## Reduced-order Non-equilibrium Radiative Transfer for 3D Problems

#### Amal Sahai<sup>\*</sup>, Christopher O. Johnston<sup>†</sup>, Bruno Lopez<sup>\*</sup>, Marco Panesi<sup>\*</sup>

\*University of Illinois at Urbana-Champaign <sup>†</sup> NASA Langley Research Center

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#### Outline

#### Introduction

- 2 Spectral Reduced-order Models
- 3 Radiation Binning Strategy
- 4 3D RTE
- 5 Mars Entry Wake Flows
- 6 Summary and Future Work

#### Introduction

 Coupled flow-radiation calculations crucial for accurately characterizing properties for different applications:



#### Hypersonic Planetary Entry

Sahai et al., AIAA Scitech 2019.

#### Introduction

• Coupled flow-radiation calculations crucial for accurately characterizing properties for different applications:



#### **Arc-heated Flows**

Sahai et al., Plasma Sources Science and Technology 2017.

#### Introduction

• Coupled flow-radiation calculations crucial for accurately characterizing properties for different applications:



#### Laser-plasma Interaction

Alberti et al., AIAA Scitech 2019.

#### Objective

"Development of a physics-based reduced-order framework for solving non-equilibrium chemical kinetics and radiation for complex flow problems."



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"Development of a physics-based reduced-order framework for solving non-equilibrium chemical kinetics and radiation for complex flow problems."



*"Model-reduction imperative for resolving two-way coupling between thermochemical and radiation models."* 

Sahai et al.

#### Objective

- Three key challenges for performing radiation calculations in conjunction with CFD:
  - Evolve efficient / accurate reduced-order models to capture spectral variance in properties.



Spectrally varying radiative wall heat flux from  $\text{CO}_2$  for a 1-D problem

- Solve radiative transfer equations (RTEs) for 3D unstructured meshes.
- Self-consistent radiation-flow coupling to account for non-local absorption.

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#### Reduced-order Models for Spectral Properties

• Monochromatic steady-state RTE describing the spectral intensity  $I_{\nu}$ corresponding to frequency  $\nu$  in the  $\Omega$  direction:

$$oldsymbol{\Omega}$$
 .  $oldsymbol{
abla} I_
u(oldsymbol{x},oldsymbol{\Omega}) \;\;=\;\; E_
u \;-\; \sigma_
u \, I_
u(oldsymbol{x},oldsymbol{\Omega})$ 

- Radiative properties can vary rapidly with frequency.
- Line-by-line (LBL) approach entails computing intensities for individual frequencies followed by integration in frequency space to obtain total quantities:

$$I(\boldsymbol{x}, \boldsymbol{\Omega}) = \int_{\nu_{\min}}^{\nu_{\max}} I_{\nu} \, d\nu$$

- This approach, although exceedingly accurate, is impractical for online radiation calculations on complex 3D systems.
- Reduced-order models imperative for reducing cost of evaluating properties  $(E_{\nu}, \sigma_{\nu})$  and then solving RTEs.

### Spectral Reduced-order Models

- First Step: Methodology for creating reduced-order groups for which RTEs are solved (not large number of original frequencies):
  - Multi-band Multi-bin based on Planck averaging (Rosseland mean).
  - Method of homogenization.
  - Correlated / Scaled k-distributions
- The last two methods rely on statistics (not assumed spectral distributions) and are said to work more reliably for a broader set of physical situations.
- Second Step: Investigate physical criteria and subsequent grouping strategy for identifying which LBL frequencies need to be clustered together (analogous to work on StS kinetics).

Sahai et al., Adaptive coarse graining method for energy transfer and dissociation [1] kinetics of polyatomic species, J. Chem. Phys. (2017).

### General Methodology for Spectral Reduced-order Models



Bands based on frequency and bins based on opacity

- Model-reduction techniques differ in what "average" properties are prescribed for groups (band/bin combination).
- More sophisticated clustering approaches expected to change this simple frequency – opacity (continuous interval) grouping paradigm.

Sahai et al.

#### Multi-band Multi-bin using Planck Averaging

 This approach assumes a frequency-wise intensity distribution while computing the representative *σ̂* for given group *i*:

$$\hat{\sigma}_i = \int \sigma_{\nu} I_{\nu} d\nu / \int I_{\nu} d\nu$$

- Setting  $I_{\nu}$  equal to Planck distribution  $B_{\nu}(T)$  ensures that spectral radiance within a group maximizes entropy (analogous to Boltzmann distribution within chemical bins).
- The maximum entropy formulation becomes more consistent if assumed spectral radiance satisfies constraint based on total group intensity  $\hat{I}_i$ :

$$\hat{I}_i = \int I_{\nu} \, d\nu = \int B_{\nu}(\mathbf{T_{rad}}) \, d\nu$$

• Re-computing  $T_{rad}$  ( $\neq T_{flow}$ ) ensures that integral of Planck weights for spectral averaging matches group intensity.

#### Homogenization

### Theory of Homogenization (Haut *et al.*, JQSRT, 2017)

- Homogenization discards assumed spectral distributions in favor of statistics to derive "averaged"  $\hat{\sigma}_i$ .
- The method relies on estimating the probability distribution  $p(\sigma_{\nu})$ (Young measure) of the value of the absorption coefficient  $\sigma_{\nu}(\phi_{o})$ .

$$I_{\nu}^{exact} = \int_{0}^{\infty} I(\sigma_{\nu}) \, p(\sigma_{\nu}) \, d\sigma_{\nu}$$

 Young measure is discretized to obtain the conventional multi-band multi-bin reduced-order model. This involves computing  $p_{ij}$  which is the probability of:

$$\sigma_j \leq \sigma_\nu < \sigma_{j+1} \quad \forall \quad \nu \in [\nu_i, \nu_{i+1}]$$

- Discretized Young measure  $p_{ij}$  is essentially the probability of being in the  $i^{th}$  frequency band and  $j^{th}$  opacity bin.
- Total intensity is then computed using a weighted average:

$$I_{total} = \sum_{i} \sum_{j} p_{ij} I_{ij}$$

#### Reordered k-distribution (Modest et al., JQSRT, 2003)

- Reodered k-distributions strictly applicable to equilibrium radiation (oscillations induced by absorption coefficients).
- Non-equilibrium radiation modeled using  $I_{\nu}^{neq}\,=\,E(\nu,\phi)\,/\,\sigma(\nu,\phi)$
- Original *v*-dependent RTE reordered in *k*-space (absorption coefficient values):

$$I_k = \int_0^\infty I_\nu \,\delta(k - \sigma_\nu(\underline{\phi}_0)) \,d\nu$$

 Non-equilibrium emission-weighted probability density function is defined for frequency band i:

$$f(\underline{\phi}, \underline{\phi}_{0}, k) = \left[ \int_{0}^{\infty} I_{\nu}^{neq}(\underline{\phi}) \,\delta(k - \sigma_{\nu}(\underline{\phi}_{0})) \,d\nu \right] / I_{i}^{neq}(\underline{\phi})$$

• RTE in the *k*-space:

 $\boldsymbol{\Omega} \cdot \boldsymbol{\nabla} I_k \ = \ \boldsymbol{k}^*(\underline{\phi}, k) \, f(\underline{\phi}, \underline{\phi}_0, k) \, I_i^{neq}(\underline{\phi}) \ - \ \boldsymbol{k}^*(\underline{\phi}, k) \, I_k$ 

#### Galileo

• Jupiter entry with ablation products, peak heating point:

$$- U_{\infty} = 41.6 \ km/s$$

$$- \rho_{\infty} = 3.49 \times 10^{-4} \ kg/m^3$$

- Strong atomic H lines and atomic continuum from H provide dominant emission from the inviscid region.
- C3 and C2H, and H2 molecular band systems provide boundary layer absorption.
- Original LBL calculations require  $\sim \mathcal{O}(10^6)$  frequencies.



## Galileo



Reduced-order models based on 25 bands × 25 bins.

### Galileo



Reduced-order models based on 25 bands × 50 bins.

#### Stardust

- Earth entry:
  - $U_{\infty} = 11.69 \ km/s$
  - $-\rho_{\infty} = 1.05 \times 10^{-4} \ kg/m^3$
- Atomic N lines are the dominant contributors.
- Molecular bands and the atomic continuum are also included.
- Original LBL calculations require  $\sim \mathcal{O}(10^6)$  frequencies.



### Stardust



Reduced-order models based on 25 bands × 25 bins.

## Stardust



Reduced-order models based on 25 bands × 50 bins.

#### Meteor Precursor

- Earth entry, no ablation products:
  - $U_{\infty} = 20 \ km/s$  $-\rho_{\infty} = 9.78 \times 10^{-4} \ kg/m^3$
- Strong N and O lines dominate.
- Original LBL calculations require  $\sim \mathcal{O}(10^6)$  frequencies.
- LOS located along the stagnation line

#### Meteor Precursor

Reduced-order models based on 25 bands × 25 bins.



Sahai et al.

#### Meteor Precursor

Reduced-order models based on 25 bands × 50 bins.



Sahai et al.

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#### Radiation Binning Strategy for MBOB Framework

- Grouping criteria for radiation not straightforward (unlike state-to-state chemistry) because spectral intensities uncoupled.
- Conventional grouping focuses on frequency bands + opacity bins.
- Non-intuitive grouping criteria can be evolved by comparing LBL and reduced-order LOS solutions:

$$I_{\nu}(s) = I_{\nu}(0) \exp\left(-\int_{0}^{s} \sigma_{\nu} ds'\right)^{\bullet} 0$$
$$+ \int_{0}^{s} E_{\nu} \exp\left(-\int_{s'}^{s} \sigma_{\nu} ds''\right) ds$$

• Reduced-order group intensity ( $I_{ij} = \int I_{\nu} d\nu$ ) is unpacked to obtain frequency-wise intensity:

$$I_v \approx I_{ij} \frac{B_\nu}{\int B_\nu \, d\nu}$$

#### Radiation Binning Strategy for MBOB Framework

• Medium assumed to be homogeneous in order to simplify analysis.

$$\frac{B_{\nu}}{\int B_{\nu} d\nu} E_{ij} \exp\left(-\int_{s'}^{s} \sigma_{ij} ds''\right) = E_{\nu} \exp\left(-\int_{s'}^{s} \sigma_{\nu} ds''\right)$$

• Term-by-term comparison of the Taylor series expansion allows group and spectral properties to be compared:

$$E_{ij} \sigma_{ij}^{n} \frac{B_{\nu}}{\int B_{\nu} d\nu} = E_{\nu} \sigma_{\nu}^{n}$$
  
$$\Rightarrow \frac{E_{\nu}}{E_{ij}} = \frac{E_{\nu} \sigma_{\nu}}{E_{ij} \sigma_{ij}} = \frac{E_{\nu} \sigma_{\nu}^{2}}{E_{ij} \sigma_{ij}^{2}} = \dots = \text{Constant}$$

- $\sigma_{\nu} = \sigma_{ij} = \text{Constant}$  is a trivial solution rationale for regular opacity binning.
- Generalized approach bands based on  $E_{\nu}$  and bins based on  $E_{\nu}\,\sigma_{\nu}.$

#### Stardust



• Reduced-order models based on 20 bands  $\times$  20 bins.

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#### Stardust

 $\bullet\,$  Reduced-order models based on 25 bands  $\times$  25 bins.



#### Stardust

 $\bullet\,$  Reduced-order models based on 25 bands  $\times$  25 bins.



#### Meteor



Reduced-order models based on 10 bands × 10 bins.

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#### Meteor



• Reduced-order models based on 25 bands  $\times$  25 bins.

#### Meteor

 $\bullet\,$  Reduced-order models based on 25 bands  $\times$  25 bins.



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#### Coupled Radiation-Flow Solutions for 3D Meshes

- Efficient spectral reduced-order models and RTE solution methodology key for managing computational loads.
- Angular integration performed with focus on reducing the number of rays required for accurate solution.
- Total radiative heat flux (and its divergence) computed using a Gaussian / Lebedev type angular quadrature:

$$\mathbf{q}^{rad} = \int_{4\pi} I_{\nu} \, \mathbf{\Omega} \, d\mathbf{\Omega} = \sum_{m} w^{m} \, I_{\nu}^{m} \, \mathbf{\Omega}^{m}$$

- FEM / FVM based discretization avoids concomitant challenges associated with ray tracing.
- Angularly / spatially resolved radiation allows species continuity source terms to be computed while accounting for non-local absorption.

#### Finite Volume based RTE Solver

• A finite-volume formulation is obtained by integrating the RTE in direction **n** over an element (and then discretizing it):

$$\sum_{f} \mathbf{n} \cdot \mathbf{S}^{f} I_{\nu}^{f} = -\hat{\sigma}_{\nu} I_{\nu}^{e} V_{e}$$

• Flux summation is evaluated by first-order upwinding:

$$I_{\nu}^{f} = \begin{cases} I_{\nu}^{e} , & \text{for } \mathbf{n} . \mathbf{S}^{f} > 0 \\ I_{\nu}^{neigh} , & \text{for } \mathbf{n} . \mathbf{S}^{f} < 0 \end{cases}$$

$$I(\mathbf{r}_{c}) = -\frac{\sum_{\mathbf{n} . \mathbf{S} < 0} \mathbf{n} . \mathbf{S} I(\mathbf{r}_{o})}{\sum_{\mathbf{n} . \mathbf{S} > 0} \mathbf{n} . \mathbf{S} + \sigma(\mathbf{r}_{c}) \Omega_{c}}$$

$$\mathbf{n} \cdot \mathbf{s} < 0$$

• Sparse linear system re-ordered into lower triangular system by sweeping the mesh according to an advance-order list.

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#### Self-consistent Radiation-flow Coupling

- Two-way coupling Flowfield solution passed on to radiation solver while radiative field information (source terms) provided to flow solver.
- Rate constants for radiative processes involving emission and absorption (no escape factor assumption) between species l and u are:  $\mathcal{M}_{u} = \int \sigma u \, dx$

$$\bar{K}_{u,l}^{em} = \frac{\mathcal{M}_{u}}{\rho_{u} N_{A}} \int E_{\nu}^{u,l} d\nu K_{l,u}^{ab} = \frac{\mathcal{M}_{l}}{\rho_{l} N_{A}} \int \left( \sigma_{\nu}^{l,u} \oint_{4\pi} I_{\nu} d\Omega \right) d\nu$$

• Source terms for species continuity and energy equations:

$$\begin{aligned} \dot{\omega}_{l}^{rad} &= \sum_{\forall u \mid u \neq l} \left( -K_{l,u}^{ab} \,\rho_{l} \,+\, \bar{K}_{u,l}^{em} \,\rho_{u} \right) \\ \Omega^{rad} &= -\boldsymbol{\nabla} \cdot \boldsymbol{q}^{rad} \,= \,-\boldsymbol{\nabla} \cdot \int \oint_{4\pi} I_{\nu} \,\boldsymbol{\Omega} \,d\boldsymbol{\Omega} \,d\nu \end{aligned}$$

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#### Mars 2020 3D Wake Flows: $CO_2 - M$ StS Model

- 9,056 vibrational levels for ground electronic state of CO<sub>2</sub>.
- Each level defined using 4 modes: 1 symmetric stretching, 2 degenerate bending, and 1 asymmetric stretching.
- $CO_2$  molecule has multiple pathways for vibrational relaxation ( $\sim 100,000$  possible transitions in current model):

$$\begin{array}{rcl} \mathsf{VT}_2 &:& \mathsf{CO}_2(v_1,v_2,v_3)\,+\,\mathsf{M}\longleftrightarrow\mathsf{CO}_2(v_1,v_2\pm 1,v_3)+\mathsf{M}\\\\ \mathsf{VV}_{1-2} &:& \mathsf{CO}_2(v_1,v_2,v_3)\,+\,\mathsf{M}\longleftrightarrow\mathsf{CO}_2(v_1\pm 1,v_2\mp 2,v_3)+\mathsf{M}\\\\ \mathsf{VV}_{2-3} &:& \mathsf{CO}_2(v_1,v_2,v_3)\,+\,\mathsf{M}\longleftrightarrow\mathsf{CO}_2(v_1,v_2\pm 3,v_3\mp 1)+\mathsf{M}\\\\ \mathsf{VV}_{1-2-3} &:& \mathsf{CO}_2(v_1,v_2,v_3)\,+\,\mathsf{M}\longleftrightarrow\mathsf{CO}_2(v_1\pm 1,v_2\pm 1,v_3\mp 1)+\mathsf{M} \end{array}$$

• Dissociation/recombination occurs as follows:

$$\mathsf{CO}_2(v_1, v_2, v_3) + \mathsf{M} \longleftrightarrow \mathsf{CO} + \mathsf{O} + \mathsf{M}$$

[1] I. Armenise, E.V. Kustova. *State-to-state models for CO*<sub>2</sub> *molecules: From the theory to an application to hypersonic boundary layers.* Chemical Physics 415 (2013).

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3D Non-equilibrium Radiation

#### Mars 2020 3D Wake Flows: Coarse Grain Method



#### Mars 2020 3D Wake Flows: Computational Setup

$\mathrm{V}_{\infty} \; [km/s]$	$ ho_\infty \ [kg/m^3]$	$\mathrm{T}_{\infty}\left[K ight]$	$\alpha [K]$
5.46	8.44E-5	144	15.26
4.64	1.05E-4	184	15.65
3.89	1.84E-3	193	15.88

1) Trajectory points considered

2) Mars 2020 vehicle

- Three-dimensional Mars 2020 mesh with  $\sim 2\times 10^6$  mesh elements and 170 quadrature directions.
- Gas mixture includes: 10 CO<sub>2</sub> Bins, CO, O<sub>2</sub>, C, O.
- Compare flowfields (US3D) and resultant IR radiation (NERO) for 1-T / 2-T Boltzmann and reduced-order StS models.
- $\bullet\,$  Radiative transitions in 1.5, 2.7, and 4.5  $\mu m$  bands are considered.







Streamline 2: Solid Lines - Reduced-order StS, Dashed Lines - 2T





## Summary and Future Work

#### Summary

- MBOB with Planck-averaging just as accurate as statistics-based model reduction methods (that still rely on reordering σ<sub>ν</sub>).
- Non-intuitive grouping strategies crucial for improving predictions for total and spectral quantities.
- Efficiency gains through reduced-order spectral models and simpler angular/spatial discretization enable coupled radiation-flow calculations even for complex 3D geometries.
- Complete characterization of CO<sub>2</sub> wake flows using reduced-order thermochemistry bins and self-consistent radiation coupling.

#### Future Work

- Experiment with other spatial discretization schemes for RTEs.
- Perform flow-radiation coupled calculations for other sytems.

#### Homogenization: Extension to Non-Equilibrium Radiation

- Original framework developed only for equilibrium radiation with fluctuations induced solely by absorption coefficients.
- Non-equilibrium emission intensity :  $I_{\nu}^{neq} = E(\nu, \underline{\phi}) \, / \, \sigma(\nu, \underline{\phi})$
- Probability distribution computed using weighted integrals (for reference state):

$$p_{ij} = \int_{\nu \in \text{bin } j} I_{\nu}^{neq} \, d\nu \quad \left/ \int_{\nu \in \text{band } i} I_{\nu}^{neq} \, d\nu \right.$$

• Bin opacity computed using weighted average:

$$\sigma_{ij} = \int_{\nu \in \text{bin}\,j} \sigma(\nu, \mathbf{T}) I_{\nu}^{neq} \, d\nu \Big/ \int_{\nu \in \text{bin}\,j} I_{\nu}^{neq} \, d\nu = \int_{\nu \in \text{bin}\,j} E_{\nu} \, d\nu \Big/ \int_{\nu \in \text{bin}\,j} E_{\nu} / \sigma_{\nu} \, d\nu$$

#### Homgenization: Extension to Non-Equilibrium Radiation

- Bin-wise source term can be computed in manner analogous to equilibrium radiation.
- Tested multiple forms for the source term most accurate based on conserving total emission:

$$E_{ij} = \int_{\substack{\nu \in \text{bin}\,j}} E_{\nu} \, d\nu \, \times \left( \frac{\int_{\substack{\nu \in \text{band}\,i}} E_{\nu} / \sigma_{\nu} \, d\nu}{\int_{\substack{\nu \in \text{bin}\,j}} E_{\nu} / \sigma_{\nu} \, d\nu} \right)_{\text{Ref}} = \frac{\int_{\substack{\nu \in \text{bin}\,j}} E_{\nu} \, d\nu}{p_{ij}}$$

- $\sigma_{ij}$  and  $E_{ij}$  can be pre-computed for different thermodynamic states.
- Computing total intensities for individual bands requires solving the RTEs for constituent bins (with properties  $\sigma_{ij}$  and  $E_{ij}$ ) and then averaging using  $p_{ij}$  as weights.

#### Reordered k-distribution

- *k*-distribution based on *f* can be ill-behaved, making integration in *k* space difficult.
- Transformation into smoother *g*-space performed through division by  $f(\underline{\phi_0}, \underline{\phi_0}, k)$ :

 $\boldsymbol{\Omega} \cdot \boldsymbol{\nabla} I_g = k^*(\underline{\phi}, \underline{\phi}_0, g) \, a(\underline{\phi}, \underline{\phi}_0, g) \, I_i^{neq}(\underline{\phi}) - k^*(\underline{\phi}, \underline{\phi}_0, k) \, I_g$ 

$$\begin{split} I_g &= I_k / f(\underline{\phi}_0, \underline{\phi}_0, k) \\ g(\underline{\phi}_0, \underline{\phi}_0, k) &= \int_0^k f(\underline{\phi}_0, \underline{\phi}_0, k) \, dk \\ a(\underline{\phi}, \underline{\phi}_0, k) &= f(\underline{\phi}, \underline{\phi}_0, k) / f(\underline{\phi}_0, \underline{\phi}_0, k) \end{split}$$

• Integration in *g*-space performed using numerical quadrature.

$$I_i = \int_0^1 I_g \, dg$$

#### Spectral Clustering for CO<sub>2</sub>



Sahai et al.

Supplementary Slides

Spectral Clustering for N<sub>2</sub>  $(^{1}\Sigma_{q}^{+}) - N(^{4}S_{u})$ 



Supplementary Slides

# Spectral Clustering for $N_2(^{1}\Sigma_{g}^{+}) - N(^{4}S_u)$

