

Design Simulation and Software Validation for **On-Board and Real-Time** Optimal Guidance

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WHY DO WE NEED REAL-TIME OPTIMAL GUIDANCE?

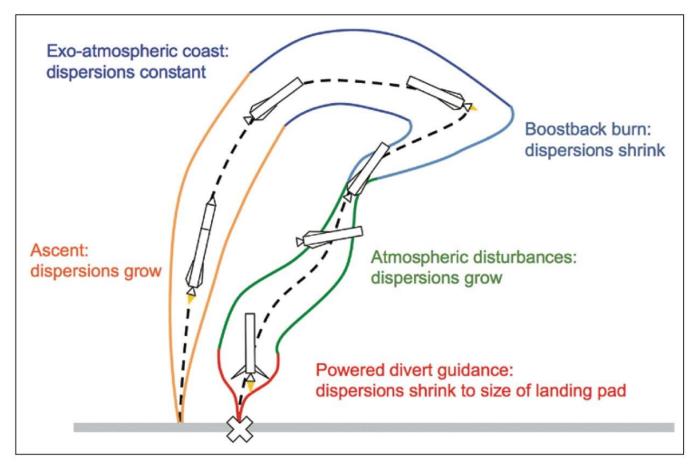


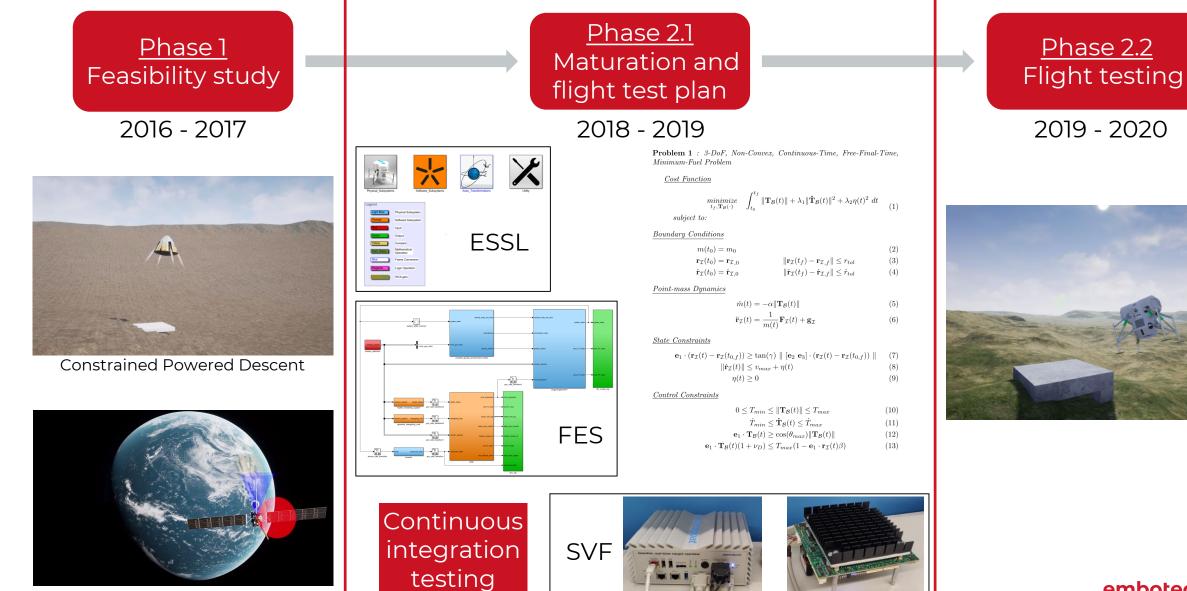
FIGURE 4 Phases of an F9R return-to-launch-site mission. The colored lines represent the largest possible variations in the trajectory, known as dispersions.

- Trajectory optimality under actual flight conditions
- Ensure mission completion under constraints and actual flight conditions
- Reduce missionization time
- Mid-flight replanning (mission flexibility)

On-line optimization enables autonomous space operations



PROJECT TIMELINE



Constrained Attitude Guidance

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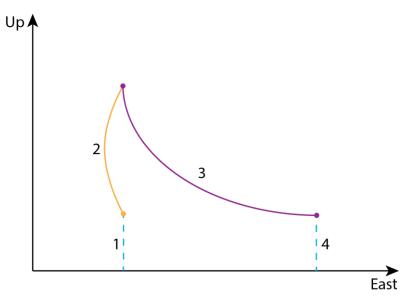
MISSION PROFILE



INCAS Demonstrator for Technology Validation: DTV

- Jet powered
- Vertical Takeoff and Landing
- Max thrust = 900N
- Weight = 60 70 Kg
- Hight = 1.2 m

End-to-End mission scenario

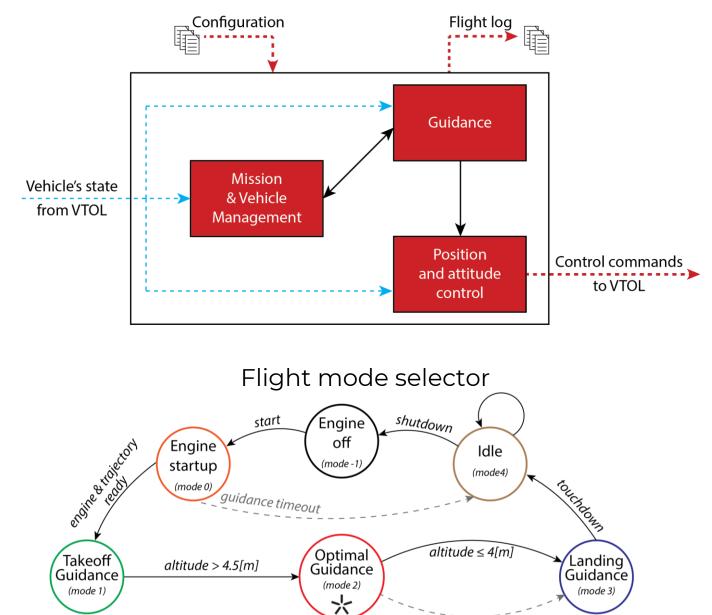


- 1. Vertical takeoff
- 2. Ascent (Real-Time Optimal Guidance)
- 3. Descent (Real-Time Optimal Guidance)
- 4. Vertical landing



GUIDANCE AND CONTROL ARCHITECTURE

auidance exception



MVM

- Flight mode selector
- Target manager
- Handle exceptions
- Tracking errors
- Engine faults
- Retargeting
- Emergency landing

Guidance

- Constant velocity takeoff
- 3-DoF NLP optimal
- Constant velocity landing

Control

- LQR on position and attitude
- FF aerodynamics balancing



OPTIMAL GUIDANCE

Tested strategies •

3-DoF non-convex

6-DoF non-convex

Thrust constraints

max

3-DoF convex

3-DoF convex with ToF lookup table

Problem 1 : 3-DoF, Non-Convex, Continuous-Time, Free-Final-Time, Minimum-Fuel Problem

Cost Function

$$\underset{t_f, \mathbf{T}_{\mathcal{B}}(\cdot)}{\text{minimize}} \quad \int_{t_0}^{t_f} \|\mathbf{T}_{\mathcal{B}}(t)\| + \lambda_1 \|\dot{\mathbf{T}}_{\mathcal{B}}(t)\|^2 + \lambda_2 \eta(t)^2 dt$$
(1)

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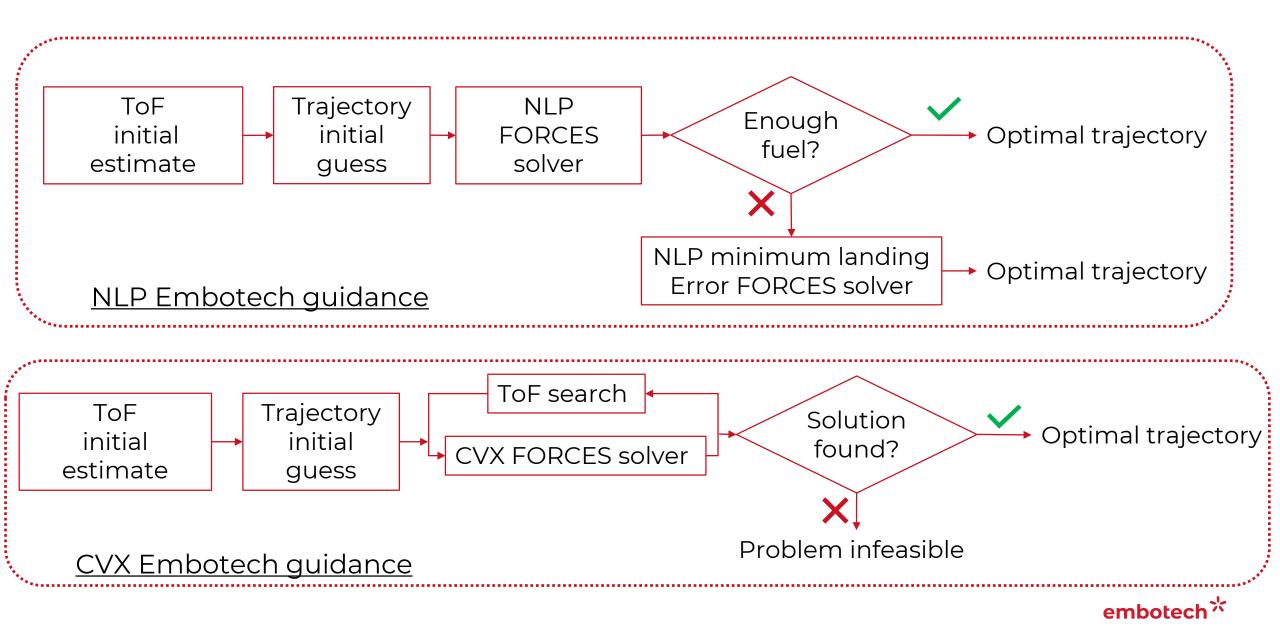
subject to:

	Boundary Conditions		
Minimize fuel consumption	$\overline{m(t_0)} = m_0$	(2)	
	$\mathbf{r}_{\mathcal{I}}(t_0) = \mathbf{r}_{\mathcal{I},0} \qquad \qquad \ \mathbf{r}_{\mathcal{I}}(t_f) - \mathbf{r}_{\mathcal{I},f}\ \le r_{tol}$	(3)	
or	$\dot{\mathbf{r}}_{\mathcal{I}}(t_0) = \dot{\mathbf{r}}_{\mathcal{I},0} \qquad \qquad \ \dot{\mathbf{r}}_{\mathcal{I}}(t_f) - \dot{\mathbf{r}}_{\mathcal{I},f}\ \le \dot{r}_{tol}$	(4)	
	Point-mass Dynamics		
Minimize landing error	$\dot{m}(t) = -\alpha \ \mathbf{T}_{\mathcal{B}}(t)\ $		
	$\ddot{\mathbf{r}}_{\mathcal{I}}(t) = rac{1}{m(t)} \mathbf{F}_{\mathcal{I}}(t) + \mathbf{g}_{\mathcal{I}}$		
	<u>State Constraints</u>		
	$\mathbf{e}_1 \cdot (\mathbf{r}_{\mathcal{I}}(t) - \mathbf{r}_{\mathcal{I}}(t_{0,f})) \ge \tan(\gamma) \parallel [\mathbf{e}_2 \ \mathbf{e}_3] \cdot (\mathbf{r}_{\mathcal{I}}(t) - \mathbf{r}_{\mathcal{I}}(t_{0,f})) \parallel$	(7)	
	$\ \dot{\mathbf{r}}_{\mathcal{I}}(t)\ \le v_{max} + \eta(t)$		
lope constraint	$\eta(t) \geq 0$	(9)	
	<u>Control Constraints</u>		
/	$0 \le T_{min} \le \ \mathbf{T}_{\mathcal{B}}(t)\ \le T_{max}$	(10)	
	$\dot{T}_{min} \leq \dot{\mathbf{T}}_{\mathcal{B}}(t) \leq \dot{T}_{max}$		
	$\mathbf{e}_1 \cdot \mathbf{T}_{\mathcal{B}}(t) \ge \cos(\theta_{max}) \ \mathbf{T}_{\mathcal{B}}(t)\ $	(12)	
γ	$\mathbf{e}_1 \cdot \mathbf{T}_{\mathcal{B}}(t)(1+\nu_D) \le T_{max}(1-\mathbf{e}_1 \cdot \mathbf{r}_{\mathcal{I}}(t)\beta)$	(13)	
		1	

Up, Glideslope constraint

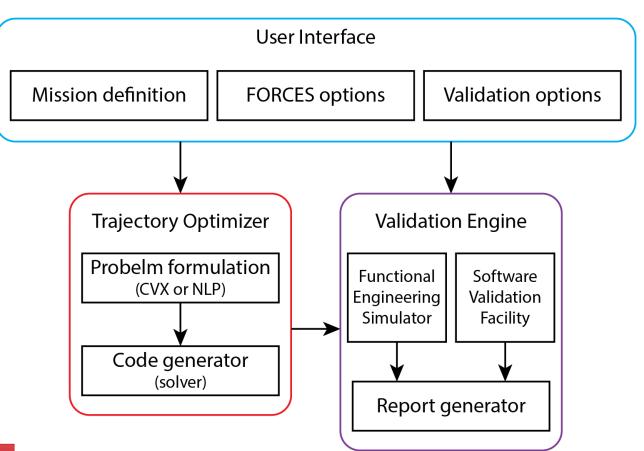
East

OPTIMAL GUIDANCE GUIDANCE



SOFTWARE FRAMEWORK

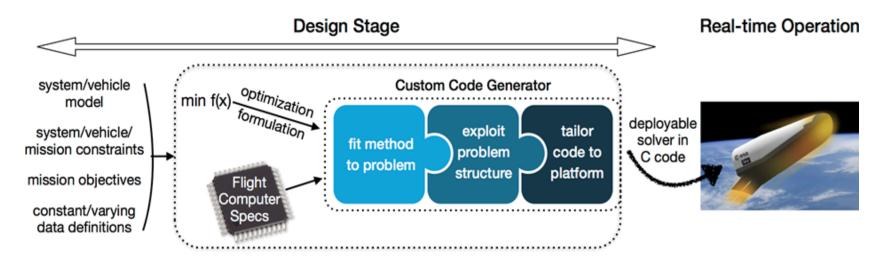
- A unifying framework designed to extensively evaluate and analyze the guidance and control performance
- Completely modular and extendable architecture
- Matlab/Simulink interface
- Support for automatic code generation and deployment on embedded platforms.



The generated C is embeddable on-board as part of the real-time flight code

FORCES PRO Concept

- State-of-the-art client/server code generation system for optimization solvers
- C code tailored for deployment on embedded systems
- Uses only static memory allocation
- No dependency on external libraries
- MISRA C compliant
- Wide range of algorithmic options for LPs, QPs, QCQPs, SOCPs, NLPs and MI-NLPs
- Developed and professionally maintained by embotech AG



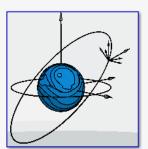


FUNCTIONAL ENGINEERING SIMULATOR (DTV)





Software_Subsystems



Axes_Transformations

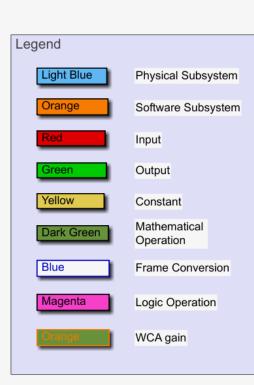


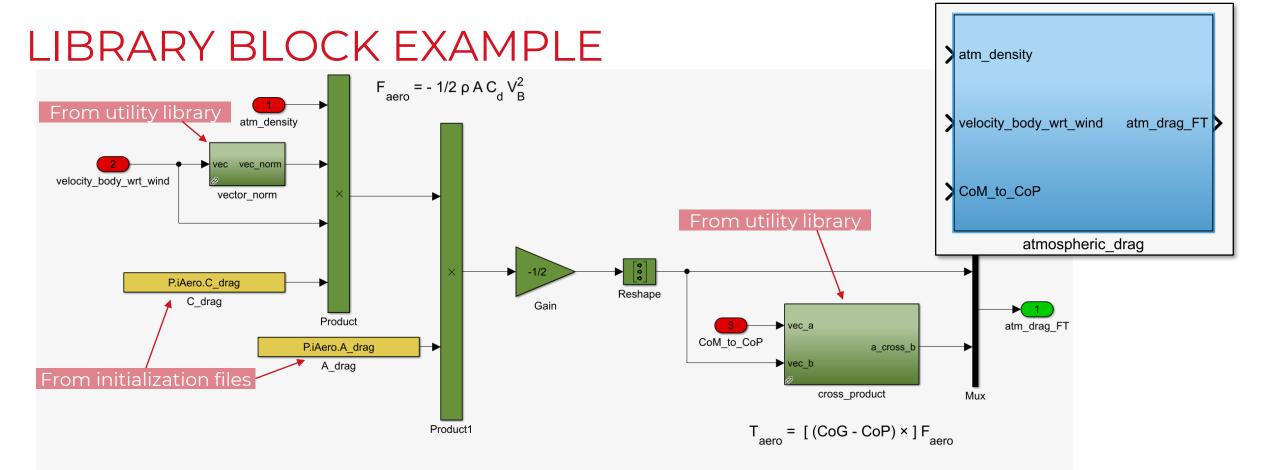
Utility

An expandable simulation library built for INCAS' DTV

Library blocks

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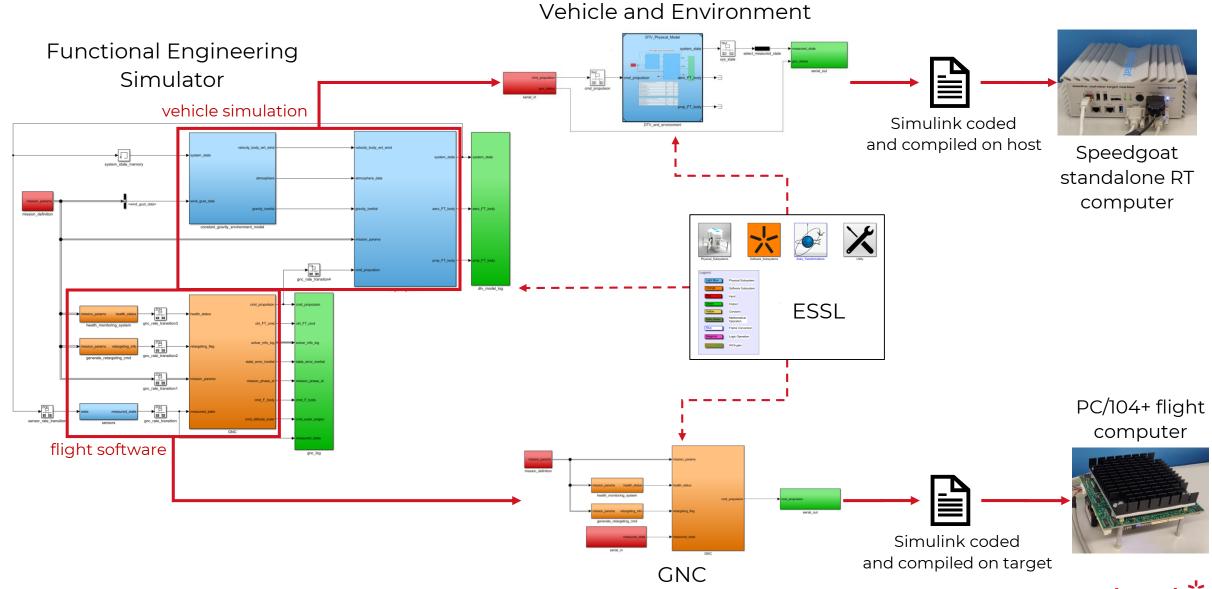
Input	Units	Dimension
Atmosphere Density	kg/m^3	1
Velocity wrt Wind (body)	m/s	3
Attitude Quaternion	-	4
Lever Arm (CoG - CoP)	m	3

Output	Units	Dimension	
Aerodynamic Drag Force (body)	Ν	3	
Aerodynamic Torques (body)	N*m	3	

Parameters	Units	Dimension
Drag Coefficient	-	1
Cross Sectional Area	m^2	1



SIMULATION ENVIRONMENTS



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SIMULATION EXAMPLE

CPU	Median [s]	Max [s]	Min [s]	10
i7 8550U @ 1.8	0.07	0.15	0.04	8 6 4 1 4
Atom E3845 @ 1.9	0.25	0.55	0.19	2

1. Nominal end-to-end mission

100

90

80

70 -

60

40

30

20

10 -

0

60

40

20

0

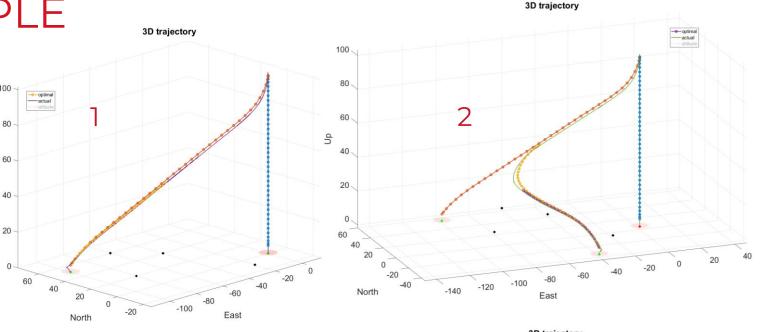
North

-20

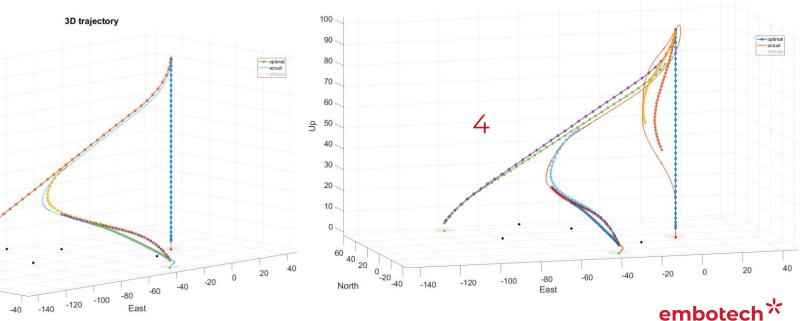
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3

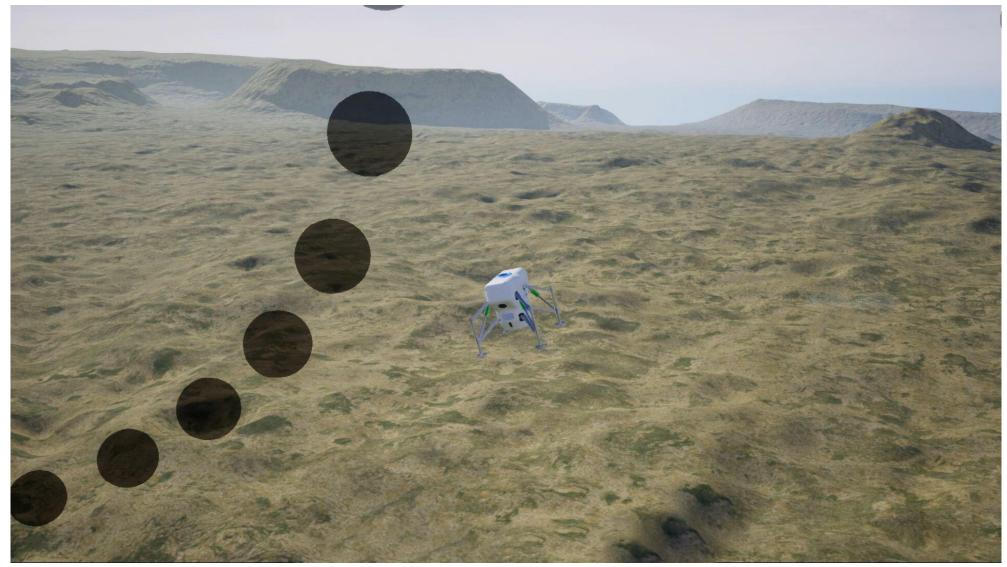
- 2. Mid-flight retargeting
- 3. Engine fault
- 4. Wind on ascent
- Takeoff pad
- Landing pad
- Emergency pad
 Glideslope



3D trajectory



END-TO-END VTOL MISSION



https://youtu.be/srjEs1iFxl8

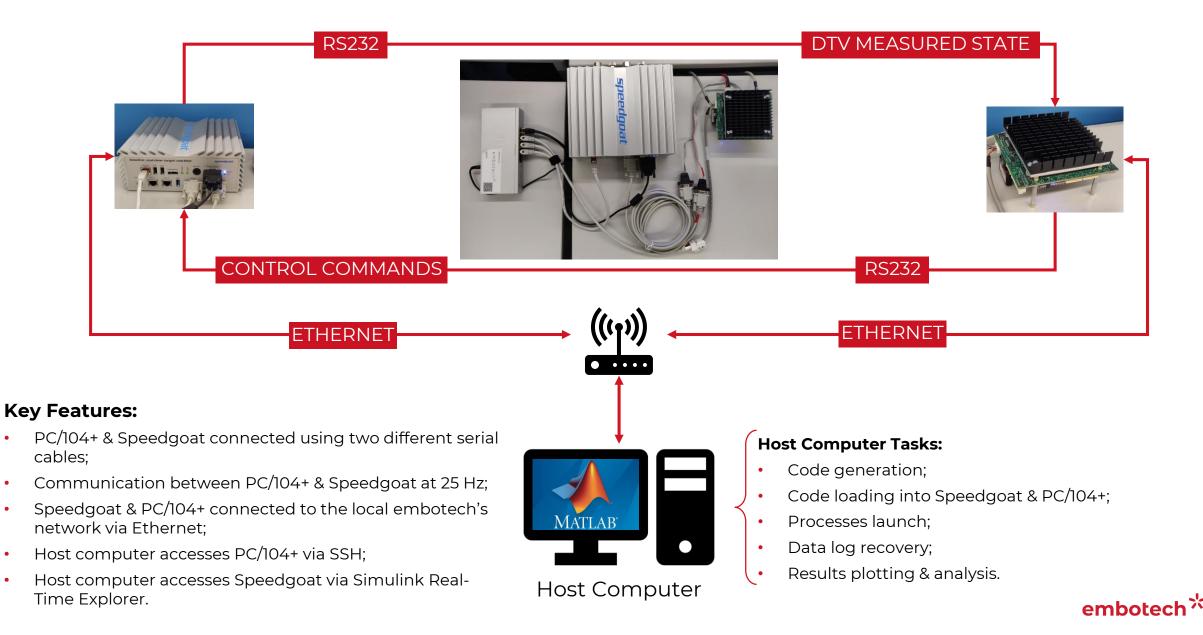


SOFTWARE VALIDATION FACILITY

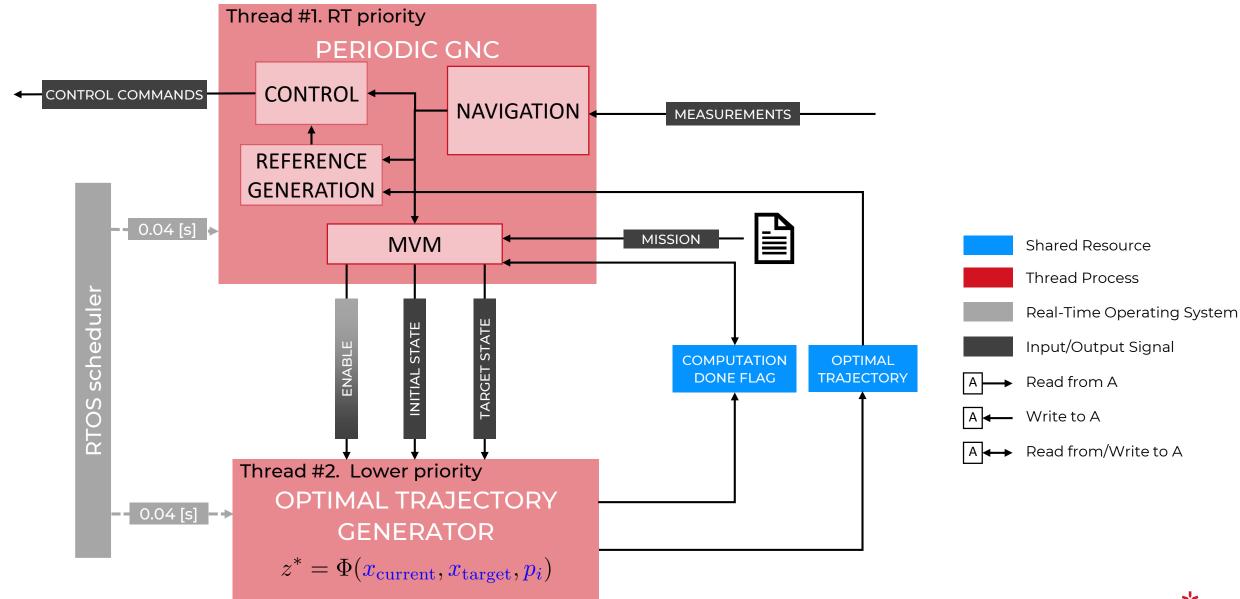
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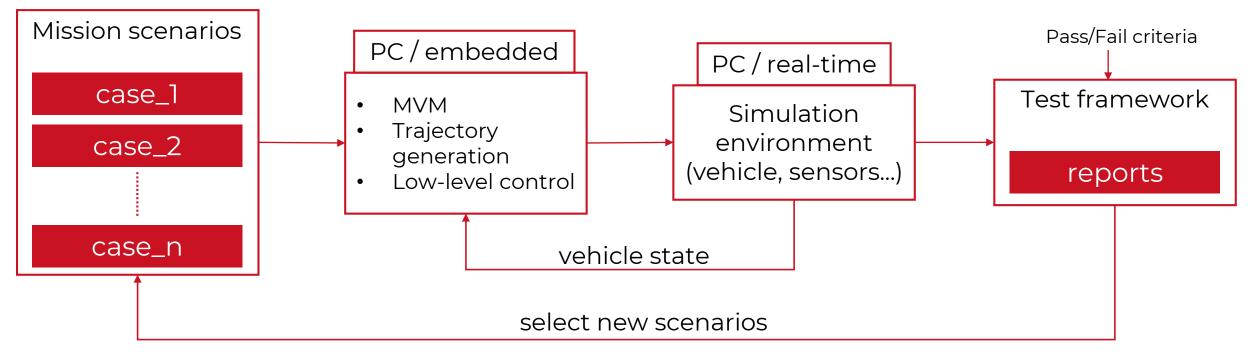
REAL-TIME FLIGHT SOFTWARE



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FLIGHT SOFTWARE QUALIFICATION

- Functional validation campaign
 - 2576 scenarios simulated under *nominal*, *robust* and *fault* conditions
 - Sensitivity analysis w.r.t. noise and dispersion
- Software validation campaign
 - Subset of scenarios necessary for full code coverage



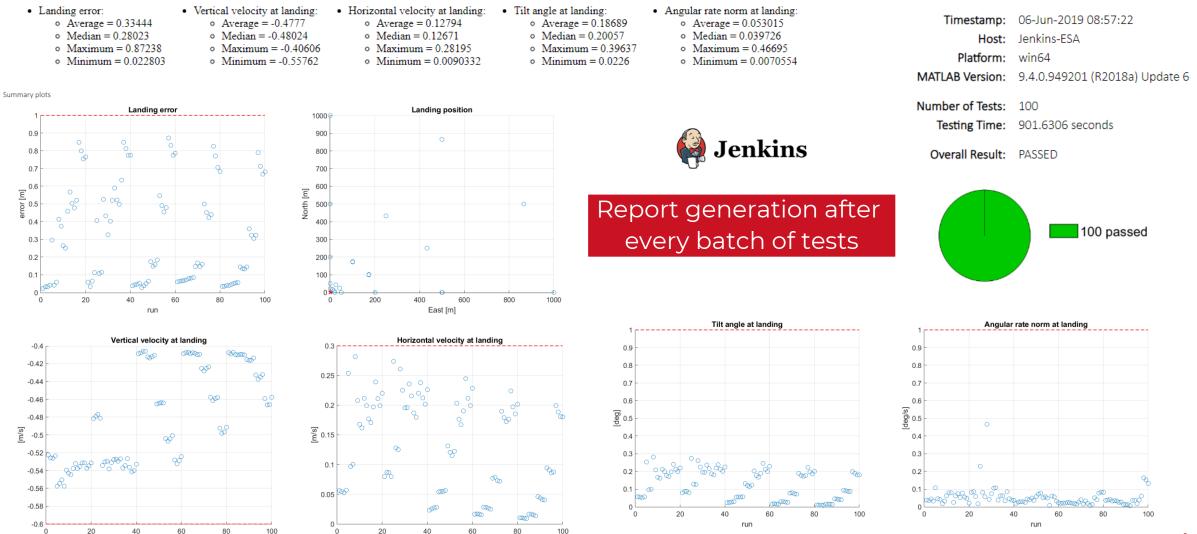


CONTINUOUS INTEGRATION

Summary Test Data

run

Statistical data



run

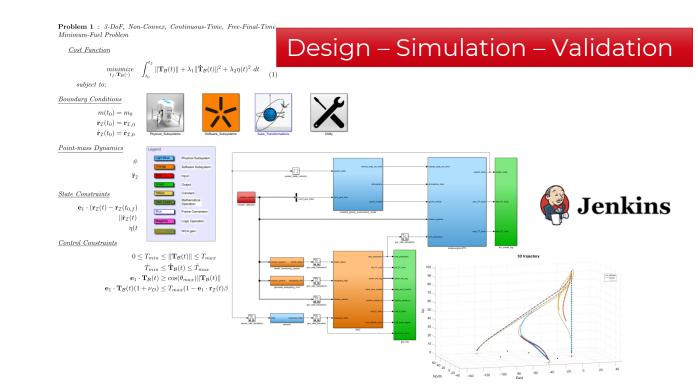


MATLAB[®] Test Report

CONCLUSION



SpaceX





T0+3	T0+6	T0+8	
Preliminary SW Checks	Harwdare Tests	Vehicle Integration	Flight Testing

Flight Testing on INCAS DTV. 03 2019





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