



# OPEN SOURCE ORBIT DETERMINATION WITH SEMI-ANALYTICAL THEORY

BRYAN CAZABONNE & LUC MAISONOBE





# AGENDA

- Context and target
- DSST presentation
- Mean Elements derivatives
- State Transition Matrices computation
- Short-periodic terms derivatives
- Orbit Determination
- Conclusion



# CONTEXT AND TARGET

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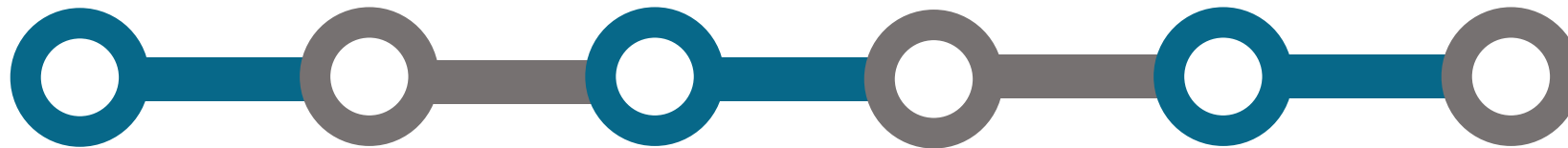
## ● Inception | 2002

Orekit instended  
as a basis for  
ground segments  
bids



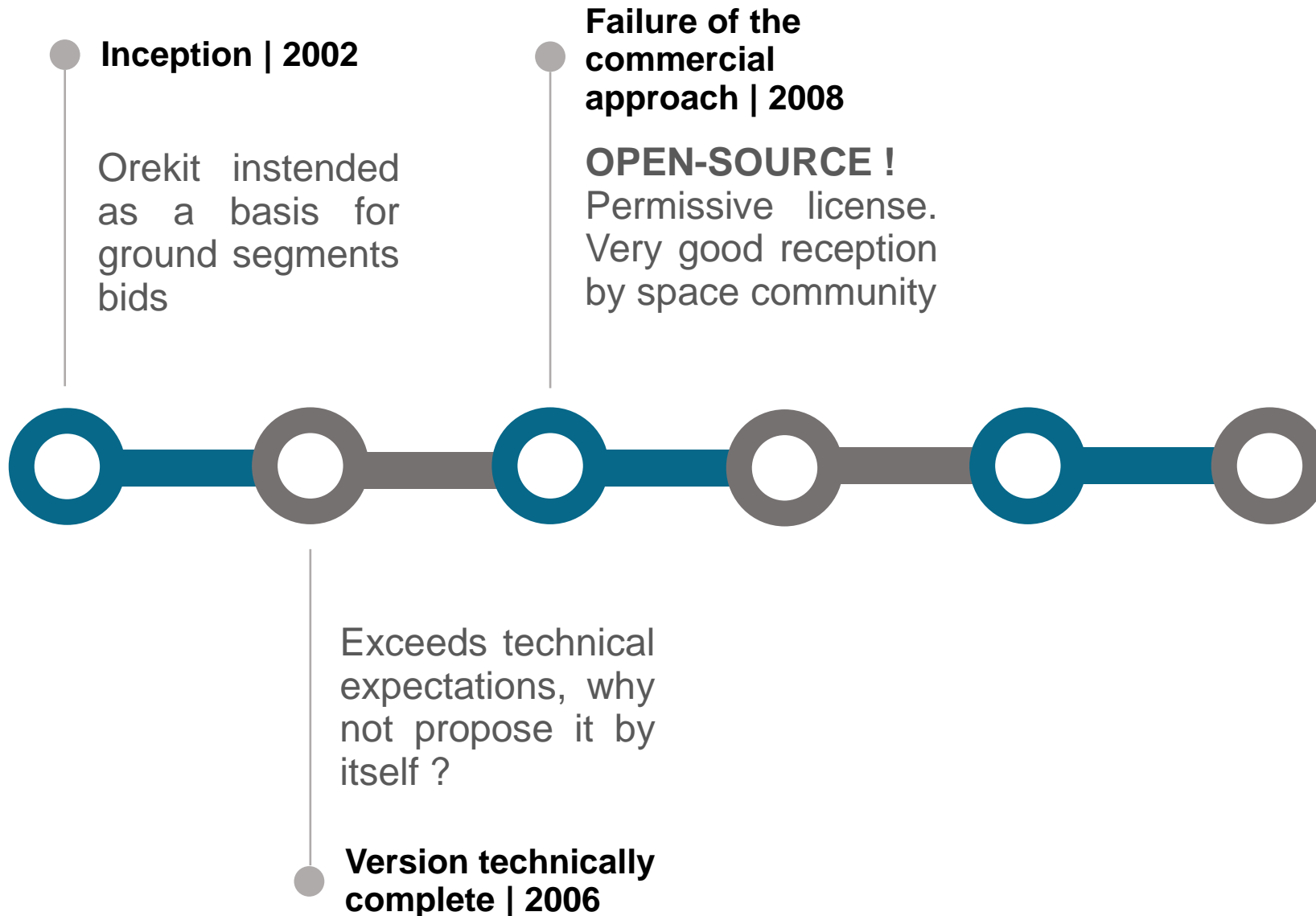
## Inception | 2002

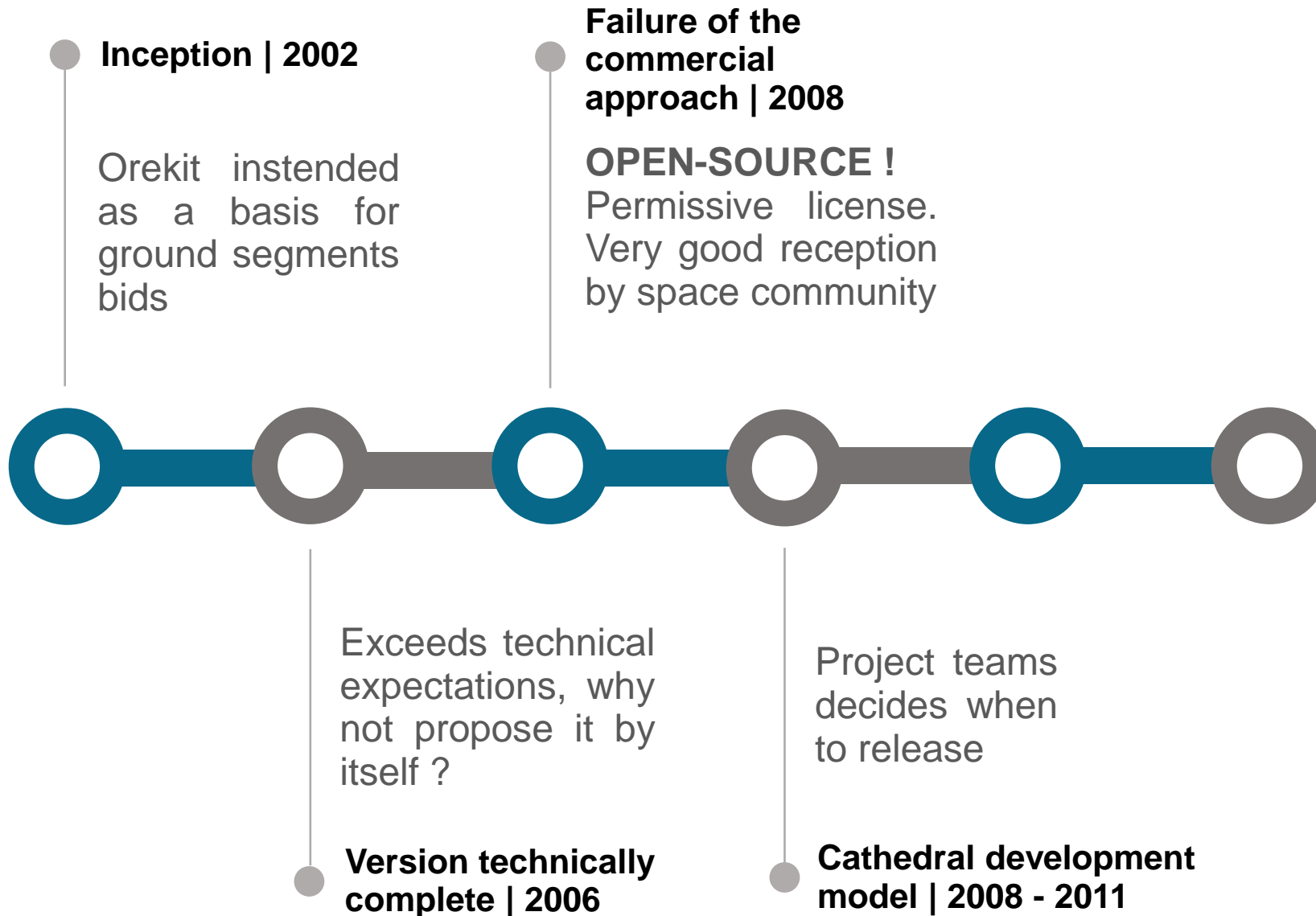
Orekit instended as a basis for ground segments bids

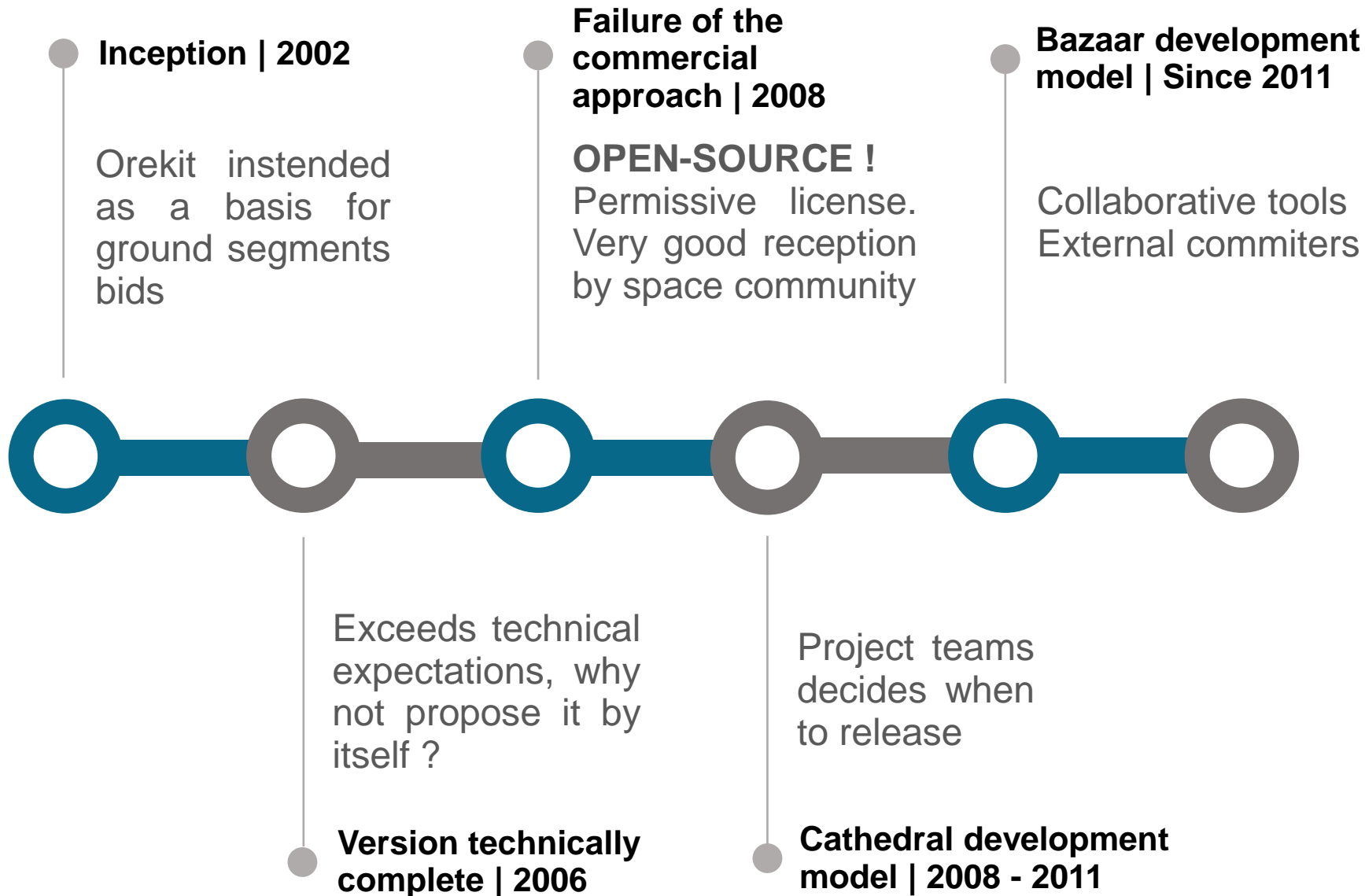


Exceeds technical expectations, why not propose it by itself ?

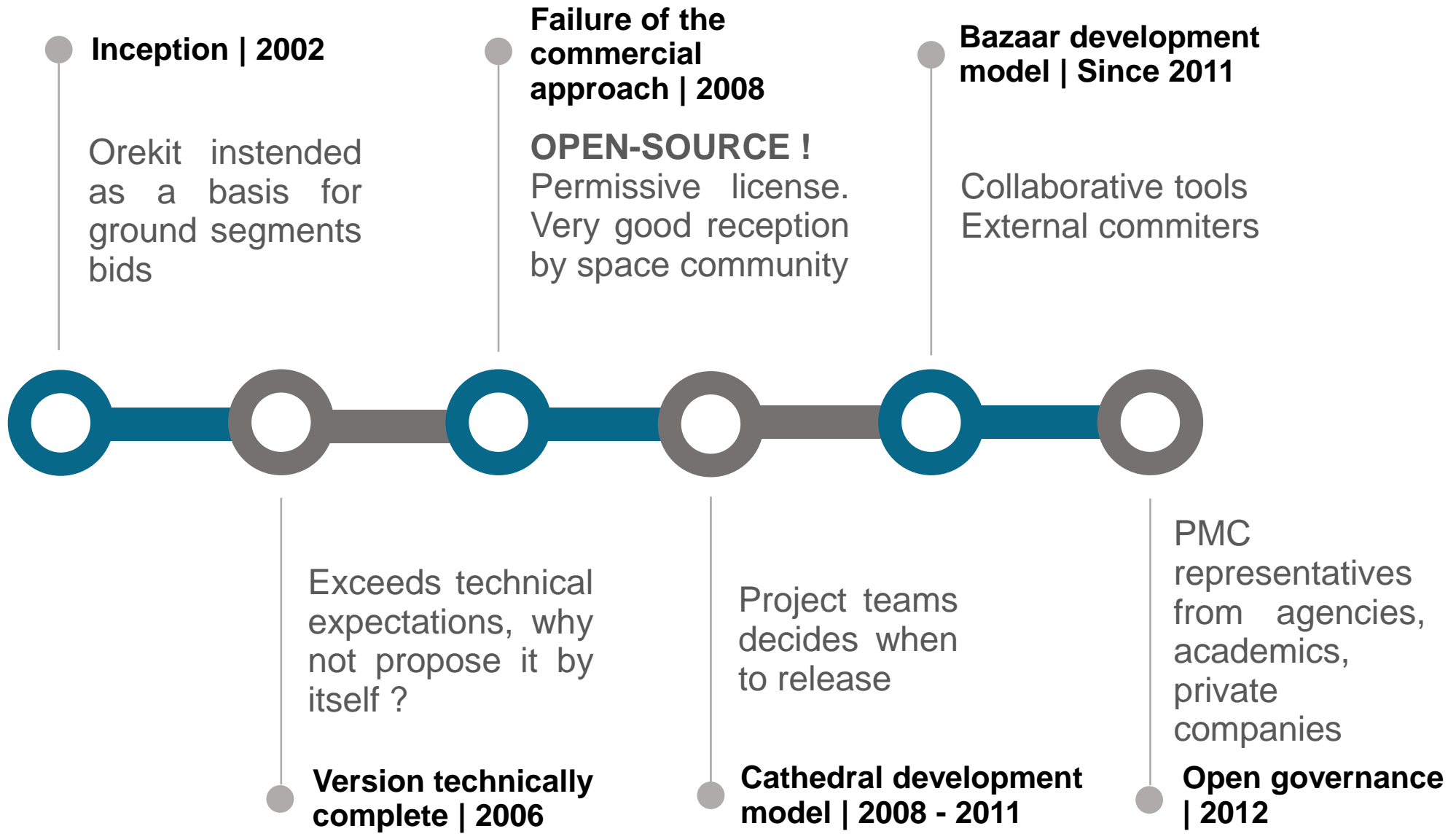
**Version technically complete | 2006**

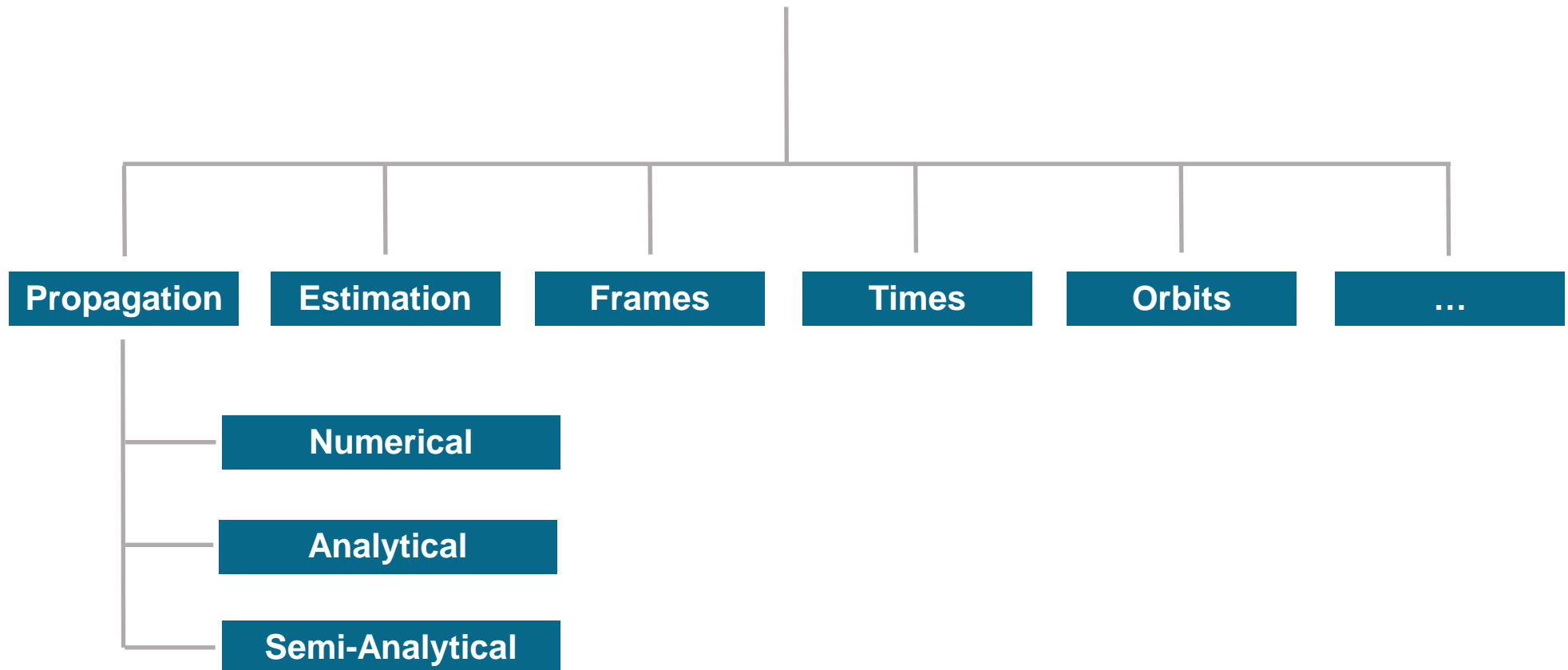


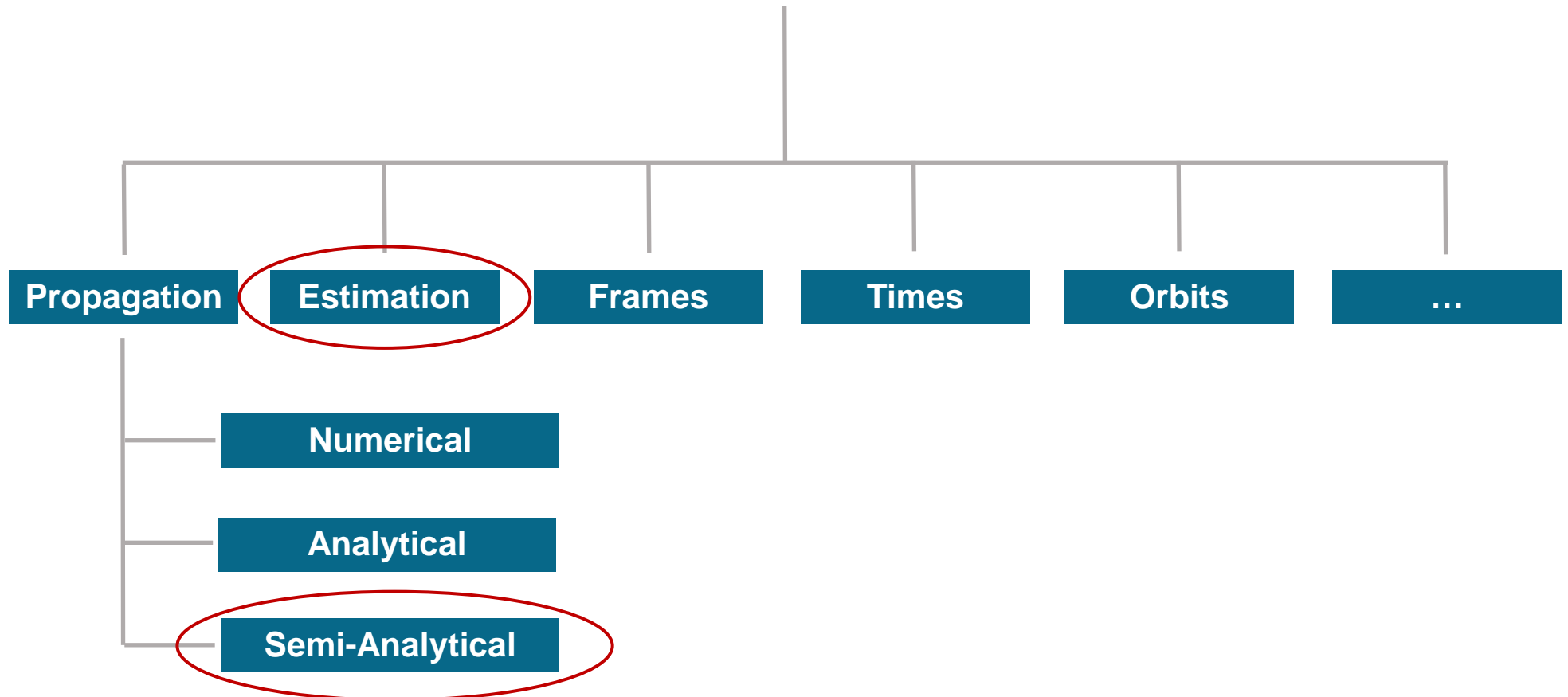












## → Fast Orbit Determination

- Several hundreds of thousands (Setty and al, 2016)

Number of Orbit Determinations performed by the US Joint Space Operation Center per day to maintain their space objects catalog.

➔ Need fast and accurate Orbit Determination

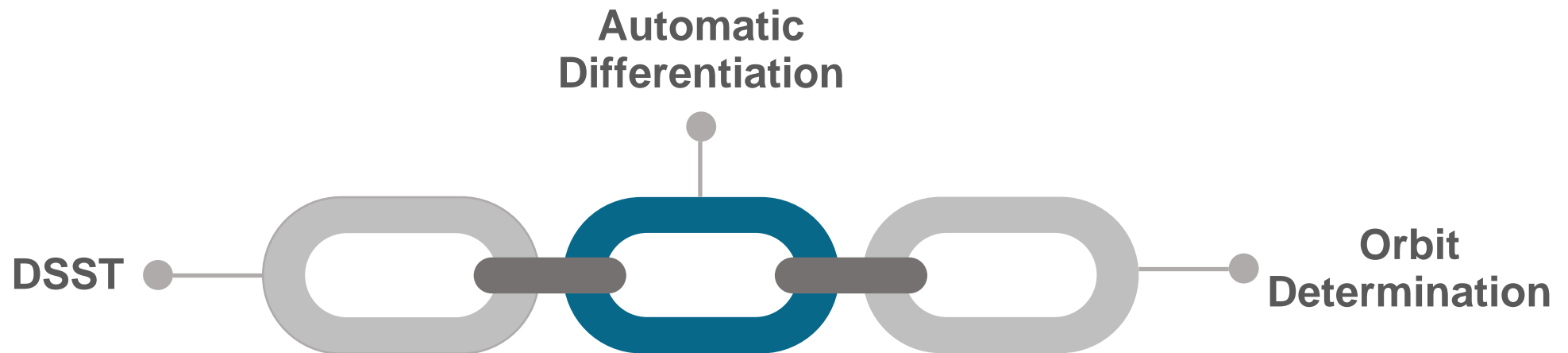
## → Mean Elements Orbit Determination

➔ Station keeping needs

## → Draper Semi-analytical Satellite Theory (DSST)

- **Rapidity** of an analytical propagator
- **Accuracy** of a numerical propagator

## → Target

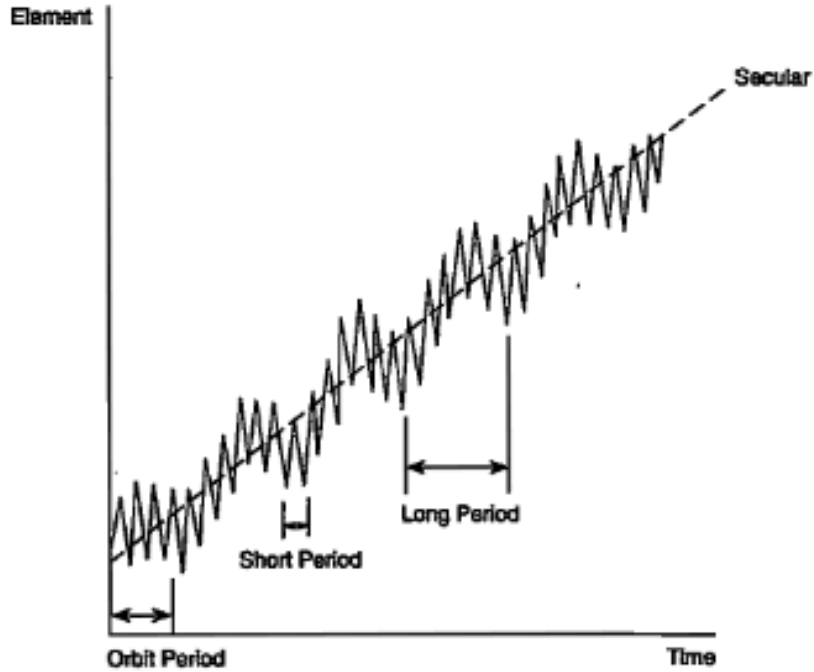




# DSST PRESENTATION

# 2

# ORBITAL PERTURBATIONS



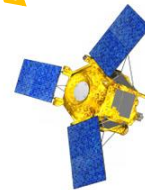
Zonal and Tesseral harmonics of terrestrial potential



Atmospheric drag



Solar radiation pressure



Third body attraction

$$c_i(t) = \overline{c_i(t)} + \sum_{j=1}^N k_{ij} \eta_{ij}(t), \quad i = 1, 2, 3, 4, 5, 6$$



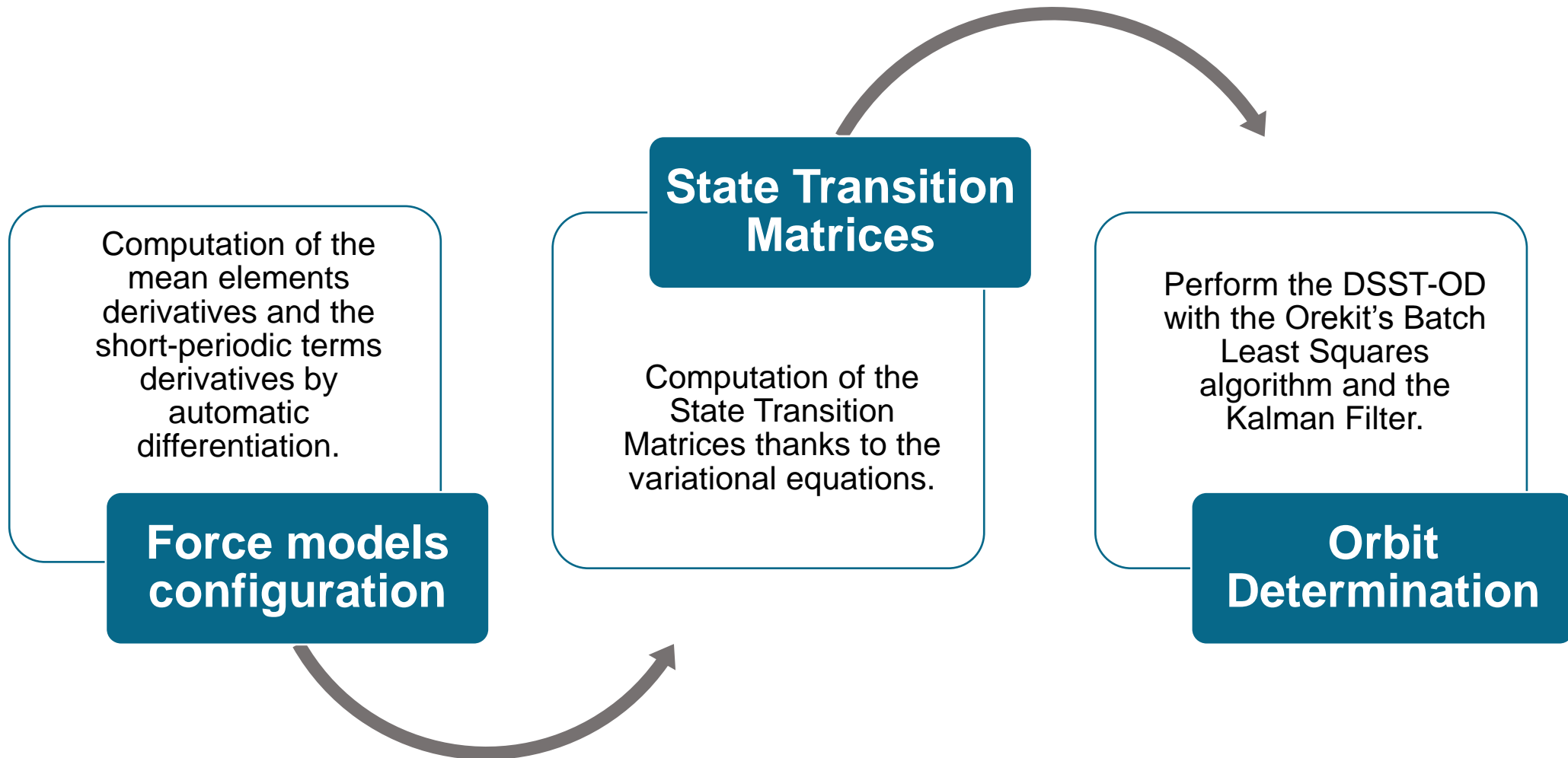
$$c_i(t) = \boxed{\overline{c_i(t)}} + \sum_{j=1}^N k_{ij} \eta_{ij}(t), \quad i = 1, 2, 3, 4, 5, 6$$

Mean Elements

$$c_i(t) = \overline{c_i(t)} + \sum_{j=1}^N k_{ij} \eta_{ij}(t), \quad i = 1, 2, 3, 4, 5, 6$$

Mean Elements

Short-periodic terms





# MEAN ELEMENTS DERIVATIVES

# 3

## → GOAL

$$\left[ Y_i \quad \frac{\partial Y_i}{\partial Y_1} \quad \frac{\partial Y_i}{\partial Y_2} \quad \dots \quad \frac{\partial Y_i}{\partial Y_6} \quad \frac{\partial Y_i}{\partial P_1} \quad \dots \quad \frac{\partial Y_i}{\partial P_N} \right]$$

- $Y_i$ : Orbital element
- $P_k$ : Force model parameter
- $N$ : The number of force model parameters taken into account for the Orbit Determination

## → GAIN

- Safer implementation
- Simpler validation

- ➔ Each DSST-specific force model on Orekit has a method allowing the computation of the mean elements rates.

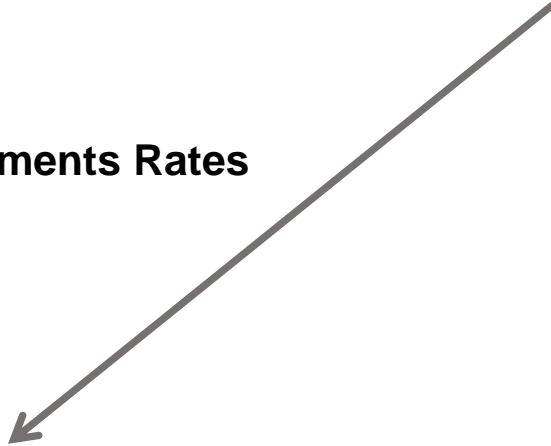
$$\mathbf{Y} = [\mathbf{a} \ \mathbf{h} \ \mathbf{k} \ \mathbf{p} \ \mathbf{q} \ \lambda] \longrightarrow \dot{\mathbf{Y}} = \begin{bmatrix} \dot{\mathbf{a}} \\ \dot{\mathbf{h}} \\ \dot{\mathbf{k}} \\ \dot{\mathbf{p}} \\ \dot{\mathbf{q}} \\ \dot{\lambda} \end{bmatrix}$$

- ➔ Method implemented for the states based on the real numbers ✓
- ➔ Need to be implemented to provide the Jacobians of the mean elements rates by automatic differentiation.

$$\mathbf{Y} = [\mathbf{a} \ \mathbf{h} \ \mathbf{k} \ \mathbf{p} \ \mathbf{q} \ \boldsymbol{\lambda}]$$

$$\mathbf{Y} = [a \ h \ k \ p \ q \ \lambda]$$

Mean Elements Rates

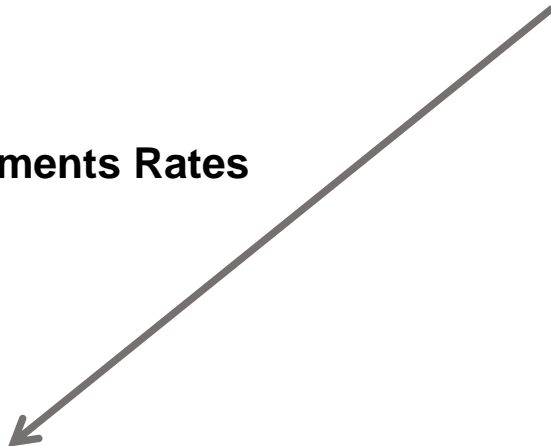


$$\dot{\mathbf{Y}} = \begin{bmatrix} \dot{a} \\ \dot{h} \\ \dot{k} \\ \dot{p} \\ \dot{q} \\ \dot{\lambda} \end{bmatrix}$$



$$\mathbf{Y} = [\mathbf{a} \ \mathbf{h} \ \mathbf{k} \ \mathbf{p} \ \mathbf{q} \ \lambda]$$

Mean Elements Rates



$$\dot{\mathbf{Y}} = \begin{bmatrix} \dot{\mathbf{a}} \\ \dot{\mathbf{h}} \\ \dot{\mathbf{k}} \\ \dot{\mathbf{p}} \\ \dot{\mathbf{q}} \\ \dot{\lambda} \end{bmatrix} \xrightarrow{\text{Automatic Differentiation}} \dot{\mathbf{Y}}' = \begin{bmatrix} \dot{\mathbf{a}} & \partial_{\mathbf{a}} \dot{\mathbf{a}} & \partial_{\mathbf{h}} \dot{\mathbf{a}} & \dots & \partial_{\lambda} \dot{\mathbf{a}} & \partial_{\mathbf{P}_1} \dot{\mathbf{a}} & \dots & \partial_{\mathbf{P}_N} \dot{\mathbf{a}} \\ \dot{\mathbf{h}} & \partial_{\mathbf{a}} \dot{\mathbf{h}} & \partial_{\mathbf{h}} \dot{\mathbf{h}} & \dots & \partial_{\lambda} \dot{\mathbf{h}} & \partial_{\mathbf{P}_1} \dot{\mathbf{h}} & \dots & \partial_{\mathbf{P}_N} \dot{\mathbf{h}} \\ \vdots & \vdots & \vdots & & \vdots & \vdots & & \vdots \\ \dot{\lambda} & \partial_{\mathbf{a}} \dot{\lambda} & \partial_{\mathbf{h}} \dot{\lambda} & \dots & \partial_{\lambda} \dot{\lambda} & \partial_{\mathbf{P}_1} \dot{\lambda} & \dots & \partial_{\mathbf{P}_N} \dot{\lambda} \end{bmatrix}$$



# STATE TRANSITION MATRICES COMPUTATION

# 4

$$\dot{Y}' = \begin{bmatrix} \dot{a} & \partial_a \dot{a} & \partial_h \dot{a} & \dots & \partial_\lambda \dot{a} & \partial_{P_1} \dot{a} & \dots & \partial_{P_N} \dot{a} \\ \dot{h} & \partial_a \dot{h} & \partial_h \dot{h} & \dots & \partial_\lambda \dot{h} & \partial_{P_1} \dot{h} & \dots & \partial_{P_N} \dot{h} \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \dot{\lambda} & \partial_a \dot{\lambda} & \partial_h \dot{\lambda} & \dots & \partial_\lambda \dot{\lambda} & \partial_{P_1} \dot{\lambda} & \dots & \partial_{P_N} \dot{\lambda} \end{bmatrix}$$

$$\dot{Y}' = \begin{bmatrix} \dot{a} & \partial_a \dot{a} & \partial_h \dot{a} & \dots & \partial_\lambda \dot{a} & \partial_{P_1} \dot{a} & \dots & \partial_{P_N} \dot{a} \\ \dot{h} & \partial_a \dot{h} & \partial_h \dot{h} & \dots & \partial_\lambda \dot{h} & \partial_{P_1} \dot{h} & \dots & \partial_{P_N} \dot{h} \\ \vdots & \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \dot{\lambda} & \partial_a \dot{\lambda} & \partial_h \dot{\lambda} & \dots & \partial_\lambda \dot{\lambda} & \partial_{P_1} \dot{\lambda} & \dots & \partial_{P_N} \dot{\lambda} \end{bmatrix}$$

↓

$$\dot{Y}$$

$$\dot{Y}' = \begin{bmatrix} \dot{a} \\ \dot{h} \\ \vdots \\ \dot{\lambda} \end{bmatrix} \begin{bmatrix} \partial_a \dot{a} & \partial_h \dot{a} & \dots & \partial_\lambda \dot{a} & \partial_{P_1} \dot{a} & \dots & \partial_{P_N} \dot{a} \\ \partial_a \dot{h} & \partial_h \dot{h} & \dots & \partial_\lambda \dot{h} & \partial_{P_1} \dot{h} & \dots & \partial_{P_N} \dot{h} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \partial_a \dot{\lambda} & \partial_h \dot{\lambda} & \dots & \partial_\lambda \dot{\lambda} & \partial_{P_1} \dot{\lambda} & \dots & \partial_{P_N} \dot{\lambda} \end{bmatrix}$$

$\swarrow$   $\dot{Y}$

$\searrow$   $\frac{\partial \dot{Y}}{\partial Y}$

$$\dot{Y}' = \begin{bmatrix} \dot{a} \\ \dot{h} \\ \vdots \\ \dot{\lambda} \end{bmatrix} \begin{bmatrix} \partial_a \dot{a} & \partial_h \dot{a} & \dots & \partial_\lambda \dot{a} & \partial_{P_1} \dot{a} & \dots & \partial_{P_N} \dot{a} \\ \partial_a \dot{h} & \partial_h \dot{h} & \dots & \partial_\lambda \dot{h} & \partial_{P_1} \dot{h} & \dots & \partial_{P_N} \dot{h} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \partial_a \dot{\lambda} & \partial_h \dot{\lambda} & \dots & \partial_\lambda \dot{\lambda} & \partial_{P_1} \dot{\lambda} & \dots & \partial_{P_N} \dot{\lambda} \end{bmatrix}$$

Diagram illustrating the Jacobian of mean elements rates. The Jacobian matrix is shown as a product of a vector of mean elements rates and a matrix of partial derivatives. The vector of mean elements rates is  $\dot{Y}' = [\dot{a}, \dot{h}, \dots, \dot{\lambda}]^T$ . The matrix of partial derivatives is  $\begin{bmatrix} \partial_a \dot{a} & \partial_h \dot{a} & \dots & \partial_\lambda \dot{a} & \partial_{P_1} \dot{a} & \dots & \partial_{P_N} \dot{a} \\ \partial_a \dot{h} & \partial_h \dot{h} & \dots & \partial_\lambda \dot{h} & \partial_{P_1} \dot{h} & \dots & \partial_{P_N} \dot{h} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \ddots & \vdots \\ \partial_a \dot{\lambda} & \partial_h \dot{\lambda} & \dots & \partial_\lambda \dot{\lambda} & \partial_{P_1} \dot{\lambda} & \dots & \partial_{P_N} \dot{\lambda} \end{bmatrix}$ . Arrows indicate the relationship between the Jacobian and the mean elements rates  $\dot{Y}$ , the partial derivative of the mean elements rates with respect to the mean elements  $\frac{\partial \dot{Y}}{\partial Y}$ , and the partial derivative of the mean elements rates with respect to the parameters  $\frac{\partial \dot{Y}}{\partial P}$ .

$$\frac{d\left(\frac{\partial Y}{\partial Y_0}\right)}{dt} = \frac{\partial \dot{Y}}{\partial Y} \times \frac{\partial Y}{\partial Y_0}$$

$$\frac{d\left(\frac{\partial Y}{\partial P}\right)}{dt} = \frac{\partial \dot{Y}}{\partial Y} \times \frac{\partial Y}{\partial P} + \frac{\partial \dot{Y}}{\partial P}$$

→ Computation of  $\frac{\partial Y}{\partial Y_0}$  and  $\frac{\partial Y}{\partial P}$  matrices by finite differences and comparison to those previously obtained.



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**Problem : Different matrices !**

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## **Problem : Different matrices !**

- Newtonian Attraction derivatives were not taken into account in the computation of the state transition matrices.
- Some dependencies to the central attraction coefficient were implicit and therefore not differentiated.

- Computation of  $\frac{\partial Y}{\partial Y_0}$  and  $\frac{\partial Y}{\partial P}$  matrices by finite differences and comparison to those previously obtained.

## **Problem : Different matrices !**

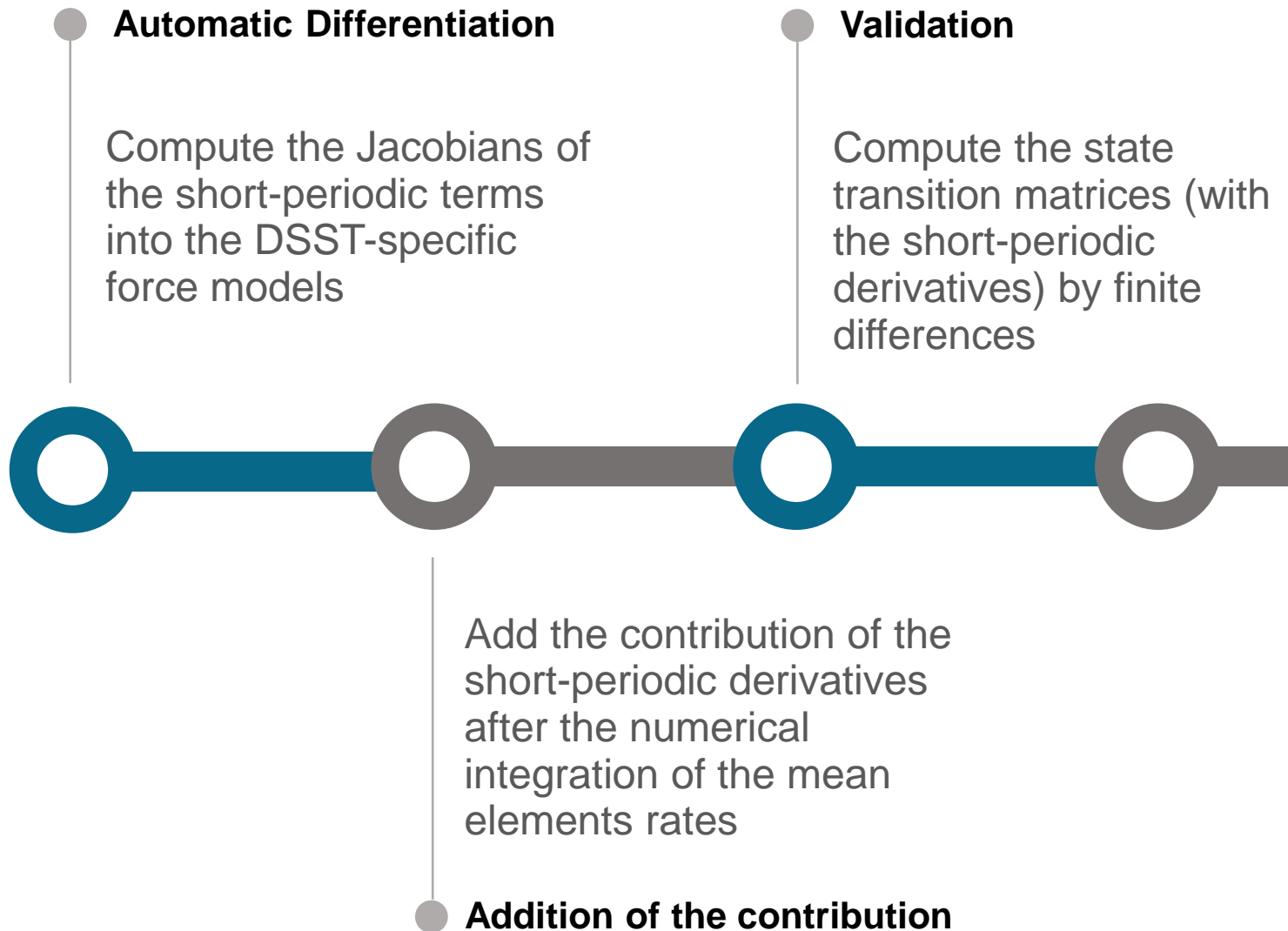
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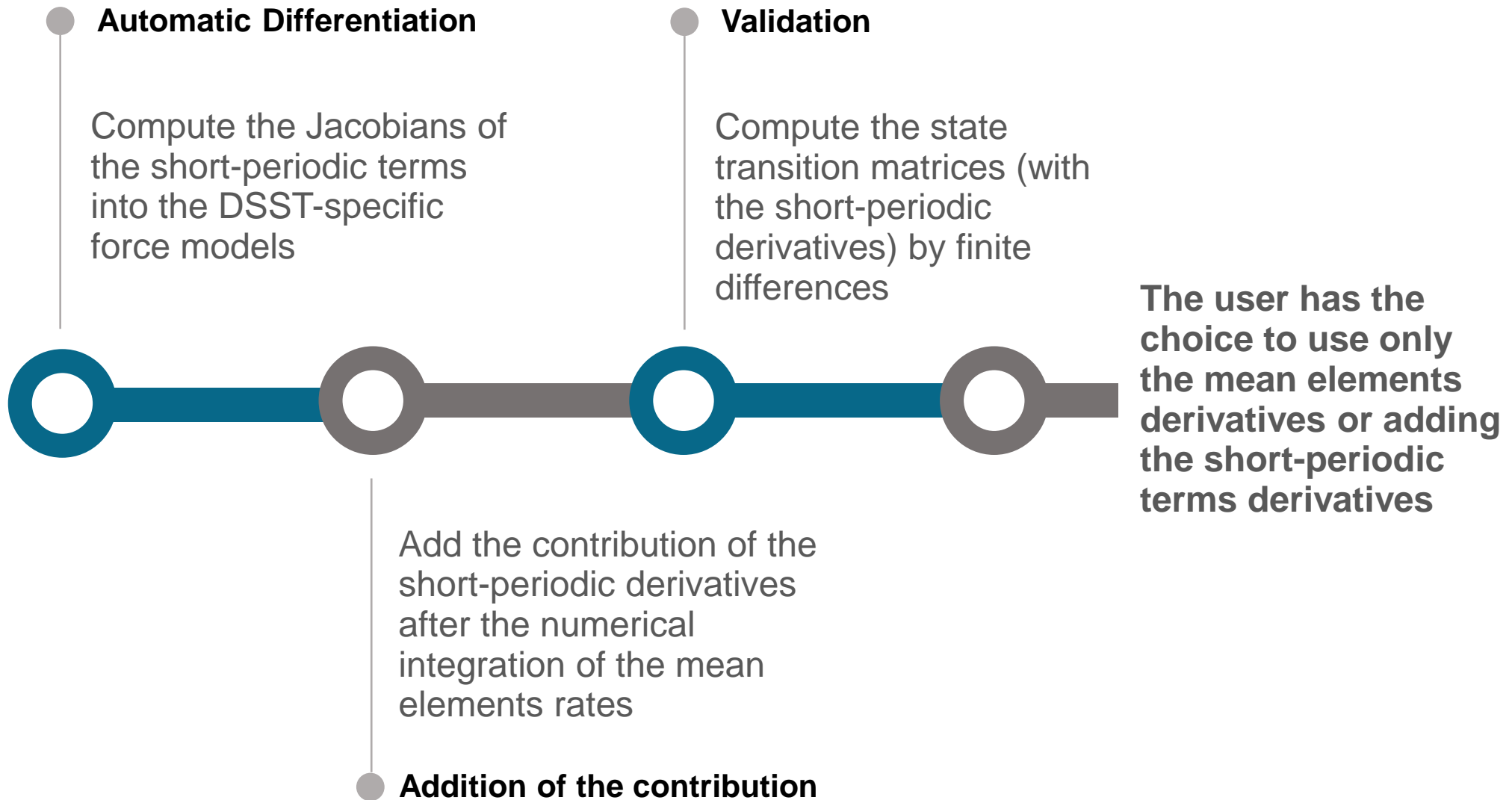
**Problem solved ✓**



# SHORT-PERIODIC TERMS DERIVATIVES

5







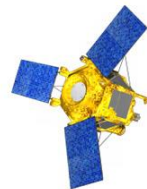
# ORBIT DETERMINATION

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## Lageos 2

Zonal and Tesseral harmonics  
of terrestrial potential

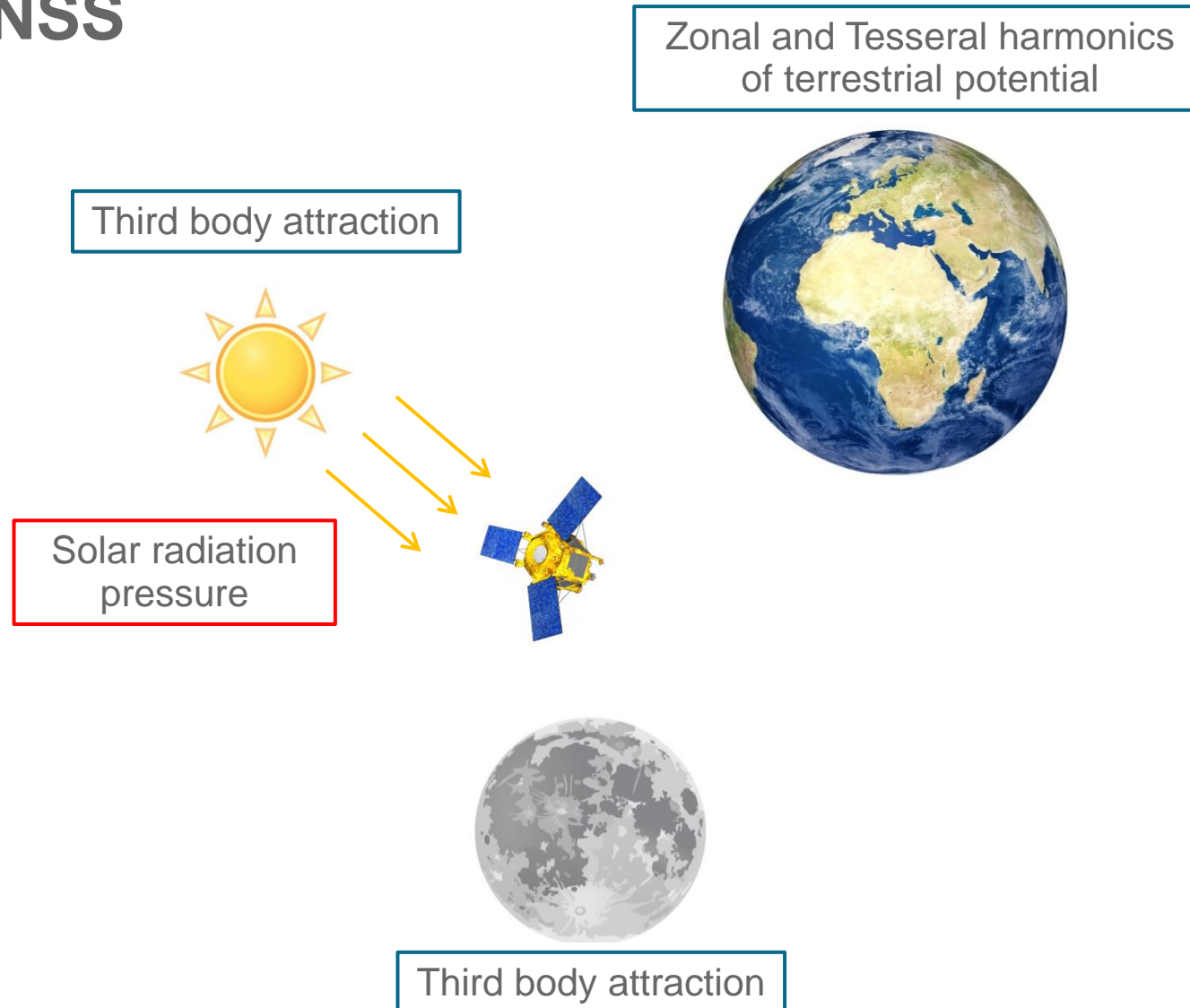
Third body attraction



Third body attraction



## GNSS



## DSST

Minimum step (s)	6000
Maximum step (s)	86400
Tolerance (m)	10



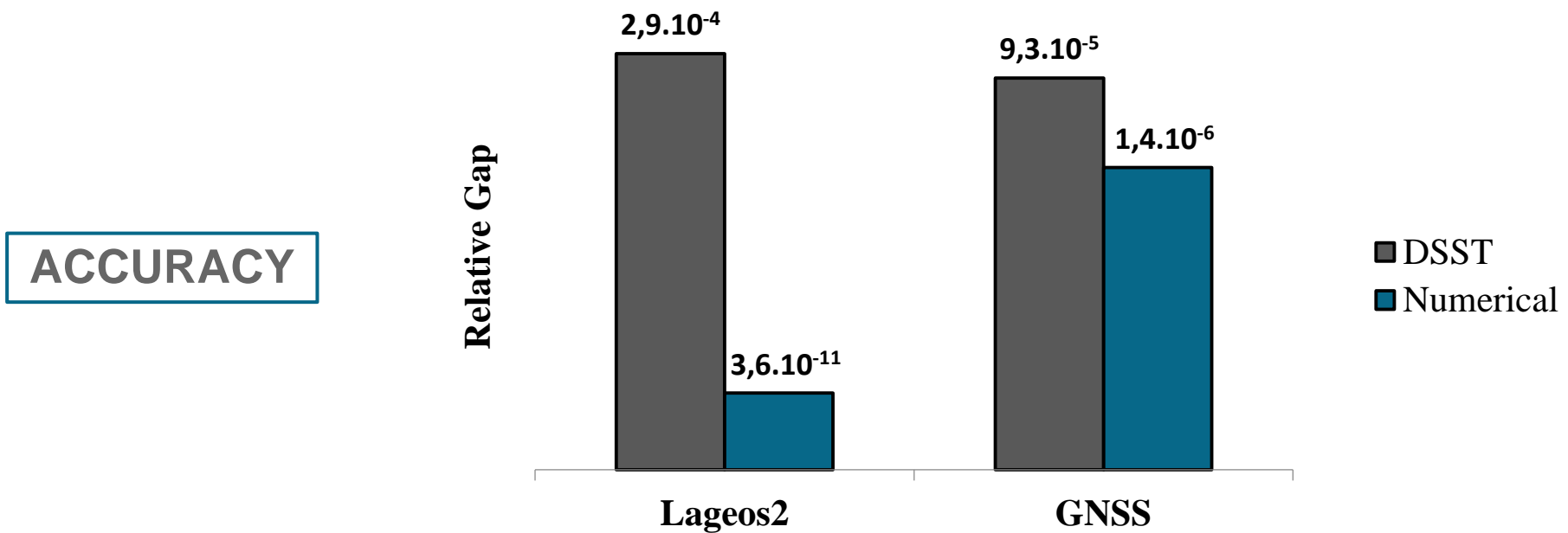
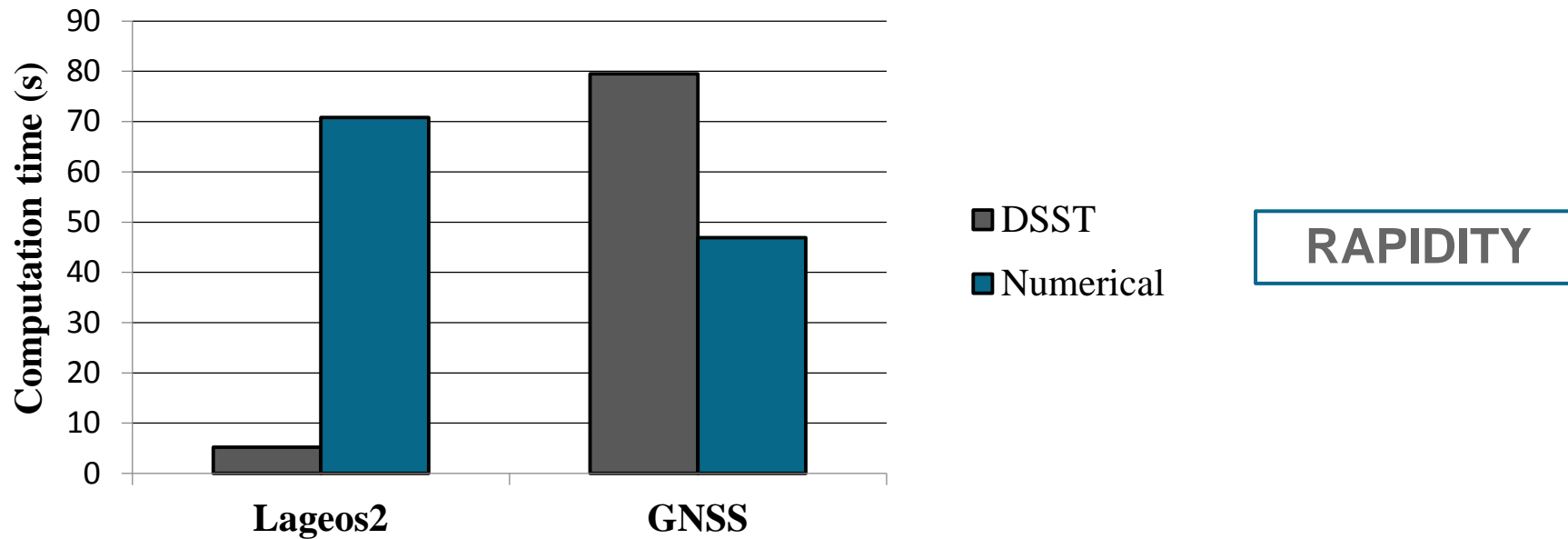
## Numerical

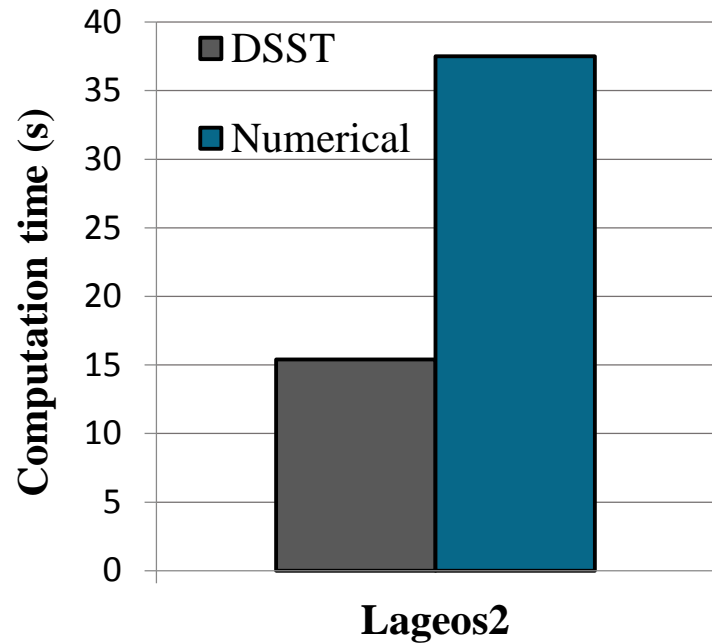
Minimum step (s)	0,001
Maximum step (s)	300
Tolerance (m)	10

➔ The DSST has **significant advantage** compared to the numerical propagator for the integration step. This because the elements computed numerically by the DSST are the mean elements.

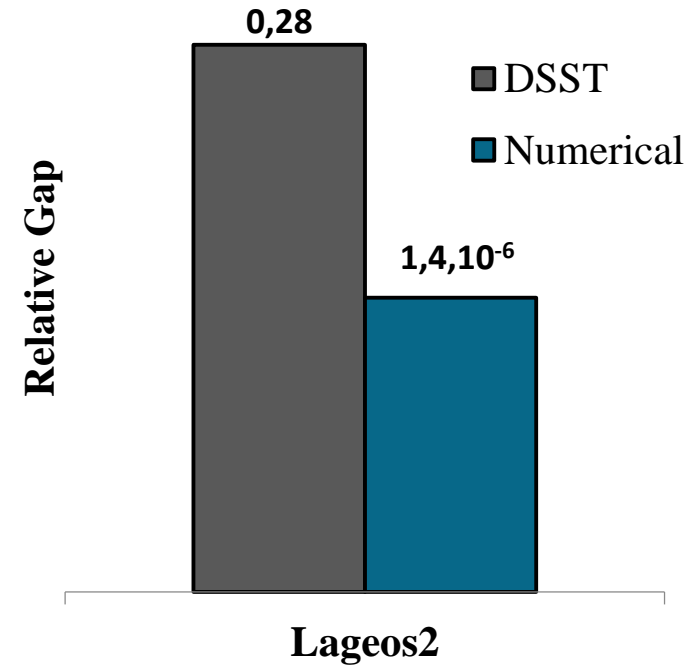
Case	Zonal	Tesseral	Third Body
1	×	×	×
2	✓	×	×
3	✓	✓	×
4	✓	✓	✓

- ➔ Gradual addition of the short-periodic terms derivatives to highlight the main contributions .
- ➔ Performed tests for Lageos2 Orbit Determination.

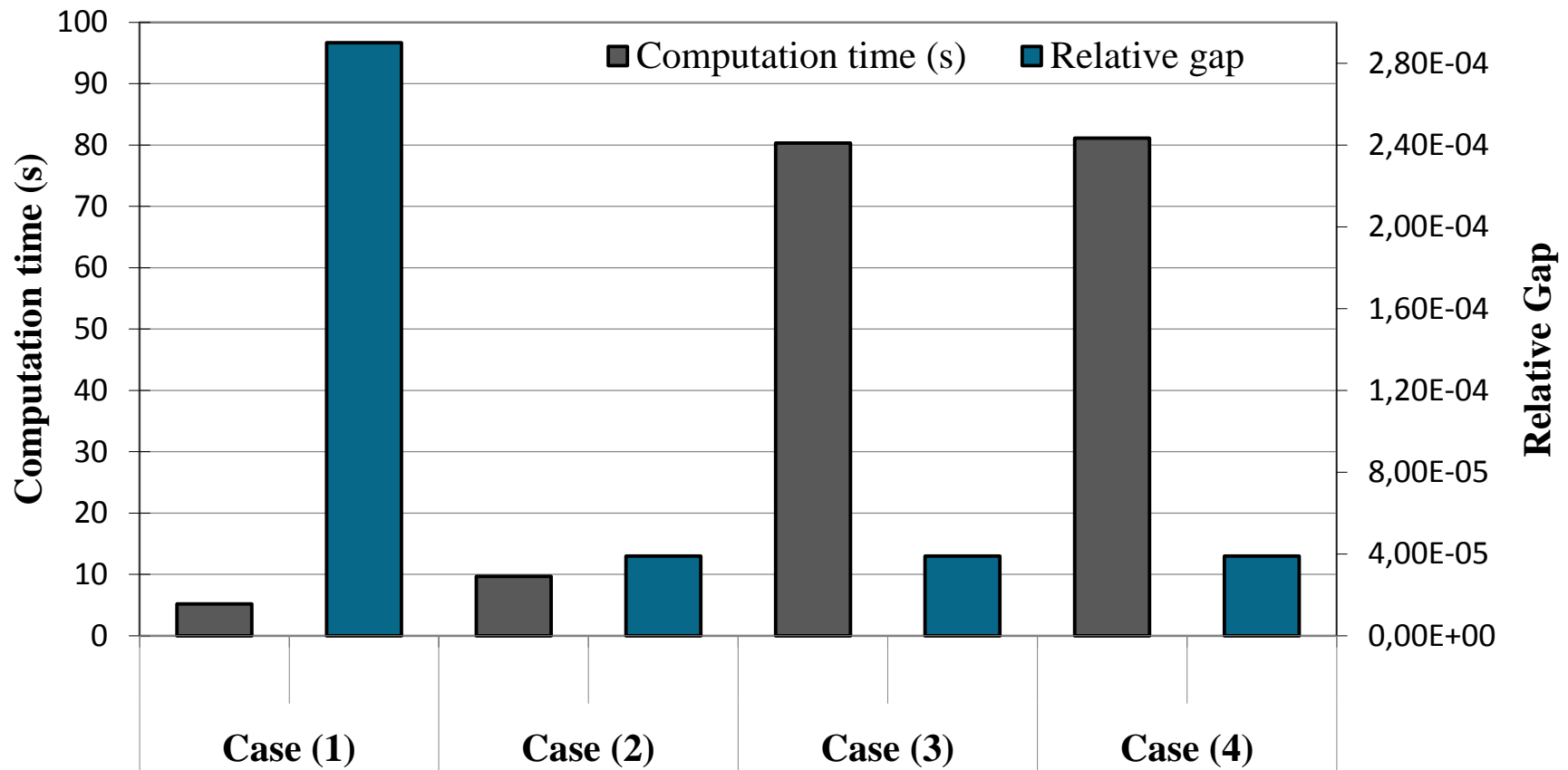


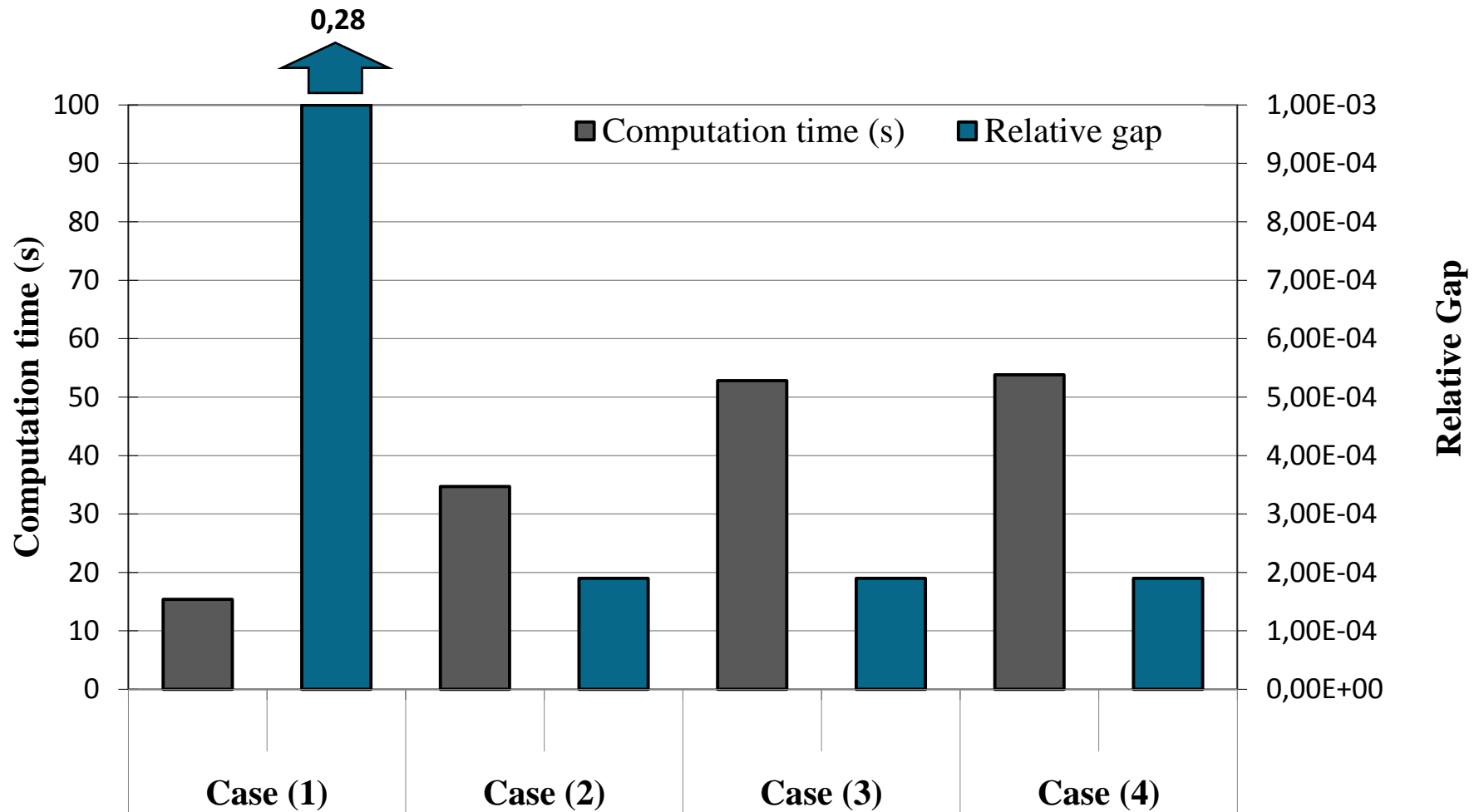


**RAPIDITY**



**ACCURACY**







# CONCLUSION

# 5



**DSST**

Need access to « optimal »  
values for force models  
initialization



**DSST**

Need access to « optimal »  
values for force models  
initialization

Need to optimize critical  
computation steps.

**DSST**

Need access to « optimal » values for force models initialization.

Need to optimize critical computation steps.

**DSST**

Improve the Kalman Filter Orbit Determination with the DSST.



**Thank you for your attention**