

# Controlled Reentry Analysis of LEO Satellites at EOL

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Introduction to controlled re-entry

## I) Mission design

- a. Orbit and spacecraft
- b. Mission overview

## II) Propulsion systems (HET, Arcjet, Monopropellant)

- a. Main features
- b. Assumptions

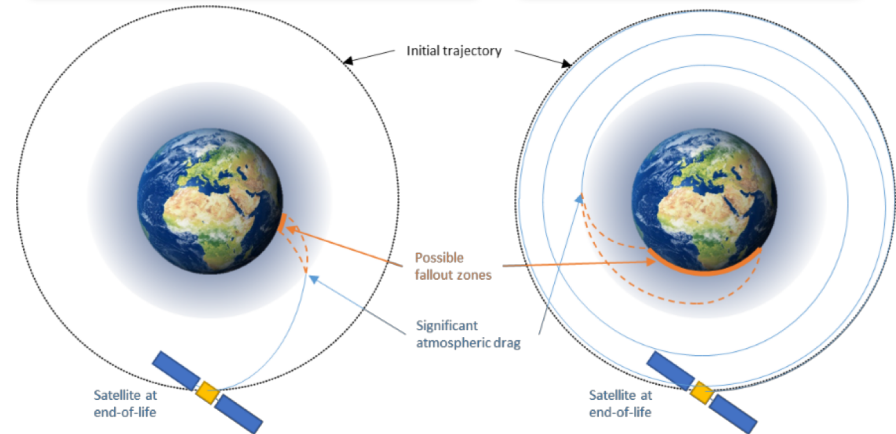
## III) Trade-off

- a. Constraints and ranking criteria
- b. Results

Conclusions

# Introduction

- **Space Debris** is a growing concern
- One objective of **CleanSat** aims to ensure satellites to leave protected regions at End-of-Life
- **Possible hazard of parts surviving re-entry => must ensure low casualty risk (<1/10 000)**
  - Uncontrolled re-entry: no control
  - Semi-controlled re-entry: fallout within one orbital period
  - Controlled re-entry: greater control over fallout zone
- **Controlled re-entry conditions**
  - Medium/big satellites
  - Steeper re-entry into the atmosphere => high thrust for 1 single final burn
  - Heavier, more complex systems



*Trajectories and fallout zones in case of a controlled (left) or semi-controlled (right) re-entry*

# I) Mission Design: a) Orbit and spacecraft

- **Orbit**

Target crowded regions with high probability collision

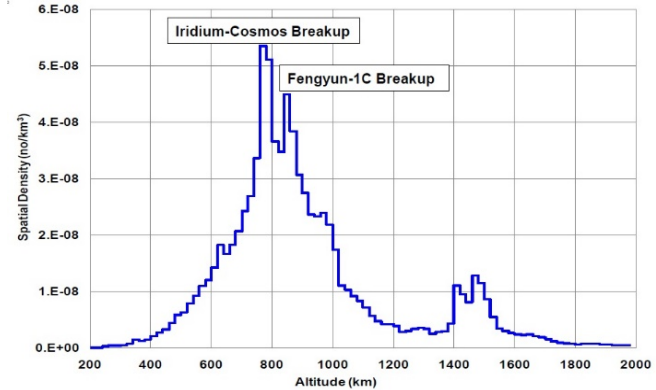
=> **SSO, ~800km**

- **Spacecraft**

Wide range of spacecraft

=> **Small (750kg), medium (1500kg), heavy (4000kg)**

**Focus on satellites** posing bigger hazard with **higher casualty risks** (with optical instruments, Ti-alloy tanks, heavy reaction wheels, ...)

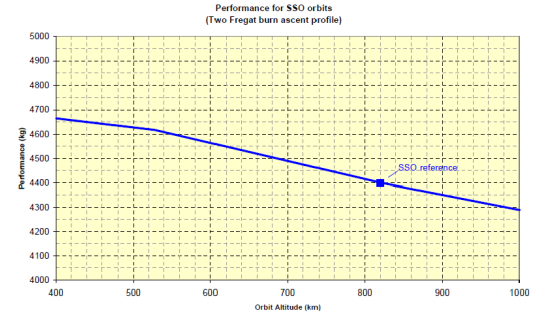
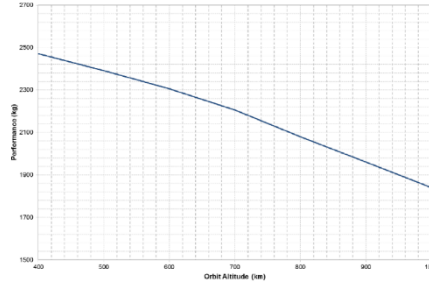


NASA report on Debris (2011)

# I) Mission Design: b) Mission overview

## Launchers' capacity

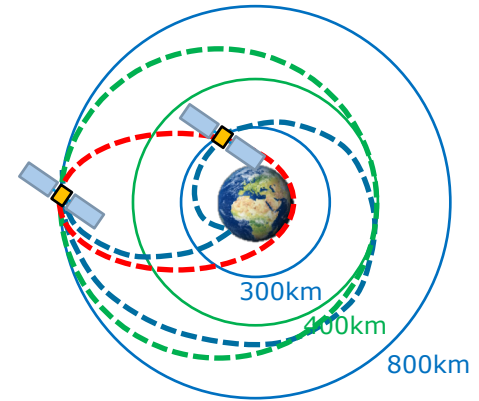
Altitude	Vega C	Soyuz ST
800 km	2080 kg	4430 kg
300 km	2550 kg	4710 kg



Performances of Vega C (left) and Soyuz ST (right) for SSO orbits as written in the launcher's manual

## Mission

- **Injection of S/C** in orbit with Vega C/Soyuz ST
  - 800km
  - 300km
- **Main propulsion system (MPS)**
  - (Orbit raising if injection at 300km:  $\Delta v_{0'}$  = 274 m/s)
  - **Operational lifetime:**  $\Delta v_0$  = 100 m/s
  - **Lowering perigee** down to 430 km:  $\Delta v_{12}$  = 99 m/s
- **Deorbiting propulsion system (DPS)**
  - **Final burn (FB)** down to 30 km:  $\Delta v_{23}$  = 124 m/s



Typical controlled re-entry mission

## II) Propulsion Systems: a) Main features



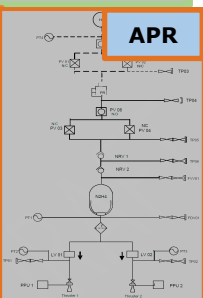
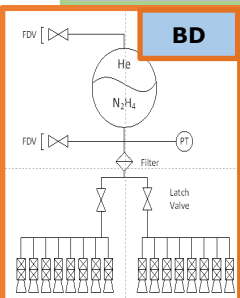
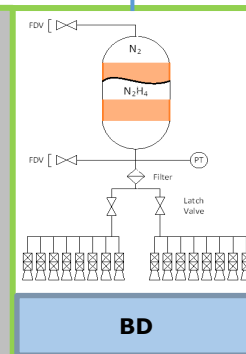
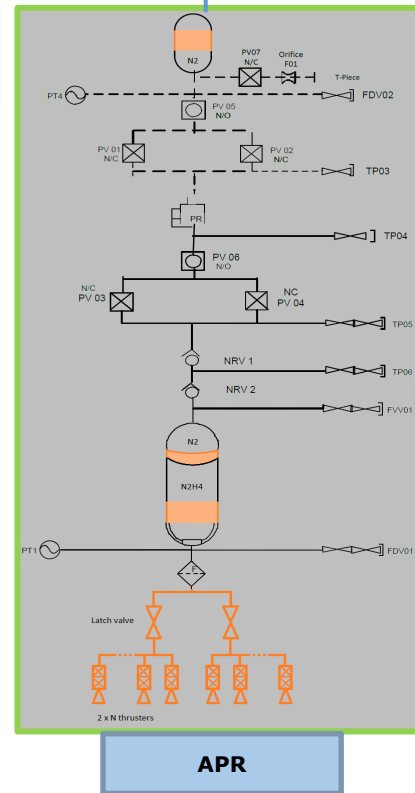
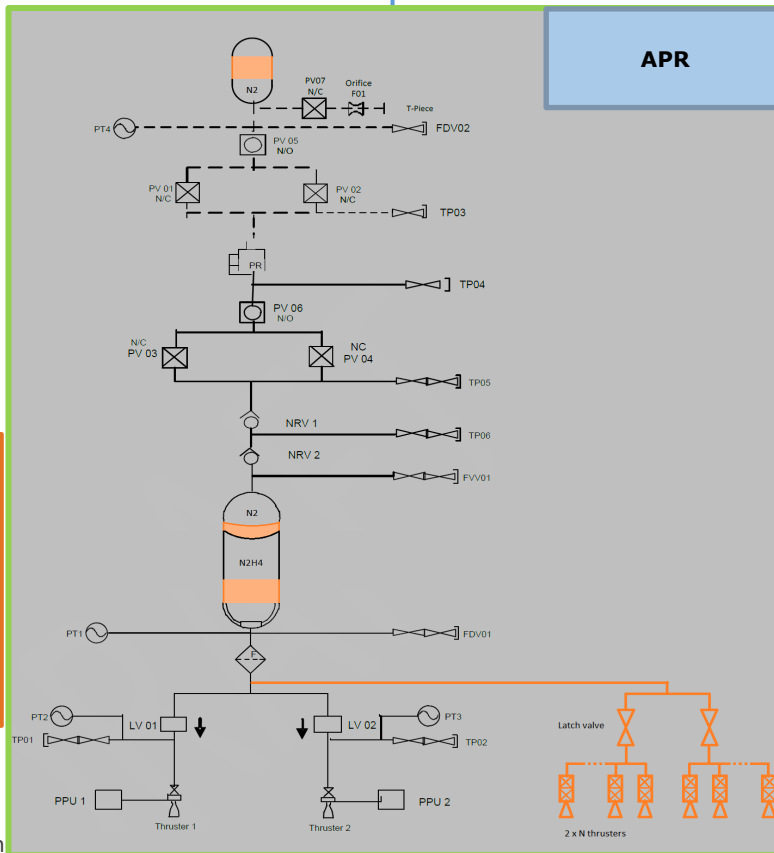
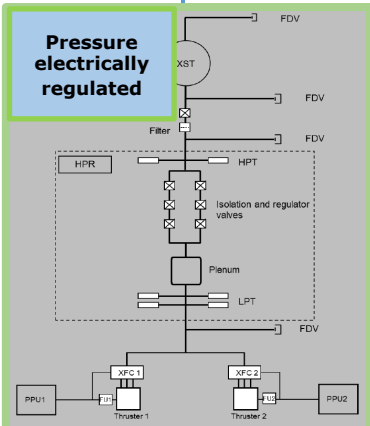
	HET	Arcjet	Monopropellant		
Model	SAFRAN: PPS-1350-G	Lockheed Martin: Aerojet MR-510	ArianeGroup		
			1N	20N	400N
Propellant	Xenon	Hydrazine	Hydrazine		
Pressuring gas	-	Nitrogen	Nitrogen		
Pressurization	Electrically regulated	APR	BD/APR		
Power	$\leq 2$ kW	$\leq 2$ kW	Neglected		
Thrust	$\leq 0.120$ N	$\leq 0.25$ N	[0.320; 1.1] N	[7.9; 24.6] N	[120; 420] N
$I_{sp}$	1660 s	600 s	[200; 223] s	[222; 230] s	[212; 220] s
Cycle life	7300	1950	59000	93130	3900
Max single burn		3 h	12 h	1.5 h	450 s
Max total burn	> 6700 h	> 1730 h	50 h	10.5 h	> 850 s
Propellant throughput	-	-	67 kg	290 kg	300 kg

**Notes:** - FB must have high thrust => **at least 1 monopropellant system** (MPS or DPS)



HET      Arcjet      Monopropellant

Monopropellant



**Electrically regulated + BD/APR**

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Note: diagrams from ADS study

## II) Propulsion Systems: b) Assumptions



- **Blowdown mode (BD):**
  - Ideal gas
  - Main operations: constant temperature
  - Final burn: isentropic adiabatic
  - Isp and thrust linear wrt inlet thruster pressure
- **Active Pressure Regulation (APR):**
  - Constant pressure
  - Isp and thrust linear wrt inlet thruster pressure
- **Performance** does not deteriorate over time
- **Redundancy 2** with thrusters
- **Negligible drag** during manoeuvres





# III) Trade-off: a) Constraints and ranking criteria

## Constraints

- **Filling ratio  $\alpha$  for blowdown**

- Pressure at thrusters' inlet: [5.5 ; 24] bar
- Temperature of hydrazine (avoid freezing):  $> 2^{\circ}\text{C}$
- **2 propulsion systems (P/S) concerned:**

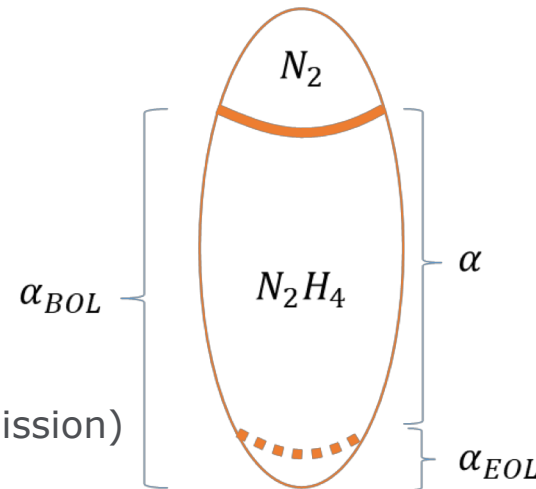
- HET + Monoprop. => Monoprop. only for FB  
=> isentropic adiabatic

$$\Rightarrow \alpha = \alpha_{BOL} - \alpha_{EOL} < 32\%$$

- Full Monoprop. => constant temperature (main mission)  
then isentropic adiabatic (final burn)

$$\Rightarrow \alpha = \alpha_{BOL} - \alpha_{EOL} < 72\%$$

- **Filling ratio  $\alpha$  for APR:**  $\alpha = \alpha_{BOL} - \alpha_{EOL} = 95\%$



# III) Trade-off: a) Constraints and ranking criteria



## Constraints

- **Maximum acceleration**
  - **< 0.04 g**
  - (tolerance up to **1 g** for small satellites)
- **FB duration**
  - **< 20%** of orbital period
- **Other thrusters constraints**
  - Number of cycles
  - Max single burn duration
  - Max total burn duration



# III) Trade-off: a) Constraints and ranking criteria



## To sum up

### Constraints

**Filling ratio  $\alpha$  for BD**  
**< 32% (HET + Monop.)**  
**< 72% (full Monop.)**

**Acceleration**  
**< 0.04 g**

**FB (% of orbital period)**  
**< 20%**

**Thrusters burn constraints**

### Ranking

**1) P/S wet mass**

**2) Reliability**

To be investigated

**3) Complexity**

**4) FB duration**

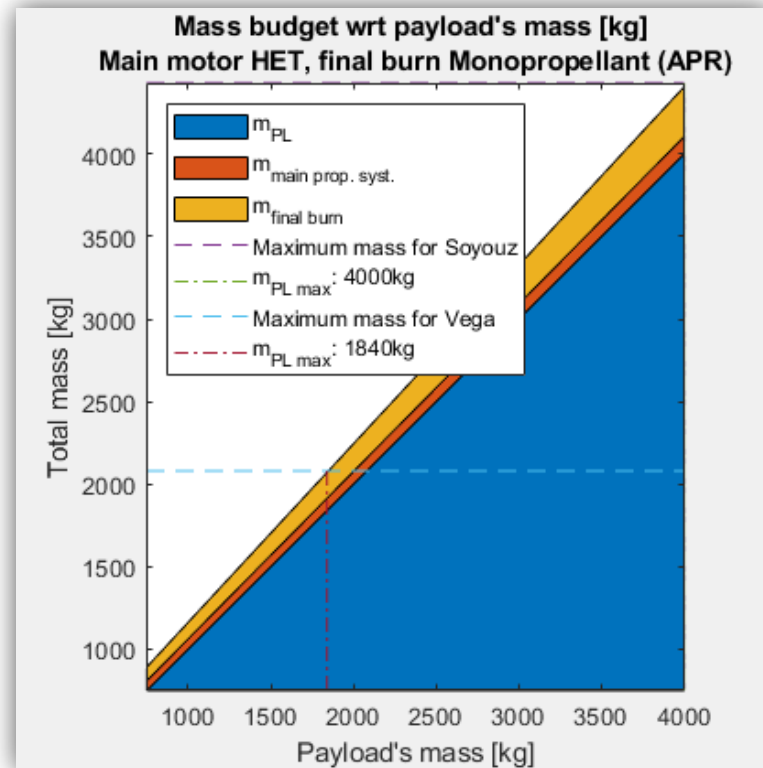
# III) Trade-off: b) Results

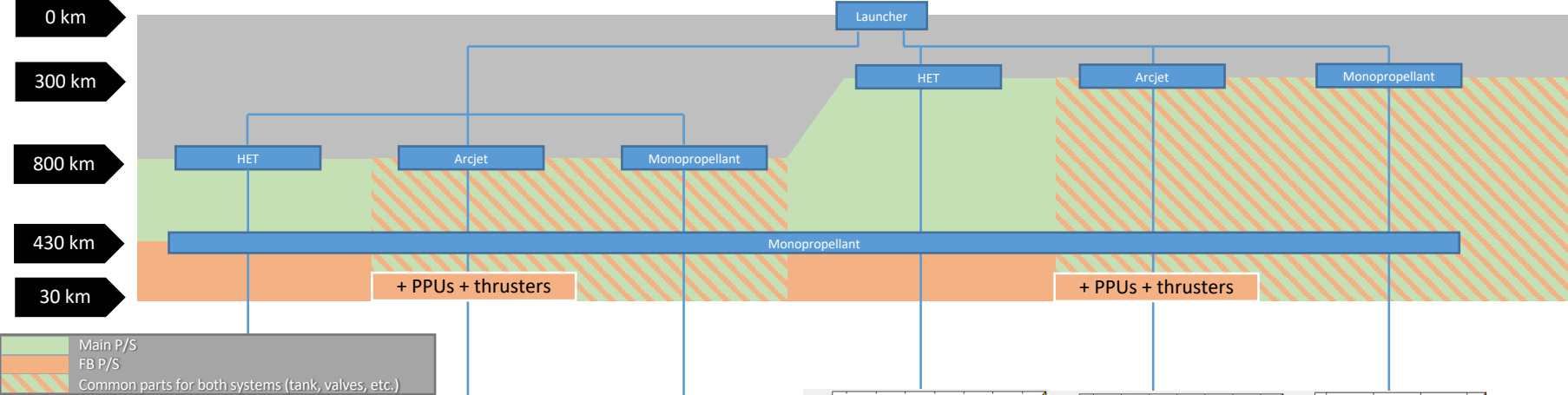
## 1. General mass comparison with different:

- Altitudes insertion
- Propulsion systems
- Pressurization systems
- Mass range [750 ; 4500] kg

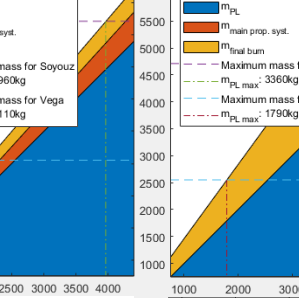
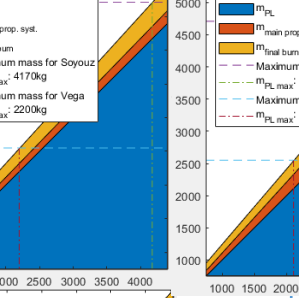
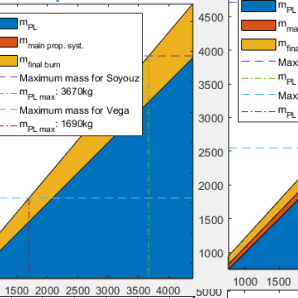
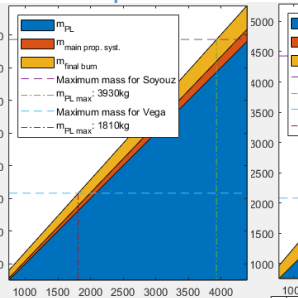
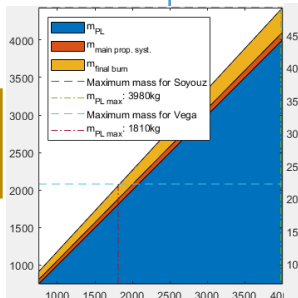


## 2. Then, focus on 750 kg, 1500 kg, 4000 kg

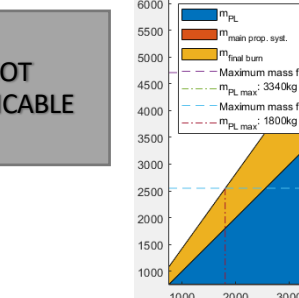
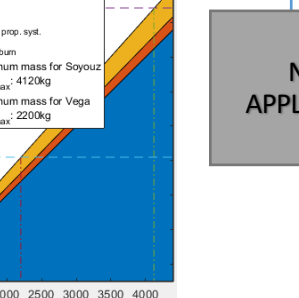
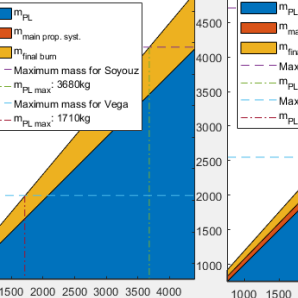
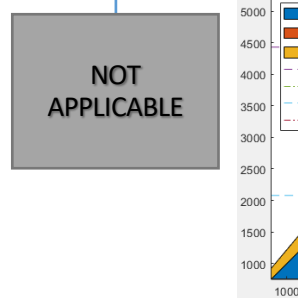
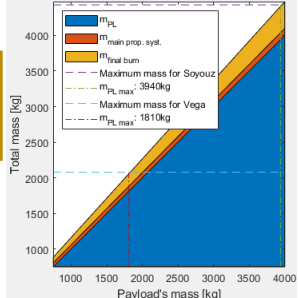


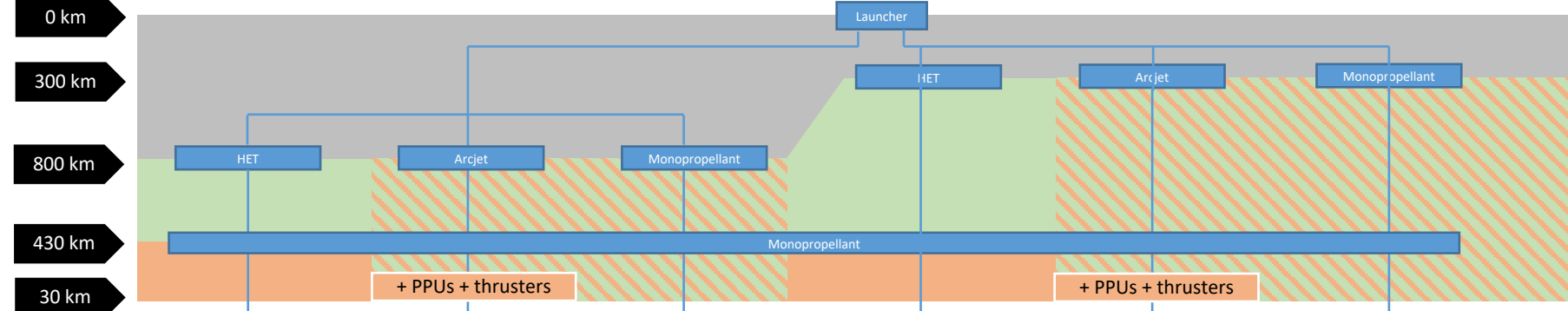


**APR**  
2x400N  
24 bar



**BD**  
2x400N  
24 bar

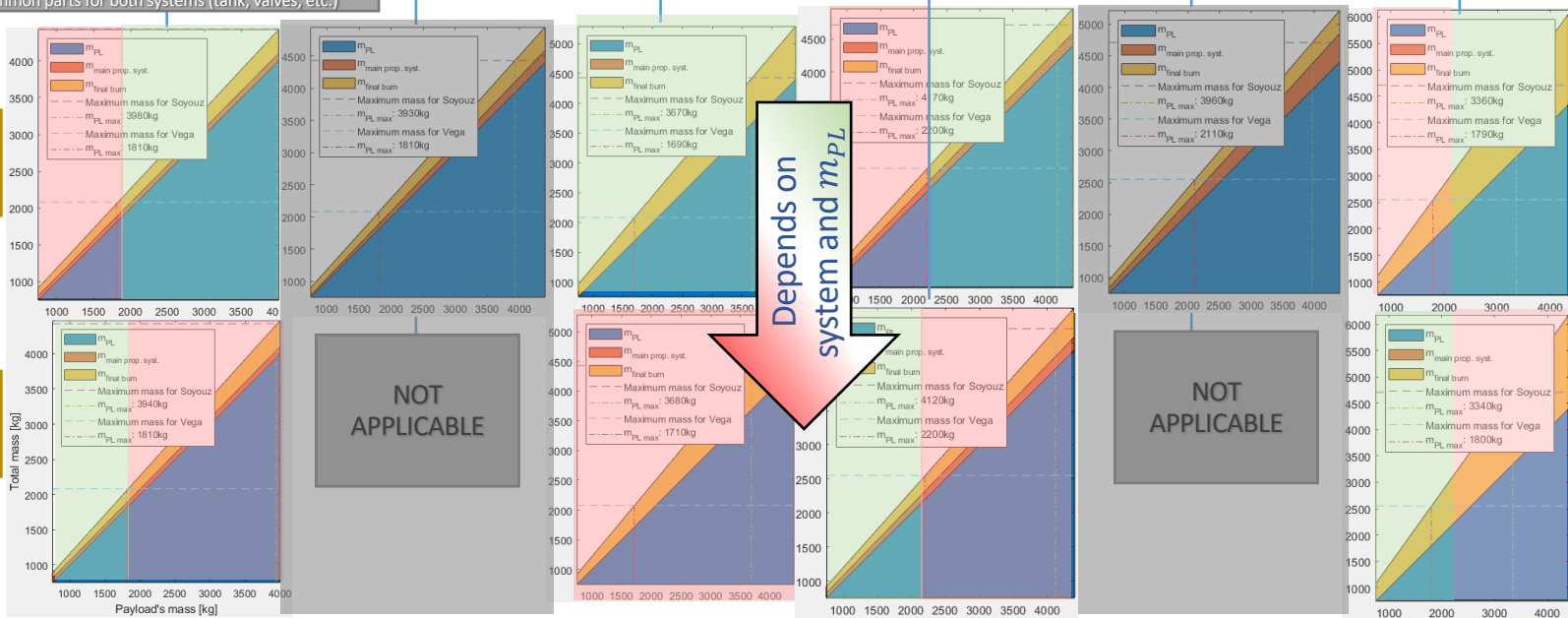


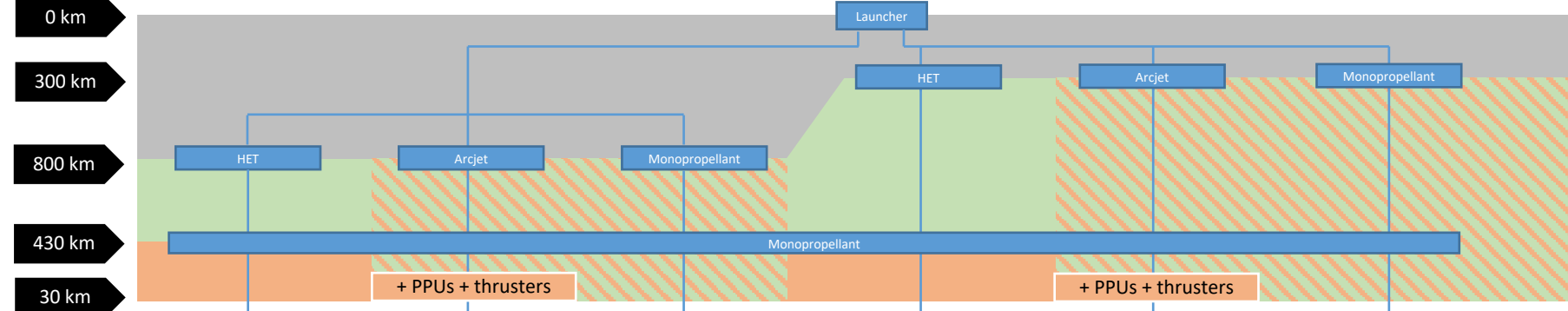


Main P/S  
 FB P/S  
 Common parts for both systems (tank, valves, etc.)

**APR**  
 2x400N  
 24 bar

**BD**  
 2x400N  
 24 bar



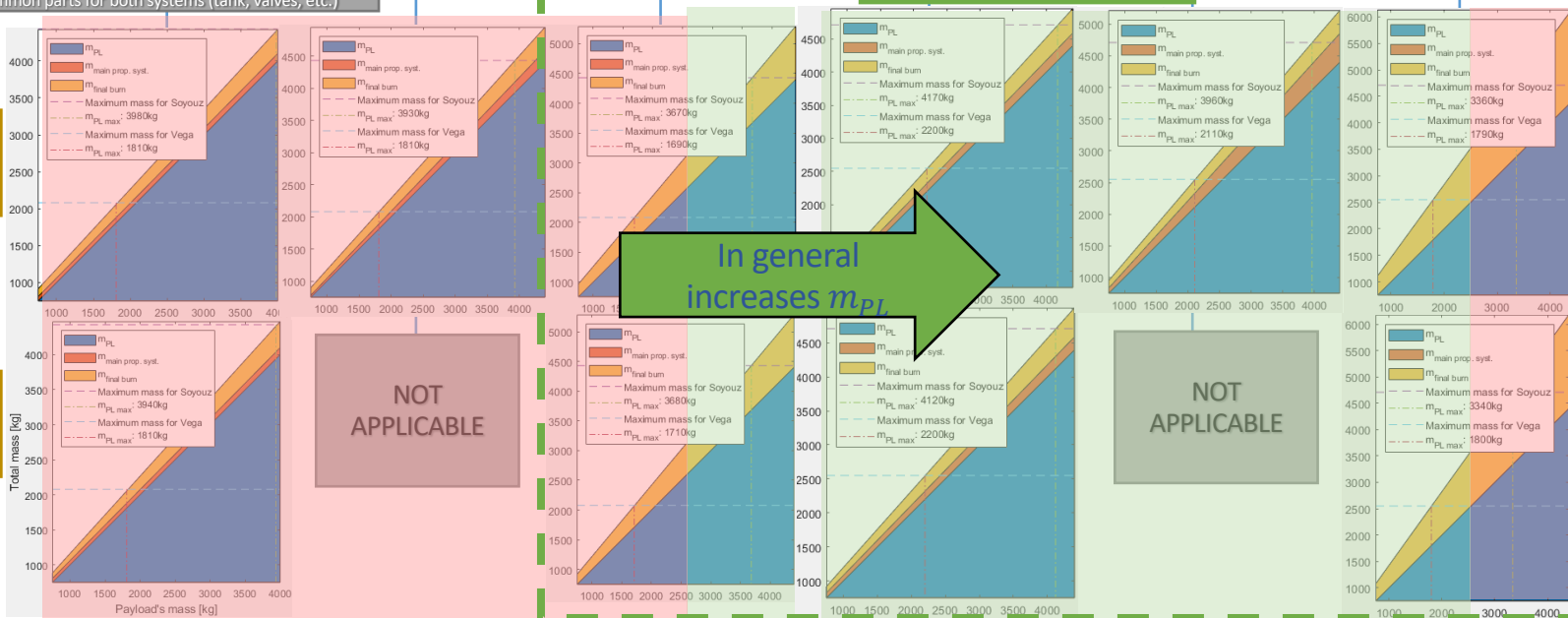


Main P/S  
 FB P/S  
 Common parts for both systems (tank, valves, etc.)

Study case

APR  
 2x400N  
 24 bar

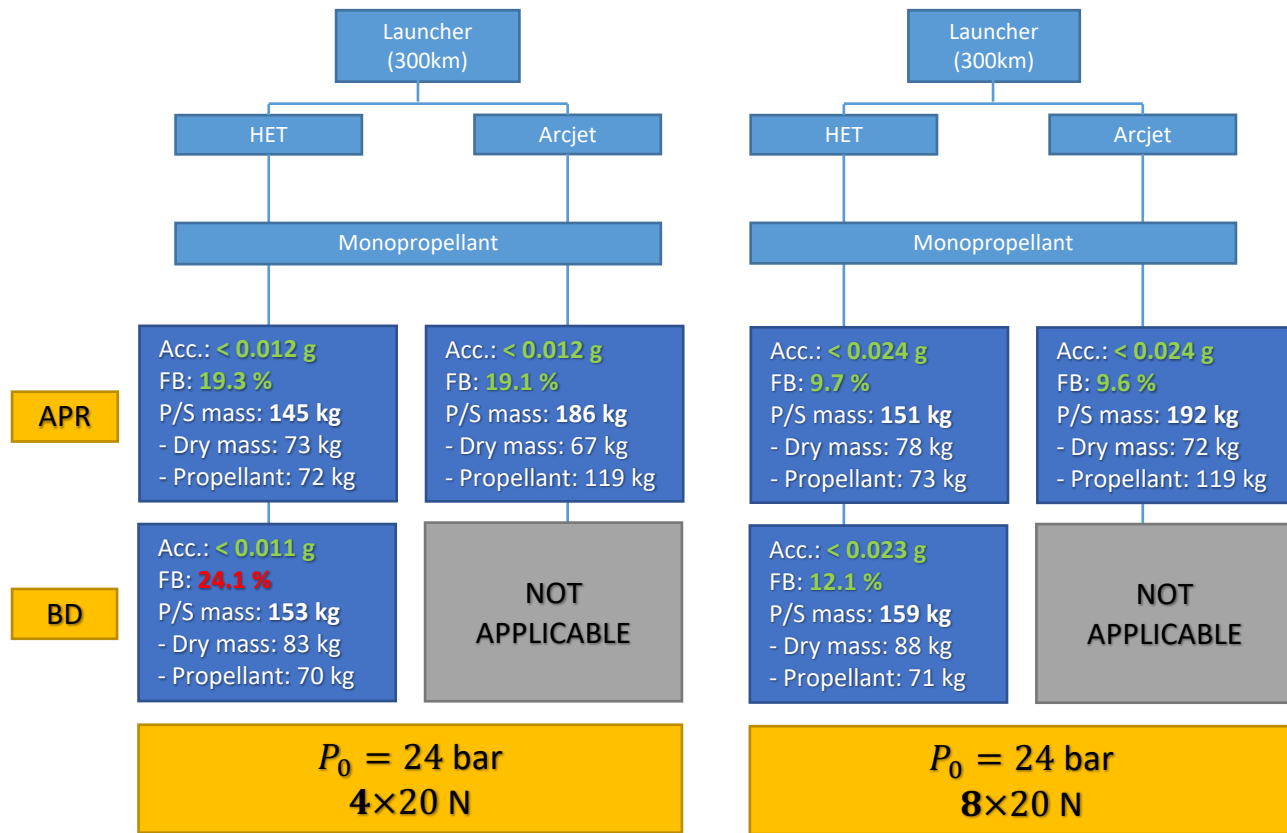
BD  
 2x400N  
 24 bar





# III) Trade-off: b) Results: example

$m_{S/C} = 750 \text{ kg}$



**Notes**

- We considered 4, 8 and 12 thrusters as a common reliable configuration, but others could be investigated
- Configuration chosen to comply with all constraints



# III) Trade-off: b) Results: summing up



$m_{S/C} = 750 \text{ kg}$

$m_{S/C} = 1500 \text{ kg}$

$m_{S/C} = 4000 \text{ kg}$

	HET	Arcjet	Monop.
Altitude	300km	300km	300km
Mode	APR	APR	BD
Thrusters	8x20N	4x20N	12x20N

	HET	Arcjet	Monop.
Altitude	300km	300km	300km
Mode	APR	APR	APR
Thrusters	8x20N	8x20N	8x20N

	HET	Arcjet	Monop.
Altitude	300k	300km	800km
Mode	APR	APR	APR
Thrusters	1x400N + 4x20N	1x400N + 4x20N	1x400N + 4x20N

P/S wet mass: 145 kg - Dry mass: 73 kg - Propellant: 72 kg	P/S wet mass: 186 kg - Dry mass: 67 kg - Propellant: 119 kg	P/S wet mass: 286 kg - Dry mass: 59 kg - Propellant: 227 kg	P/S wet mass: 224 kg - Dry mass: 85 kg - Propellant: 139 kg	Added mass: 316 kg - Dry mass: 86 kg - Propellant: 230 kg	P/S wet mass: 562 kg - Dry mass: 82 kg - Propellant: 480 kg	P/S wet mass: 485 kg - Dry mass: 113 kg - Propellant: 372 kg	P/S wet mass: 748 kg - Dry mass: 136 kg - Propellant: 612 kg	P/S wet mass: 772 kg - Dry mass: 107 kg - Propellant: 665 kg
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## Conclusion:

- **Best option mass-wise is with HET, however:**
  - HET low thrust => **higher collision risks (long transfer time) and operational complexity**
  - Two independent system => **more complex**
  - If Monopropellant system for deorbit is unused for decades => **uncertain behaviour**
- **Arcjet is a good option:**
  - Good compromise between  $I_{sp}$  and thrust => **high efficiency and reduced time, thus hazard, in space**
  - One shared system => **limit complexity**
- **Next steps:** consider and weight the other criteria (reliability, complexity, etc.) to complete the trade-off