactions on Nuclear Science, vol. 57, no. 6, pp. 3432–3437, Dec. 2010.**
- [8] **R. Ladbury and B. Triggs, 'A Bayesian Approach for Total Ionizing Dose Hardness Assurance', IEEE Transactions on Nuclear Science, vol. 58, no. 6, pp. 3004–3010, Dec. 2011.**
- [9] **R. L. Ladbury and M. J. Campola, 'Bayesian Methods for Bounding Single-Event Related Risk in Low-Cost Satellite Missions', IEEE Transactions on Nuclear Science, vol. 60, no. 6, pp. 4464–4469, Dec. 2013.**
- [10] **'Part-to-part and lot-to-lot variability study of TID effects in bipolar linear devices' ESA study report ref. TRAD/ESA/IR/VAR/NS/241115 of 29/11/2015.**
- [11] **J. Guillermin, N. Sukhaseum 'Part-to-part and lot-to-lot variability study of TID effects in bipolar linear devices', Radecs 2016 Proceedings PC-2**