

3D Internal Charging Analysis in FASTRAD®

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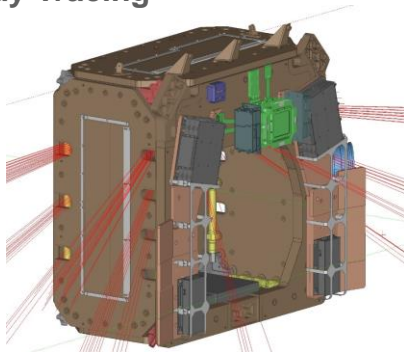
TRAD Tests & Radiations, Labège, France

28th SPINE meeting: 8th-10th of June 2021, ESA/ESTEC, The Netherlands

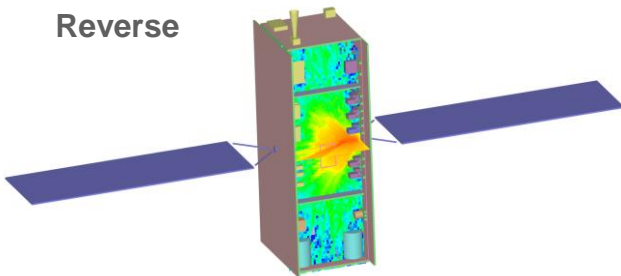
- Introduction to FASTRAD
 - ▶ A radiation analysis tool
- First level analysis: current density
 - ▶ Identify the critical parts
- Second level analysis: electric field
 - ▶ Example on a 25-pins connector
- 3D comparison
 - ▶ Coaxial cable
- Conclusion

**Dose calculation (TID & TNID)
based on two methods:**

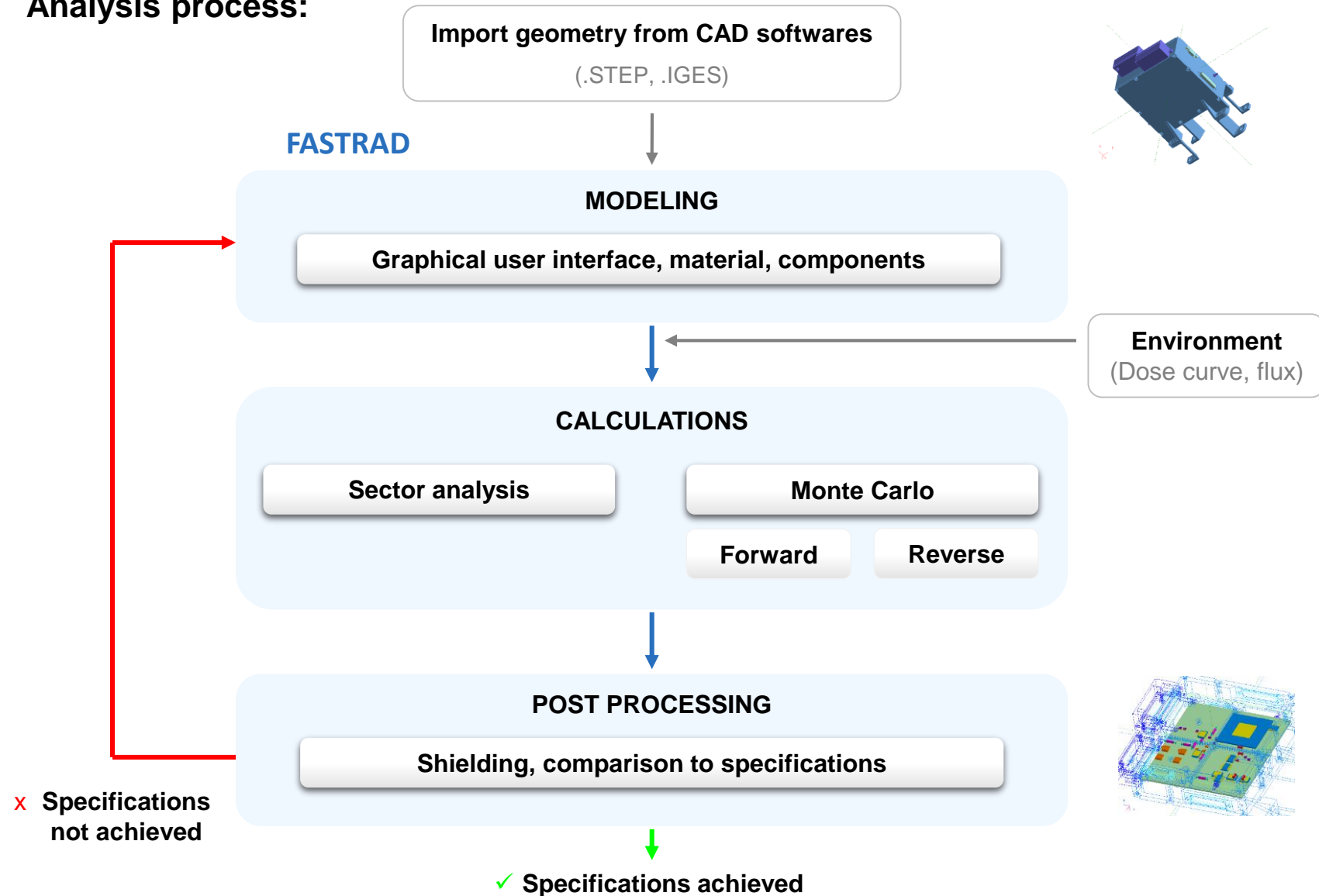
- **Sector analysis**
Ray-Tracing



- **Particle transport based on
GEANT4: Monte Carlo**
Forward
Reverse



Analysis process:

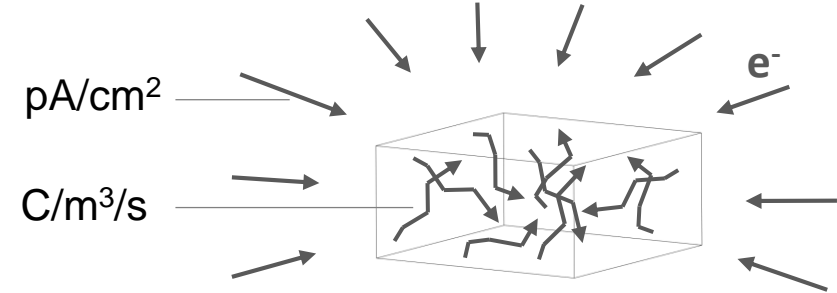


First level analysis: current density

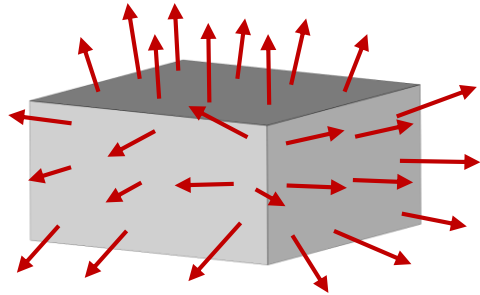
Inputs

- Worst case electron flux (short term average).
- Select a sensitive volume in the 3D model.

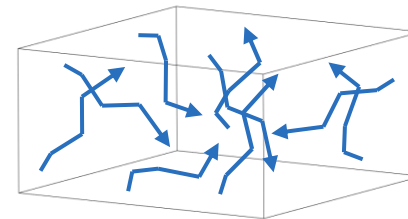
Calculation method



From the surface to the outside:
Reverse Monte-Carlo

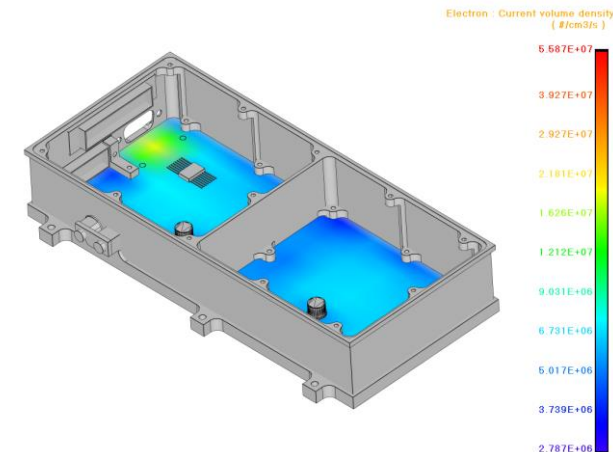


From the surface to the interior:
Forward Monte-Carlo



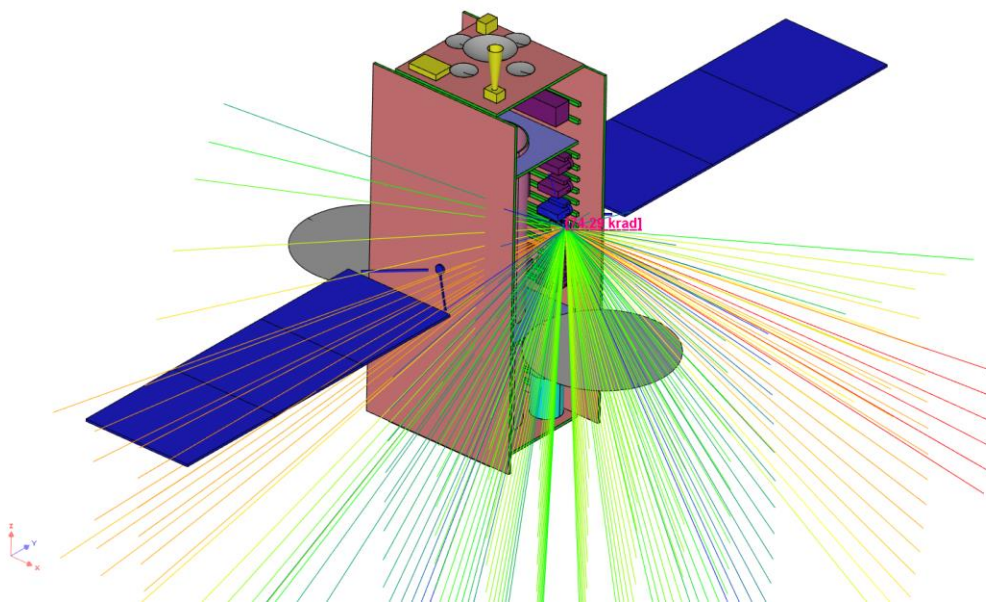
Outputs

- Current density (pA/cm^2) of the incident electrons at the surface of the sensitive volume.
- Charge deposition rate ($\text{C}/\text{m}^3/\text{s}$) inside the sensitive volume.

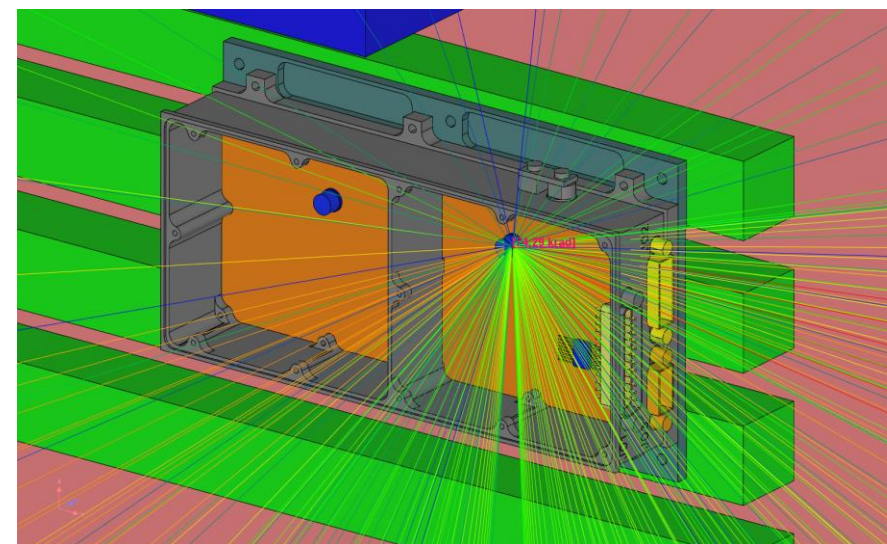


- Geometry model

- ◆ Use the same geometry model as for the TID/TNID analysis.
- ◆ Example: geometry from the ray tracing analysis.



Ray tracing view

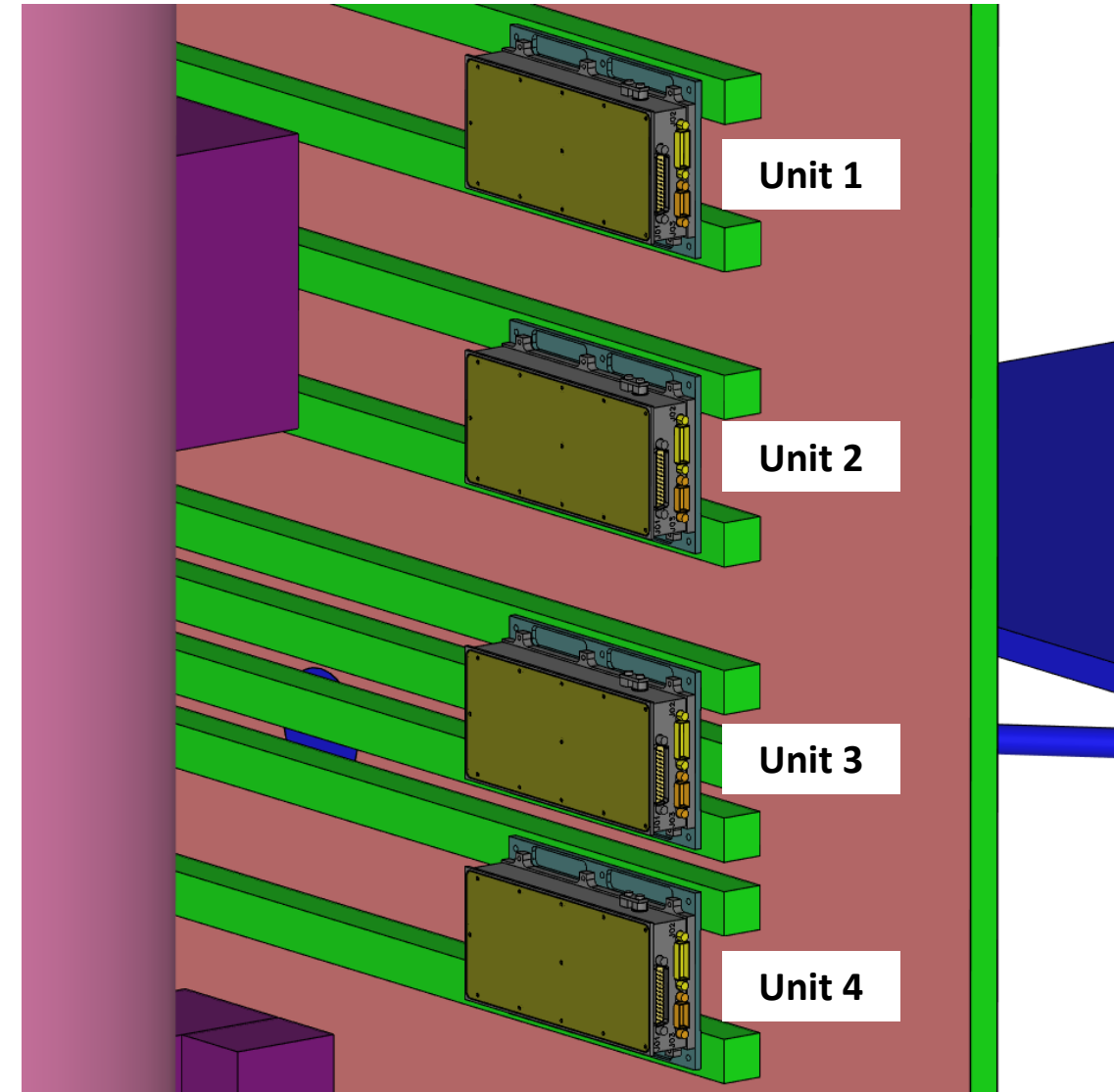


Ray tracing view

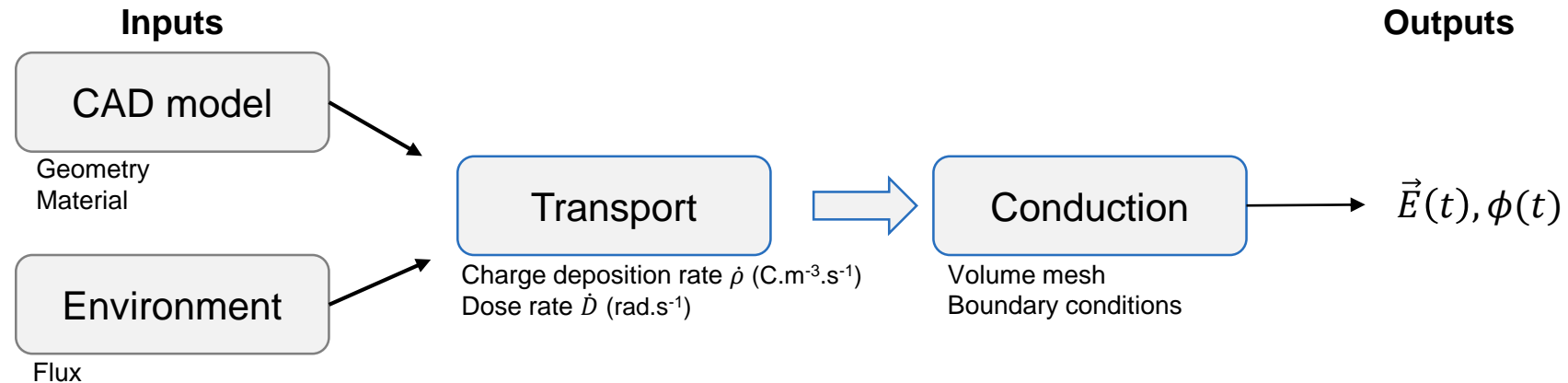
- Identify the critical parts: Reverse Monte Carlo method

- Run a Reverse Monte Carlo transport calculation on every critical part among connectors, PCBs, cables.
- Calculation of the incident current density
- Display the current density and compare to the ECSS threshold [ECSS-E-ST-20-06_0070118]
 - If $T > 25^{\circ}\text{C}$: $J_{\text{max}} = 0.10 \text{ pA/cm}^2$
 - If $T < 25^{\circ}\text{C}$: $J_{\text{max}} = 0.02 \text{ pA/cm}^2$

Unit	Part	Current density	Calculate Electric Field ?
1	Connector	$J > 0.02 \text{ pA/cm}^2$	YES
1	PCB	$J < 0.02 \text{ pA/cm}^2$	NO
2	Connector	$J < 0.02 \text{ pA/cm}^2$	NO
2	PCB	$J < 0.02 \text{ pA/cm}^2$	NO
3	Connector	$J < 0.02 \text{ pA/cm}^2$	NO
3	PCB	$J < 0.02 \text{ pA/cm}^2$	NO
4	Connector	$J > 0.02 \text{ pA/cm}^2$	YES
4	PCB	$J > 0.02 \text{ pA/cm}^2$	YES



- General approach for the ESD risk assessment:



- Starting from the charge deposition $\dot{\rho}$ and the dose rate \dot{D} , the potential is solved in 3D.

Gauss equation

$$-\nabla \epsilon \nabla \phi = \rho$$

Continuity equation

$$\frac{\partial \rho}{\partial t} + \nabla \vec{J} = \dot{\rho}$$

Ohm's law

$$\vec{J} = -\sigma \nabla \phi$$

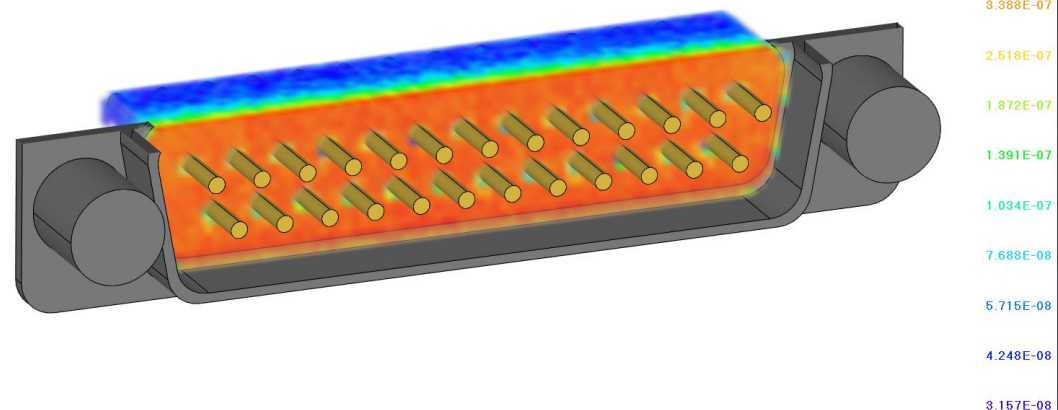
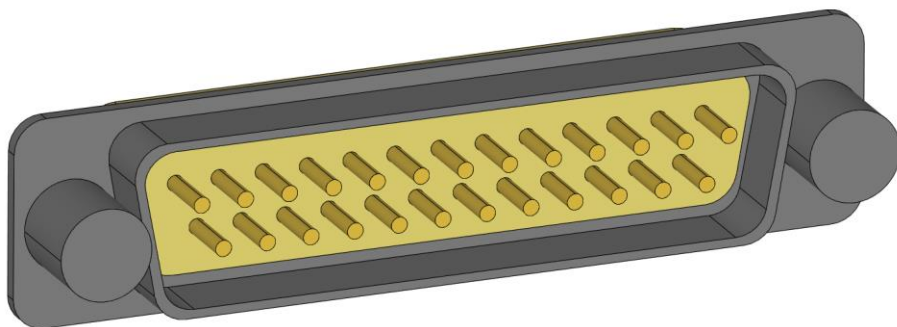
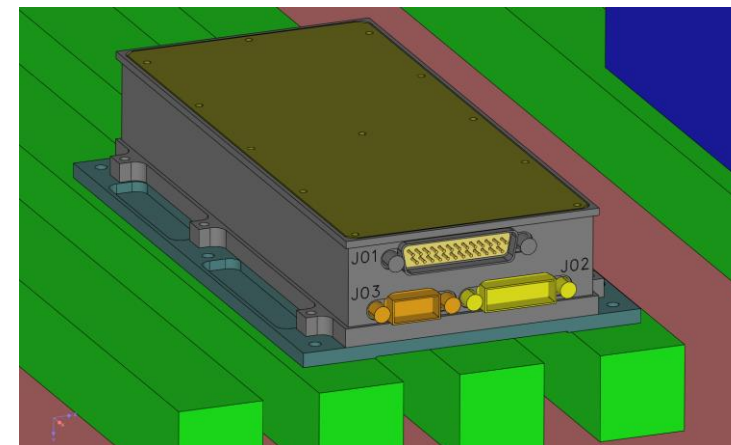
Differential equation for the potential

$$-\nabla \epsilon \nabla \frac{d\phi}{dt} - \nabla \sigma \nabla \phi = \dot{\rho}$$

Outputs

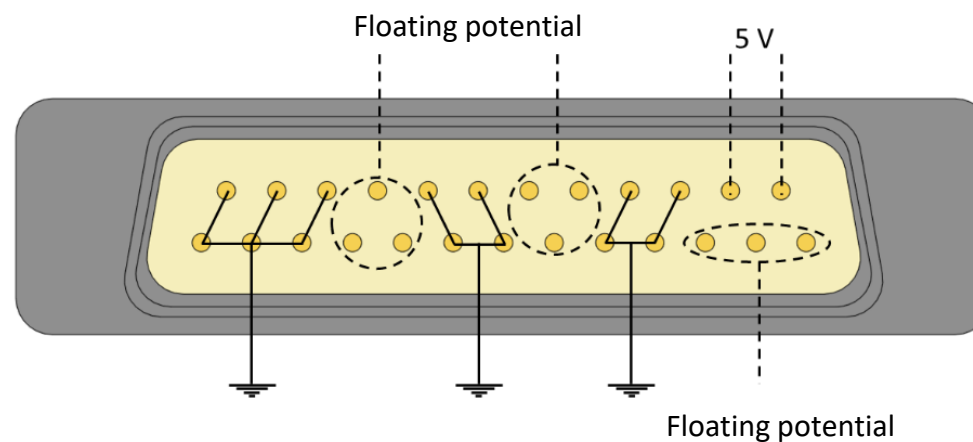
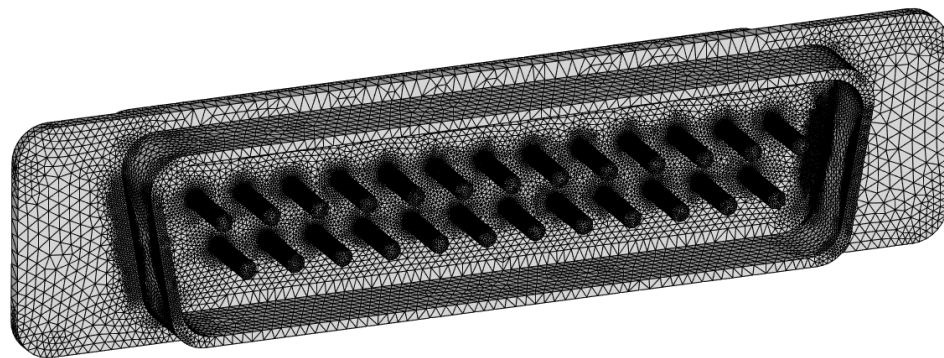
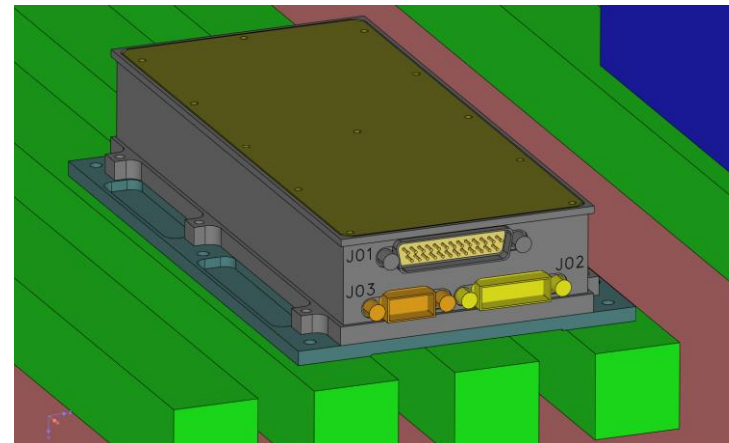
- $\phi(\vec{r}, t)$
- $\vec{E}(\vec{r}, t) = -\nabla \phi$

- Step 1: charge and energy deposition
 - Both Forward and Reverse Monte Carlo methods can be used.
- Example:
 - Connector: 25 pins
 - Complete geometry model: satellite geometry + unit geometry
 - Particle transport method: Reverse Monte Carlo



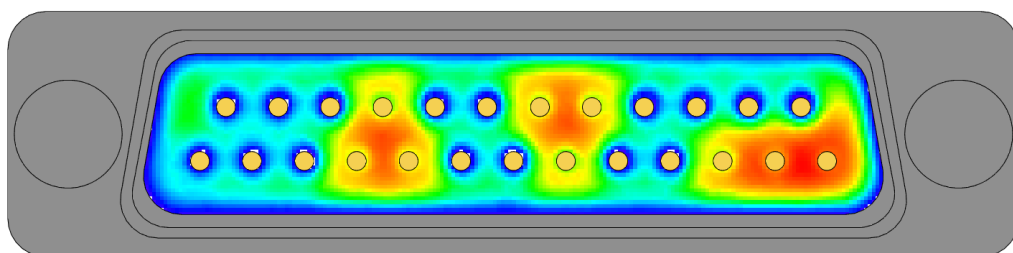
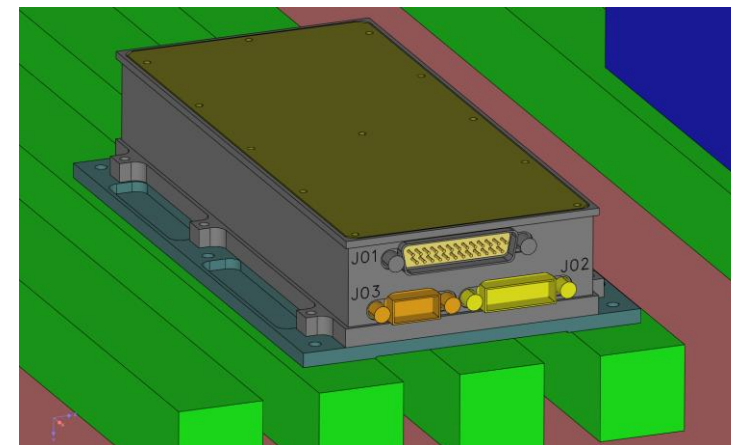
■ Step 2: mesh and boundary conditions

- Create the volume mesh
- Display and refine the volume mesh
- Assign boundary conditions

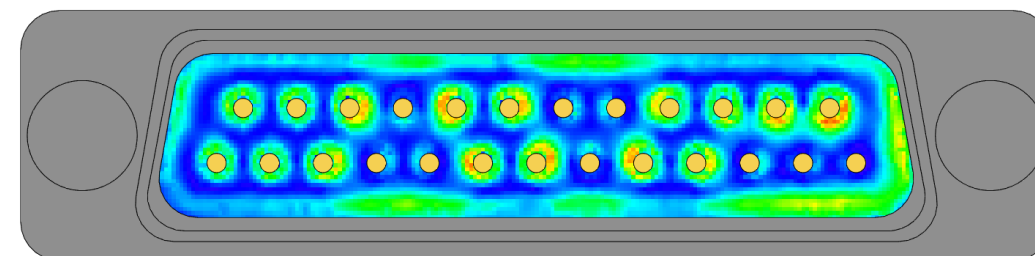


Step 3: electric field calculation

- Define the duration of irradiation, e.g. 24h
- Define the time step
- Run the electric field calculation
- Display the potential and electric field evolution



Potential t = 24 h
 $\phi_{\max} = 1\,414\text{ V}$

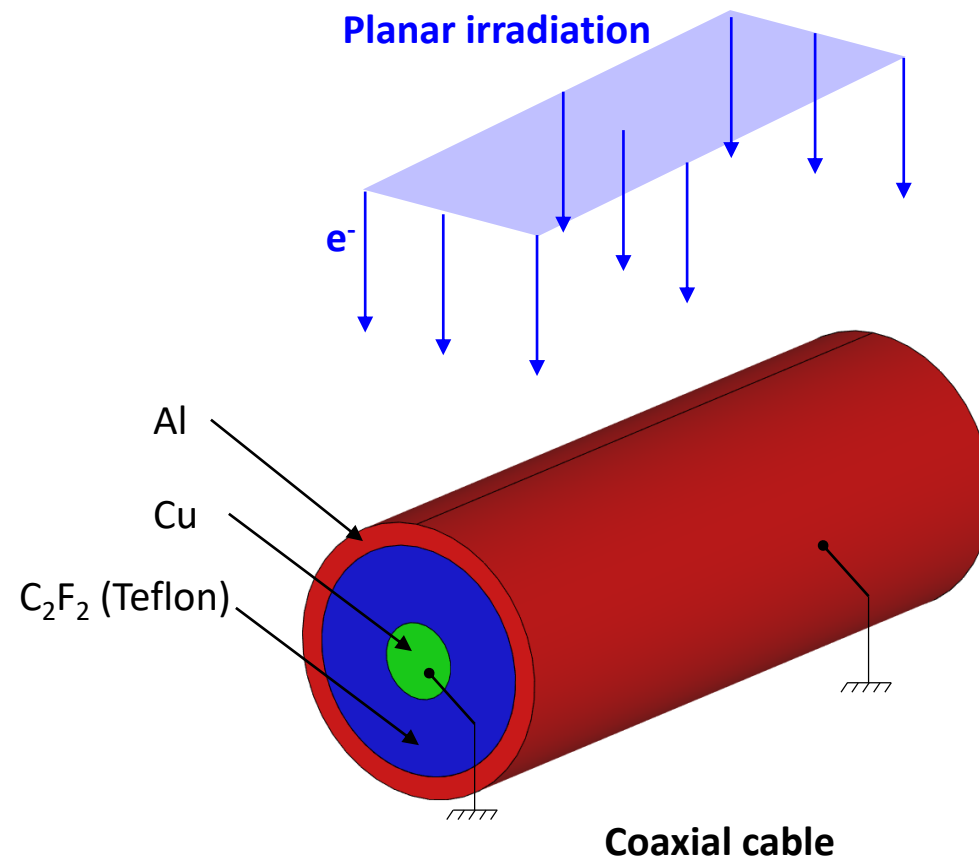


Electric field t = 24 h
 $E_{\max} = 1.3\text{ MV/m}$

- 3D comparison by using a coaxial cable.
- The comparison is made with 3DNUMIT [1].
 - Coaxial cable: Al, Cu and Teflon
 - Planar irradiation for 400 h
 - Inner conductor and shielding are grounded

Dielectric properties	Teflon
Relative permittivity	2.15
Bulk conductivity ($\Omega^{-1} \cdot \text{m}^{-1}$)	2.60×10^{-19}
Radiation induced conductivity ($\Omega^{-1} \cdot \text{m}^{-1} \cdot \text{rad}^{-1} \cdot \text{s}^{\Delta}$)	6.10×10^{-16}
Δ	1

[1] "Benchmarking internal dielectric charging simulation platforms" Likar et al. , ASEC 2019

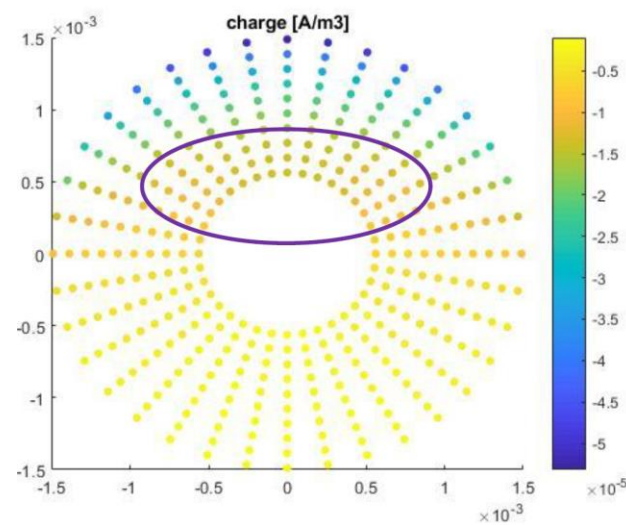


■ Charge & Energy deposition

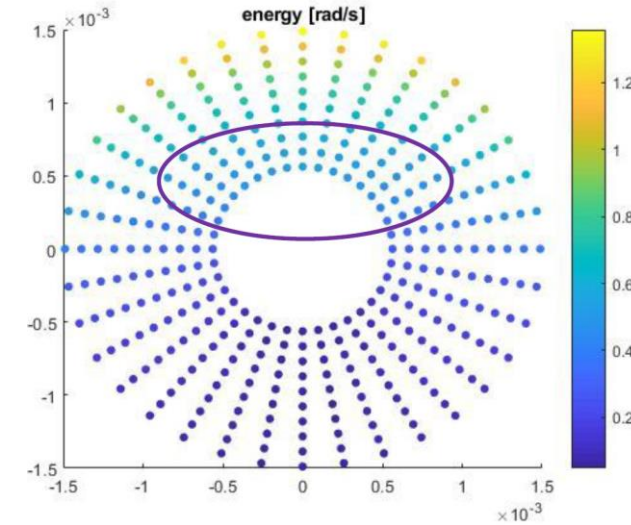
- Good agreement with distribution and magnitudes.
- Subtle differences in magnitudes (different particle transport codes, different meshing)

3DNUMIT

Max: $5.2 \times 10^{-5} \text{ A/m}^3$

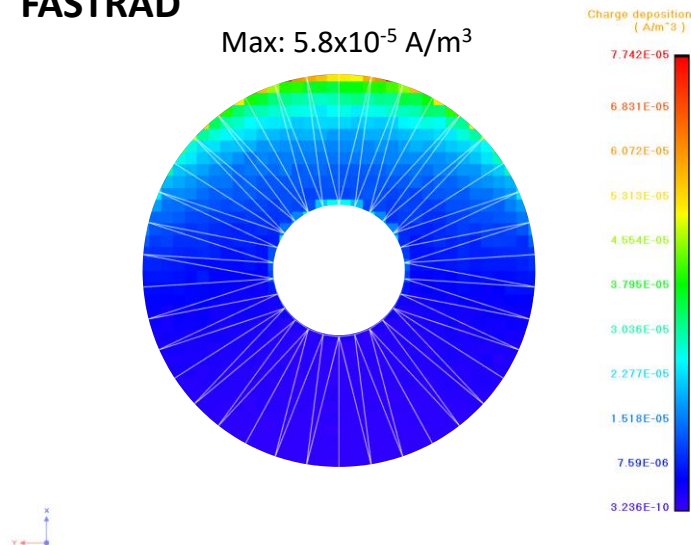


Max: 1.30 rad/s

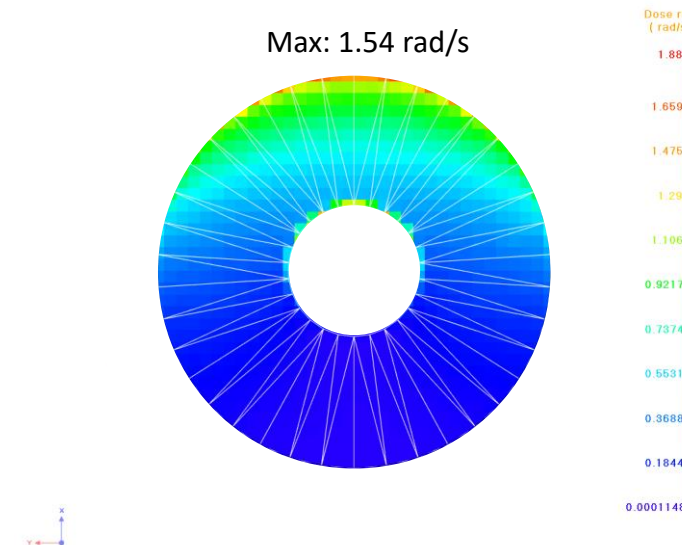


FASTRAD

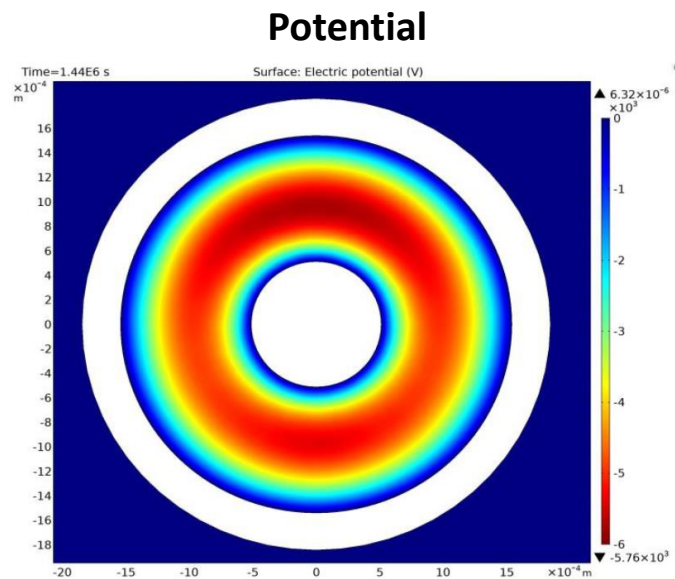
Max: $5.8 \times 10^{-5} \text{ A/m}^3$



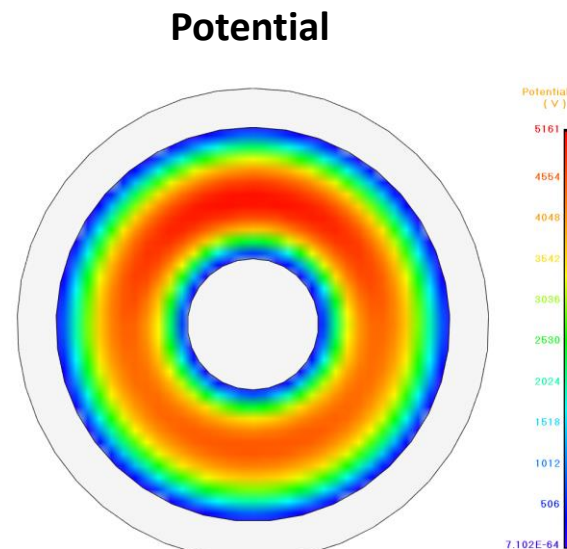
Max: 1.54 rad/s



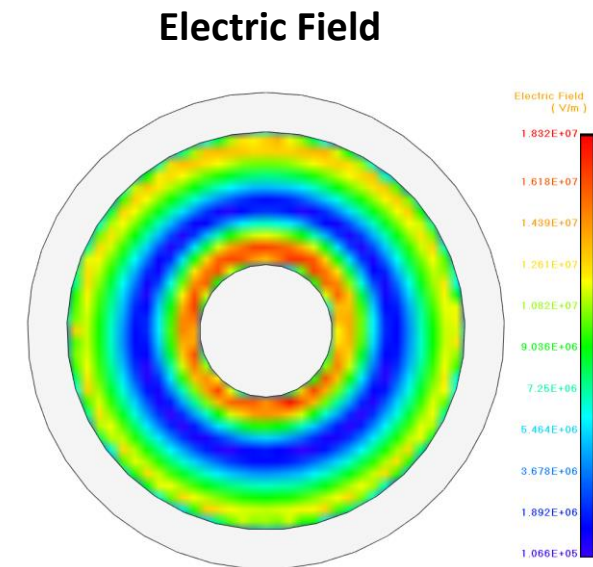
- Potential after 400 h irradiation
 - Good agreement of potential for space distribution and value
 - The maximum potential is -15% lower than 3DNUMIT



3DNUMIT
 $\phi_{\max} = -6\,000\text{ V}$



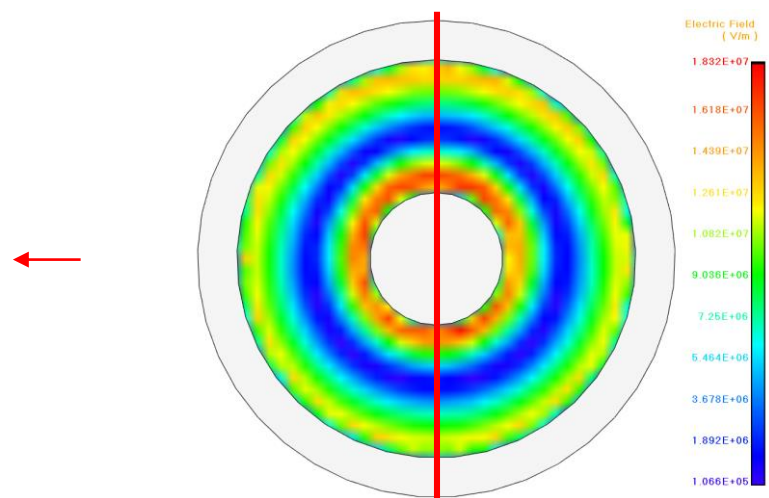
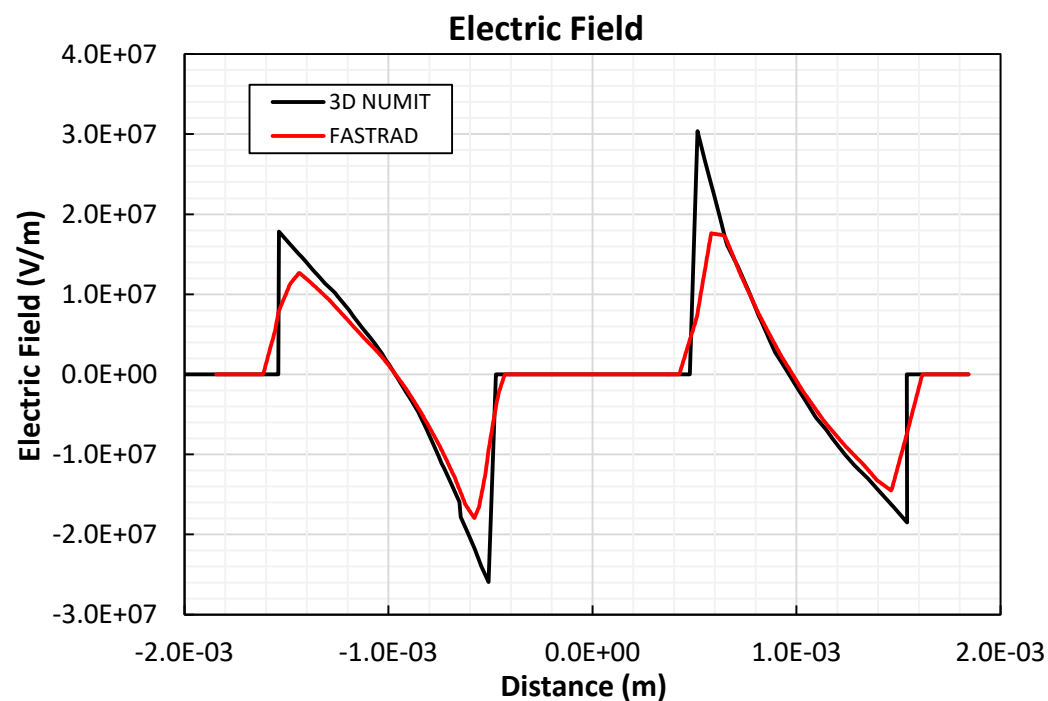
FASTRAD®
 $\phi_{\max} = -5\,161\text{ V}$



FASTRAD®
 $E_{\max} = 18\text{ MV/m}$

■ Electric field after 400 h irradiation

- Good agreement of electric field for space distribution.
- The maximum electric field at the interfaces is lower than 3DNUMIT.
- Maybe due to different interface behavior for the electric field solver in the finite element method.



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 $E_{\max} = 18 \text{ MV/m}$

- Internal charging analysis with geometry coming from the TID analysis.
- Two levels of internal charging analysis in FASTRAD, allowing save time:
 - ✦ First level: electron current density
 - particle transport method: Reverse Monte Carlo can be used
 - comparison to ECSS thresholds
 - identification of critical parts
 - ✦ Second level analysis: electric field calculation
 - Only on critical parts
 - Display potential and electric field evolution
- Validation
 - ✦ Particle transport code, based on Geant4 physics, validated and published [RADECS 2016]
 - ✦ 1D cases have already been used for validation (not shown here)
 - ✦ 3D validation with one case
 - ✦ Additional 3D validations with other tools and experimental data are in progress
- Beta version available June 2021
 - ✦ Official FASTRAD release September 2021

Thank you for your attention