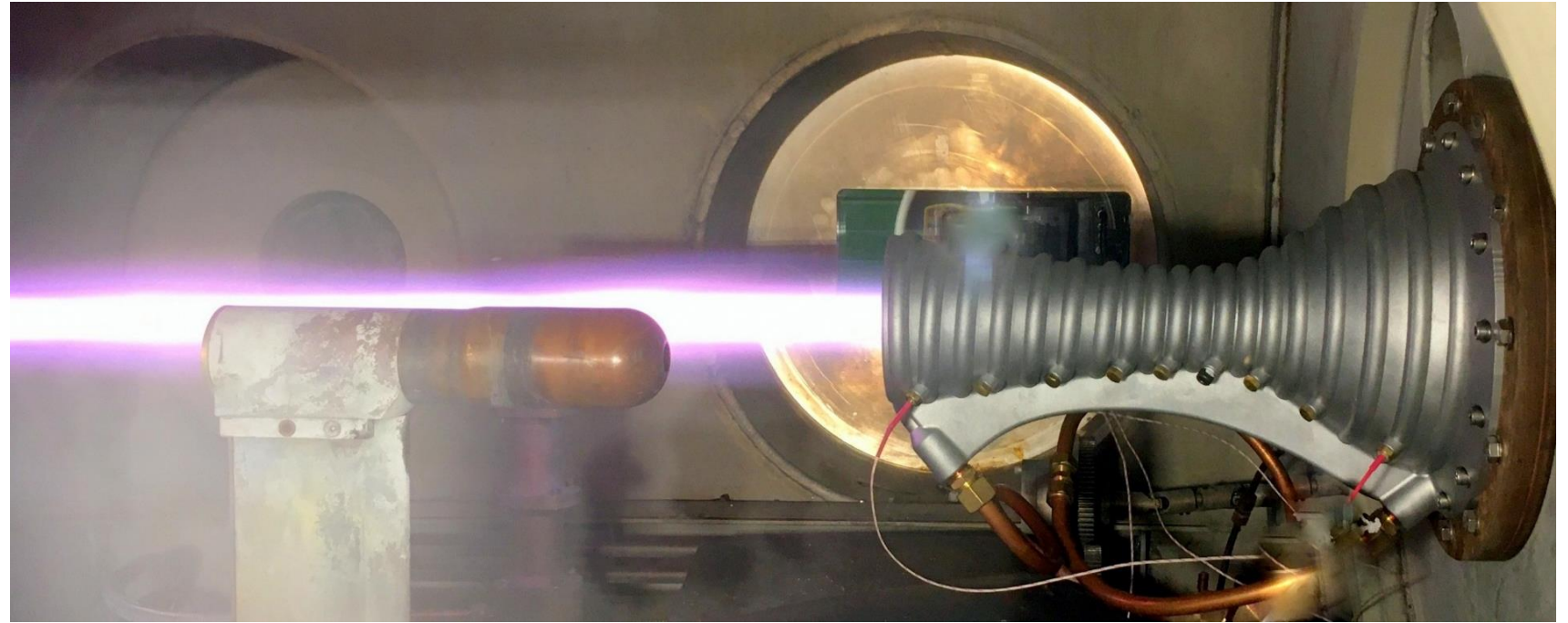


# Advancements in demise testing at VKI: Sub- and supersonic experiments of titanium, Zerodur and quartz



B. Helber, A. Fagnani, A. Turchi, B. Dias, A. Viladegut, L. Sombaert, T. E. Magin, O. Chazot  
von Karman Institute for Fluid Dynamics

P. Schrooyen

Cenaero

L. Walpot

ESA

02 December 2021



# Background: Belgian GSTP

## *Validation of Space Debris Demise Tools using Plasma Wind Tunnel Testing and Numerical Tools*

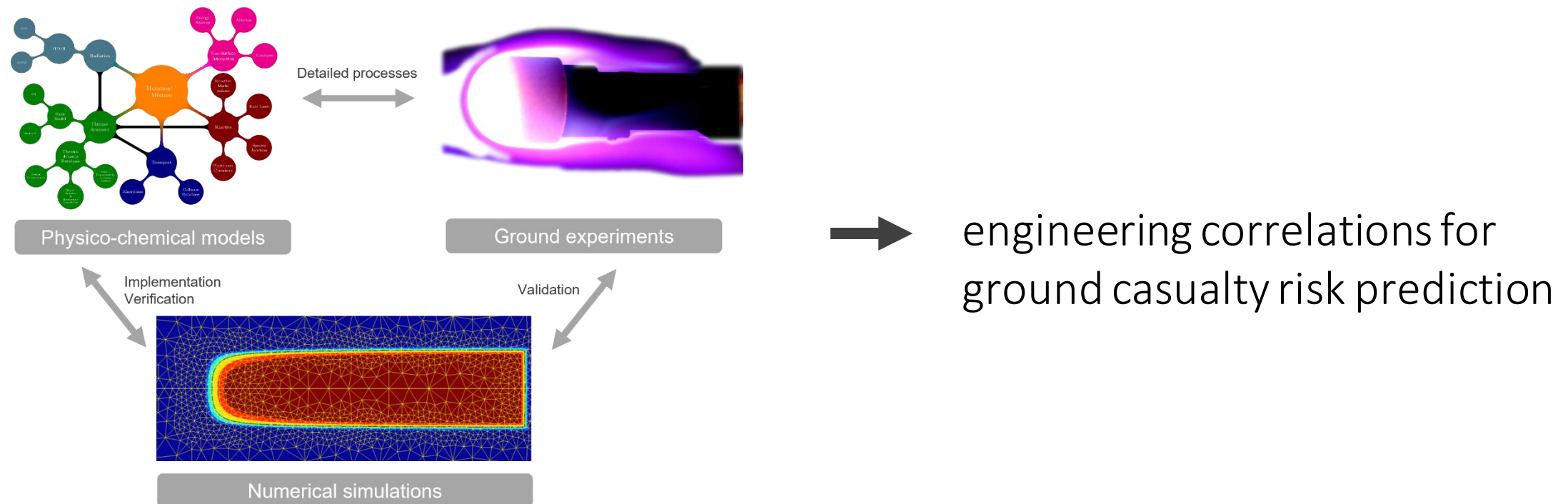
Objectives:

VKI (Plasmatron, Mutation<sup>++</sup>): High-enthalpy experiments of problematic space debris materials

Cenaero (ARGO): High-fidelity models and numerical simulations

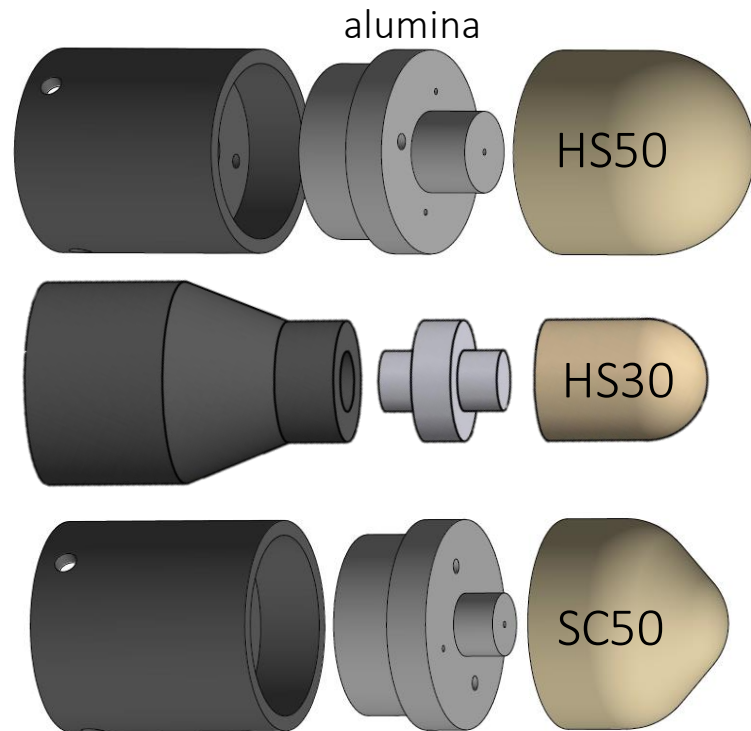
→ strengthening our understanding of demise phenomena

→ produce engineering correlations from high-fidelity simulations



# Background: Extensive sub- and supersonic demise experiments

The variety of materials make their demise prediction difficult



Complicated oxidation mechanisms

More complicated chemistry  
Partial evaporation

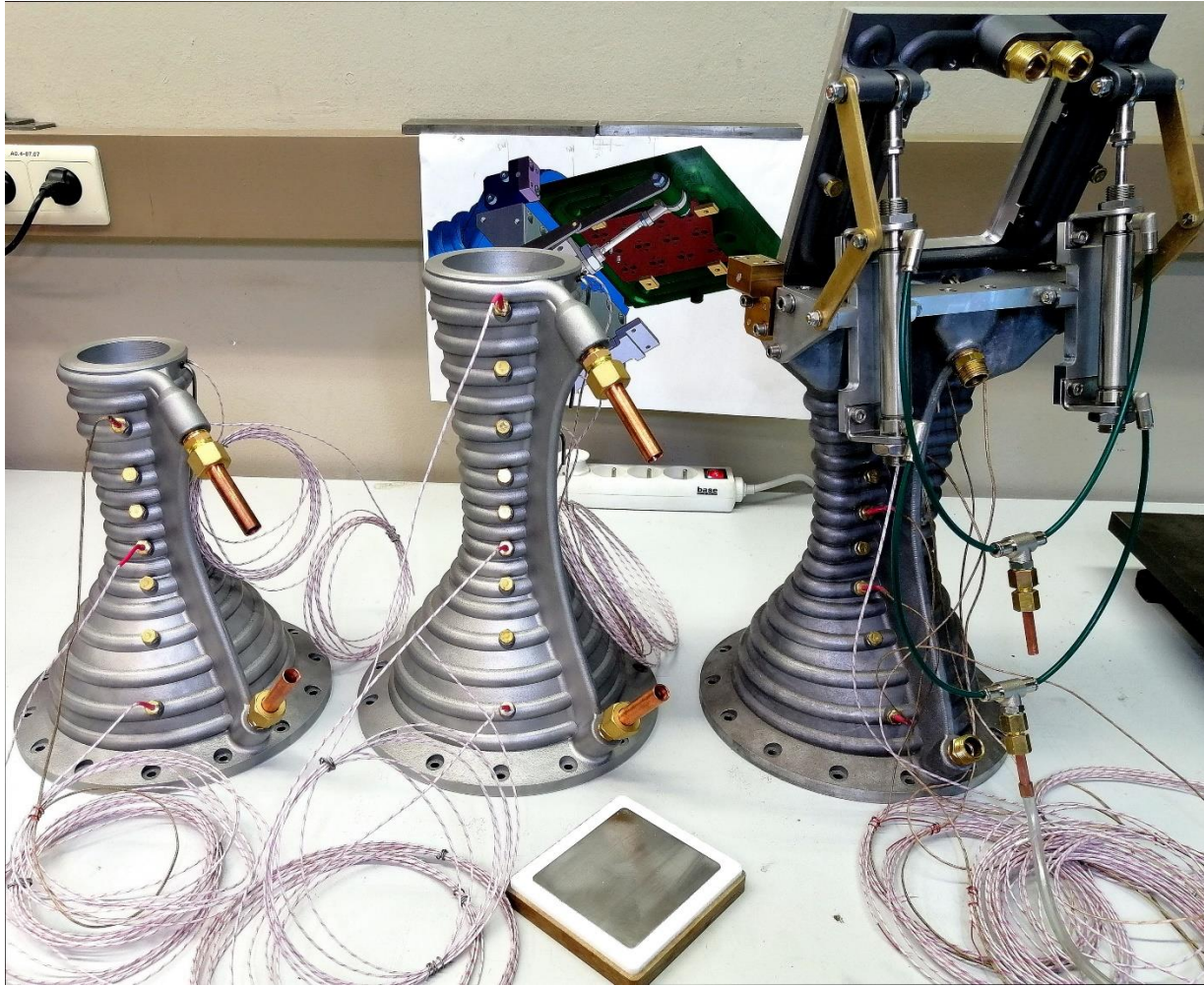
Low  $T_{\text{surface}}$ : no mass removal, validation SEB

High  $T_{\text{surface}}$ : validation evaporation + shear



# Background: Extensive sub- and supersonic demise experiments

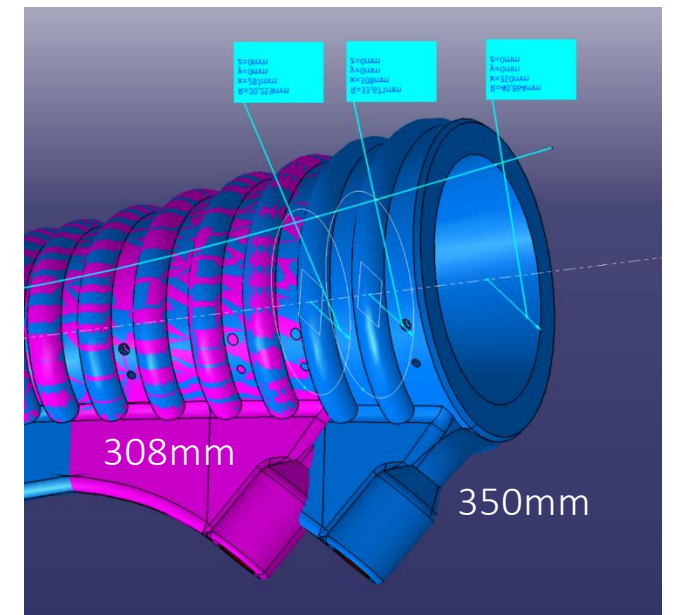
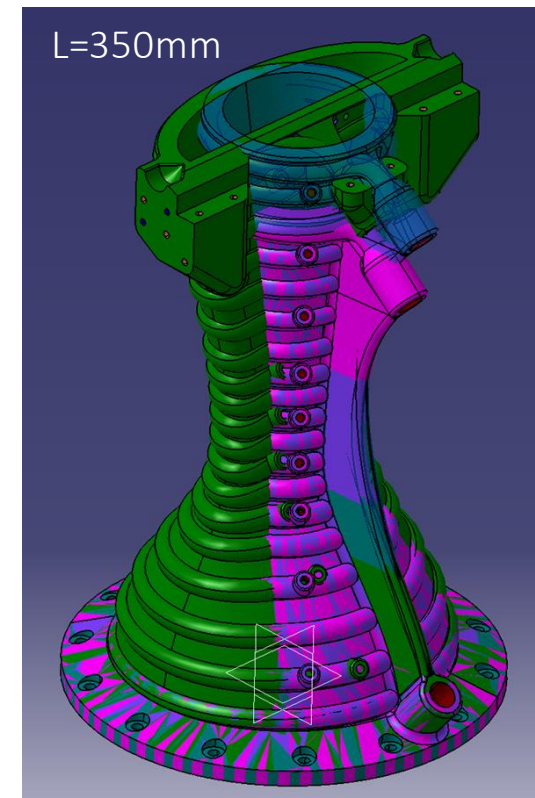
Design and commissioning of conical and semi-elliptical nozzles (additive manufacturing)



identical length, area ratio and exit area for SE and conical nozzle

Identical cooling loop design

Shorter nozzle for less expansion



# Overview

## Experimental methods

Plasmatron facility

Instrumentation setup and new hardware

## Experiments

Quartz

Zerodur

Titanium

Supersonic

## Numerical simulations outlook

Mutation<sup>++</sup>

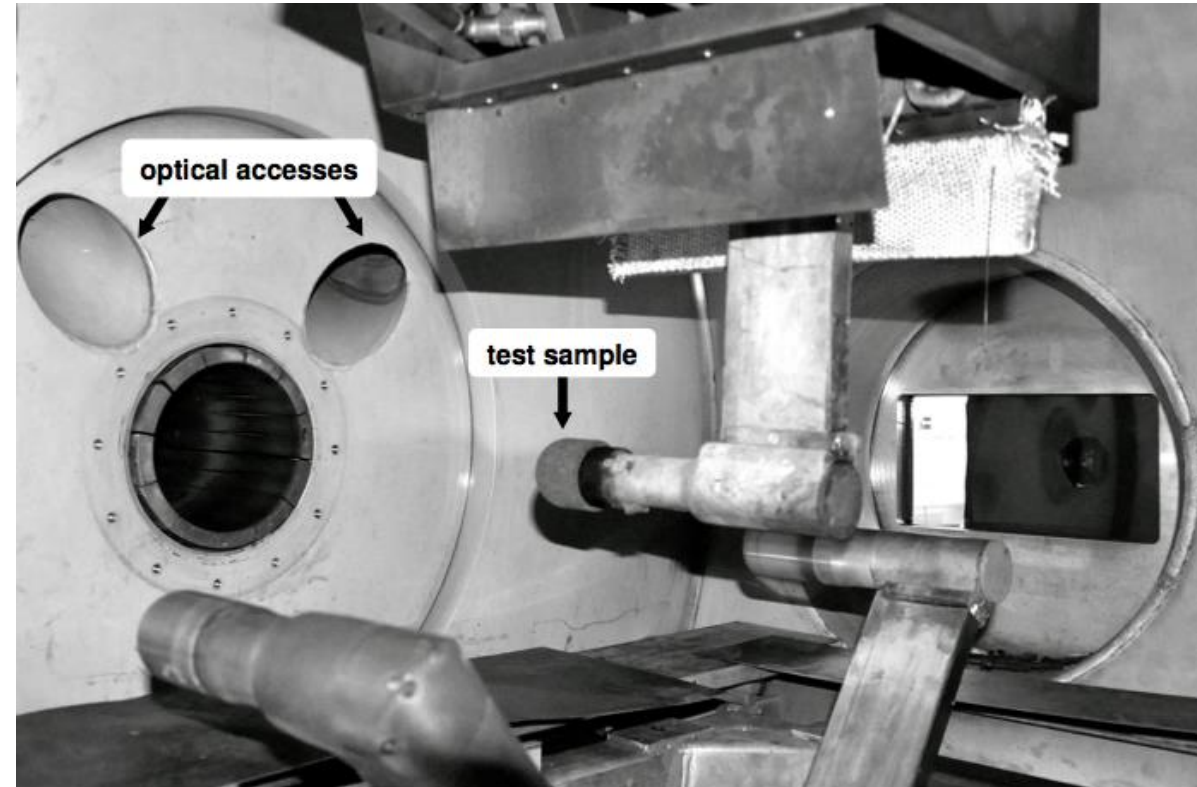
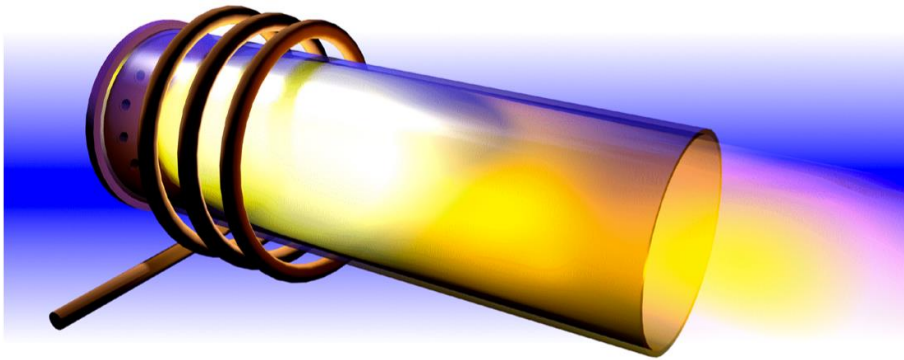
1D-stagnation line code with melting model

High-fidelity *ARGO* simulations



# 1.2 MW Inductively Coupled Plasmatron

A subsonic test bed for re-entry flow reproduction



Gas

air, N<sub>2</sub>, CO<sub>2</sub>, Ar

Power

1.2 MW

Max. heat flux

15 MW/m<sup>2</sup>

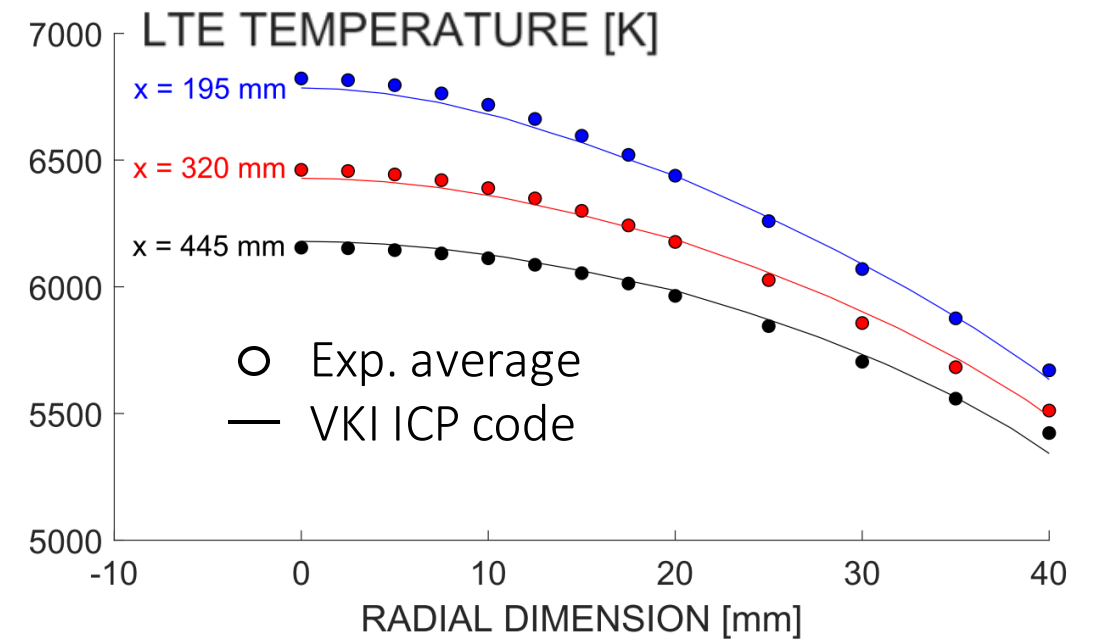
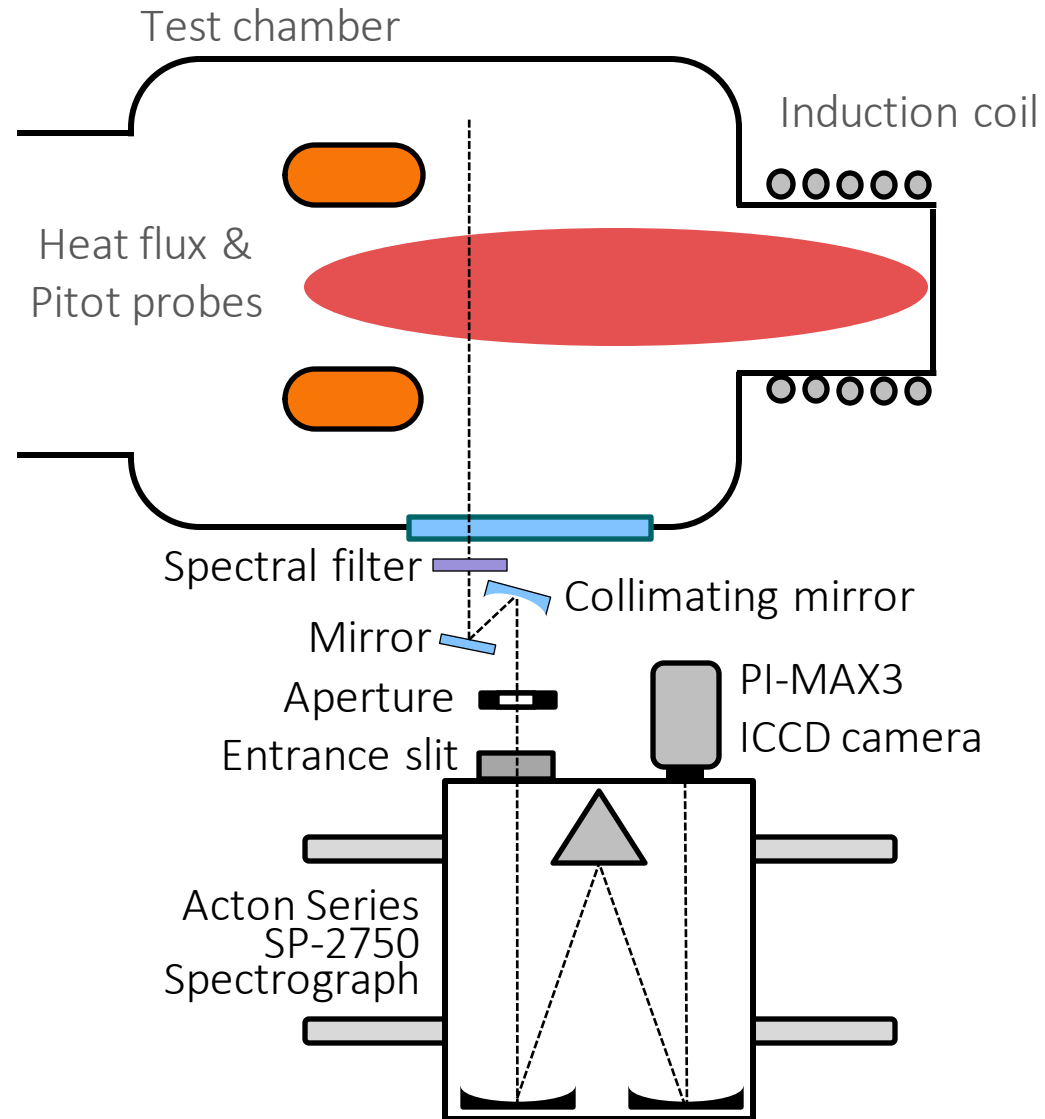
Pressure

10 hPa - 400 hPa



# 1.2 MW Inductively Coupled Plasmatron

Plasma flow characterization by emission spectroscopy

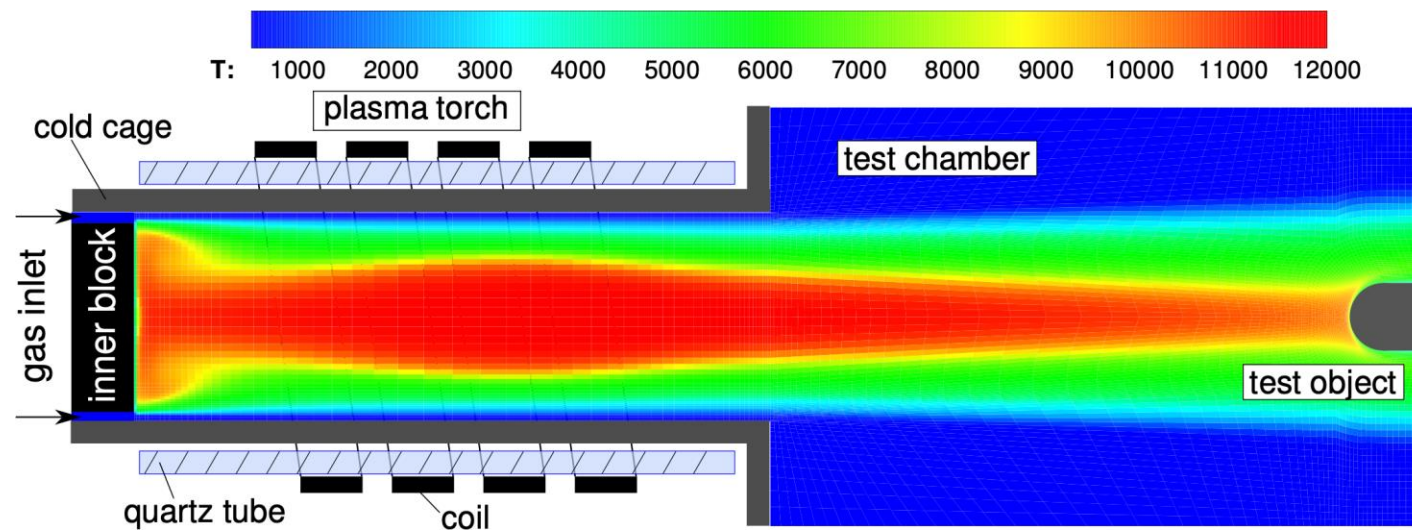


*A. Fagnani et al., AIAA 2020-0382*

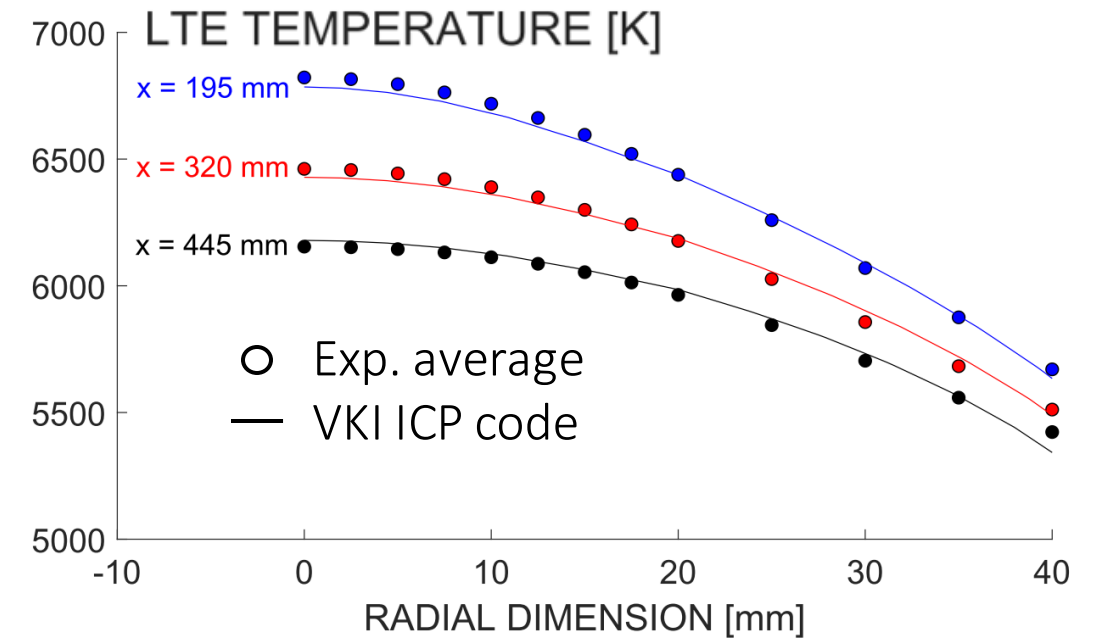
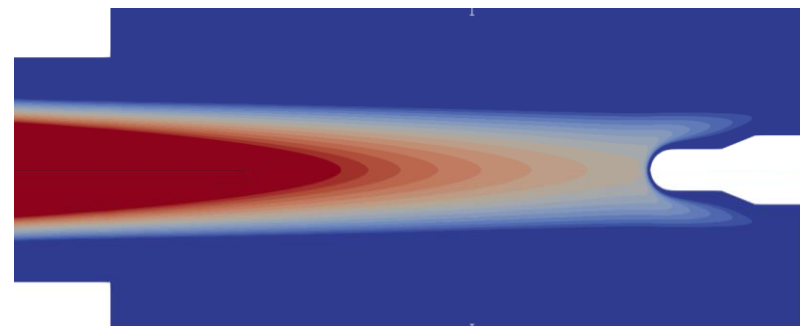


# 1.2 MW Inductively Coupled Plasmatron

MHD-CFD simulations: Serving as input to material simulations



Input ARGO



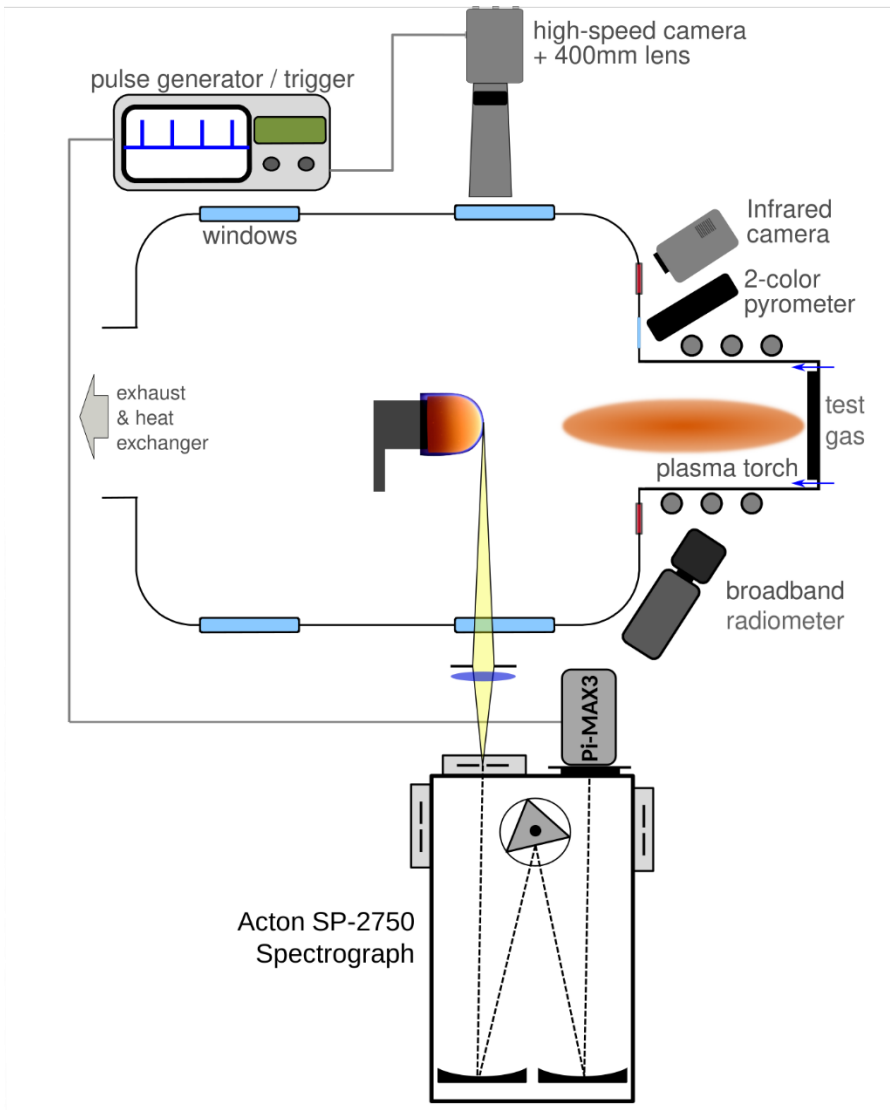
A. Fagnani et al., AIAA 2020-0382





# In-situ material response characterization

## Comprehensive high-temperature experimental setup



FLIR A6750sc MWIR (3-5 $\mu$ m)

450 - 3270 K calibrated (FLIR)

2-colour pyrometer (0.75-1.1 $\mu$ m)

1300 - 3270 K calibrated (NPL London)

Broadband radiometer (0.65-39 $\mu$ m)

RT - 3270 K calibrated (NPL London)

Optris 1C pyrometer (3-5 $\mu$ m)

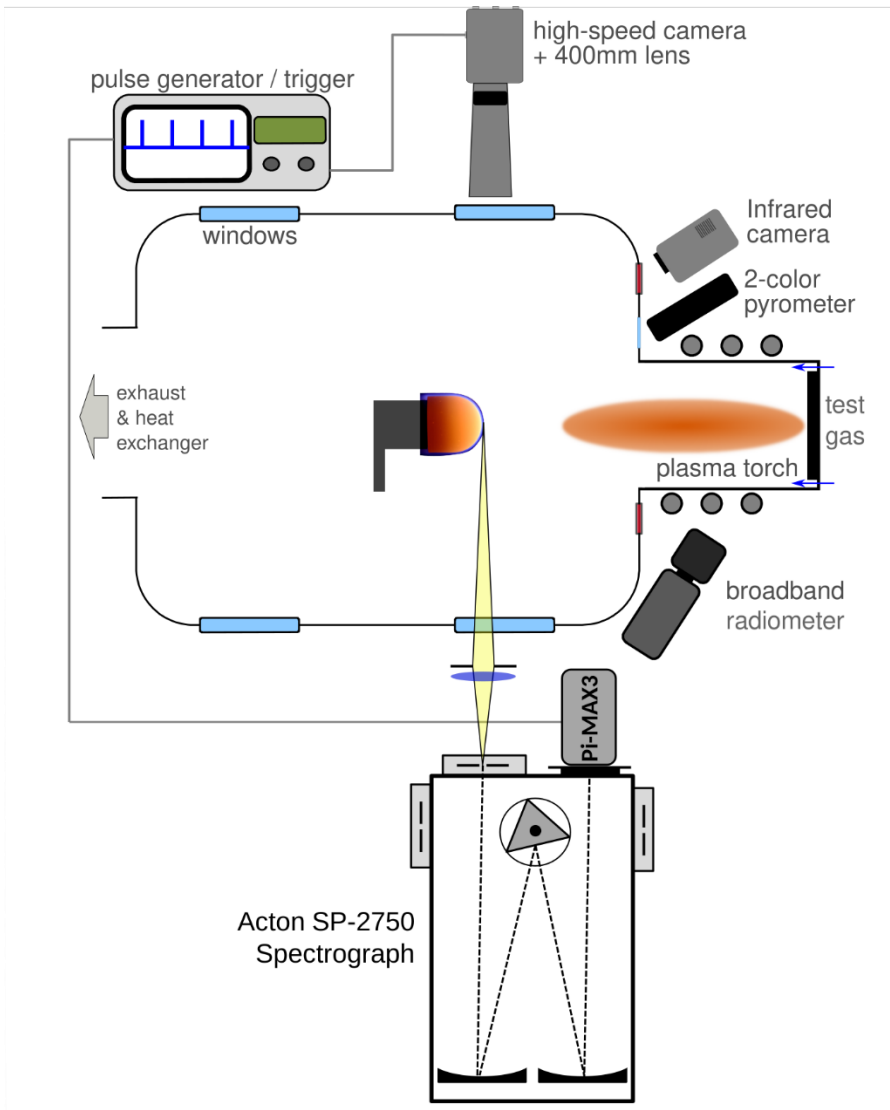
RT - 2000 K

Type-K thermocouples (Nickel-Chromium/Nickel-Alumel)

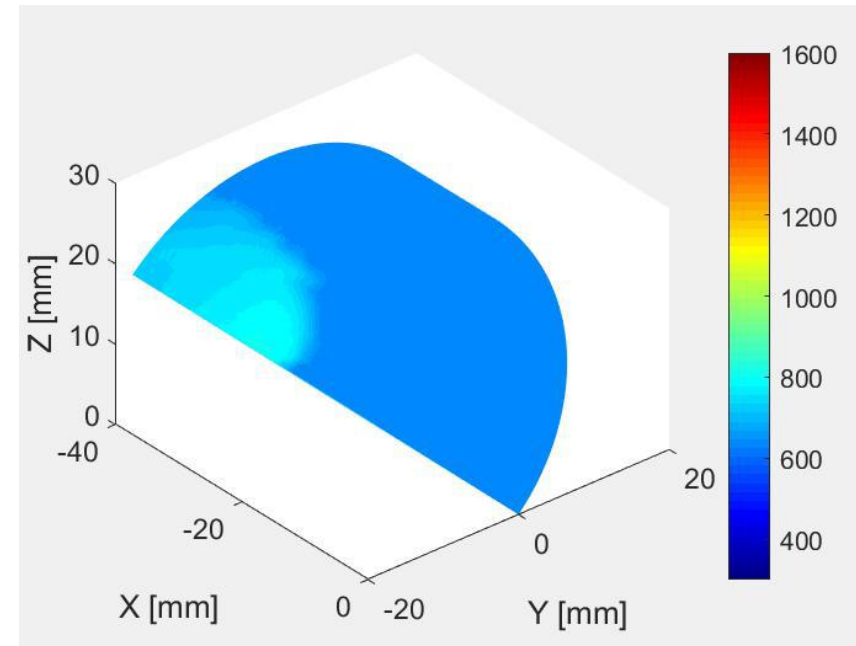
RT - 1500 K

# In-situ material response characterization

## Comprehensive high-temperature experimental setup



FLIR A6750sc MWIR (3-5 $\mu\text{m}$ )  
450 - 3270 K calibrated (FLIR)

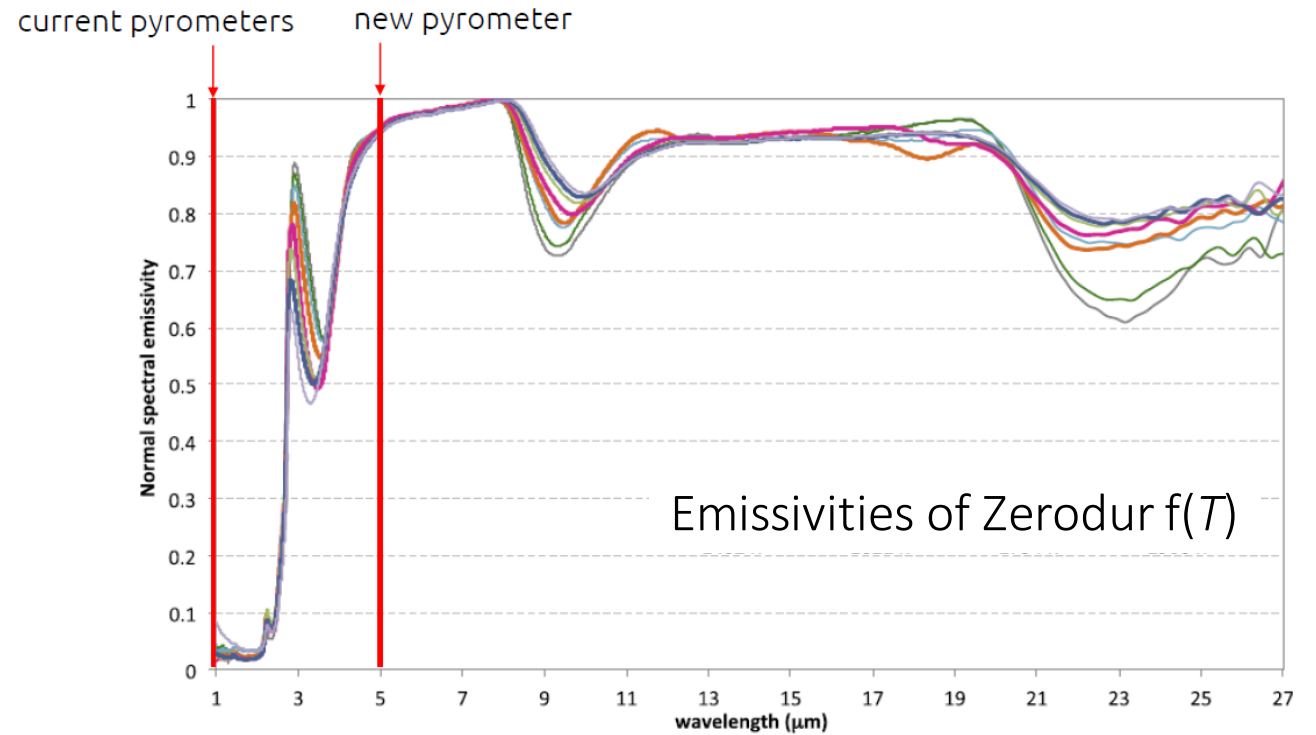


# In-situ material response characterization

Quartz surface pyrometry: Problems with transmissivity

New glass pyrometer:

- OPTRIS CTlaserG5
- spectral range  $5\mu\text{m}$
- to be calibrated at VKI
- emissivity required [Balat et al.]



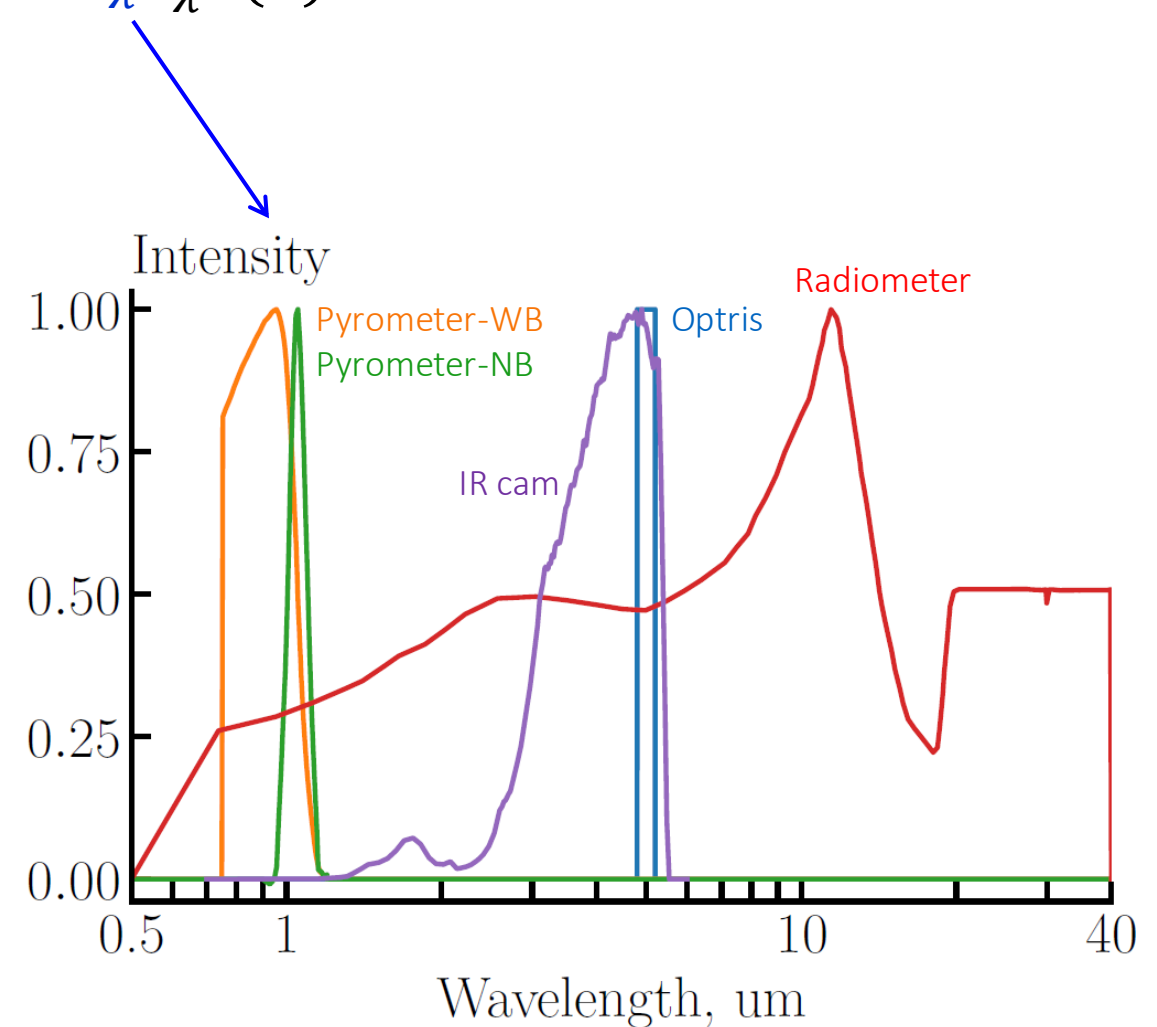
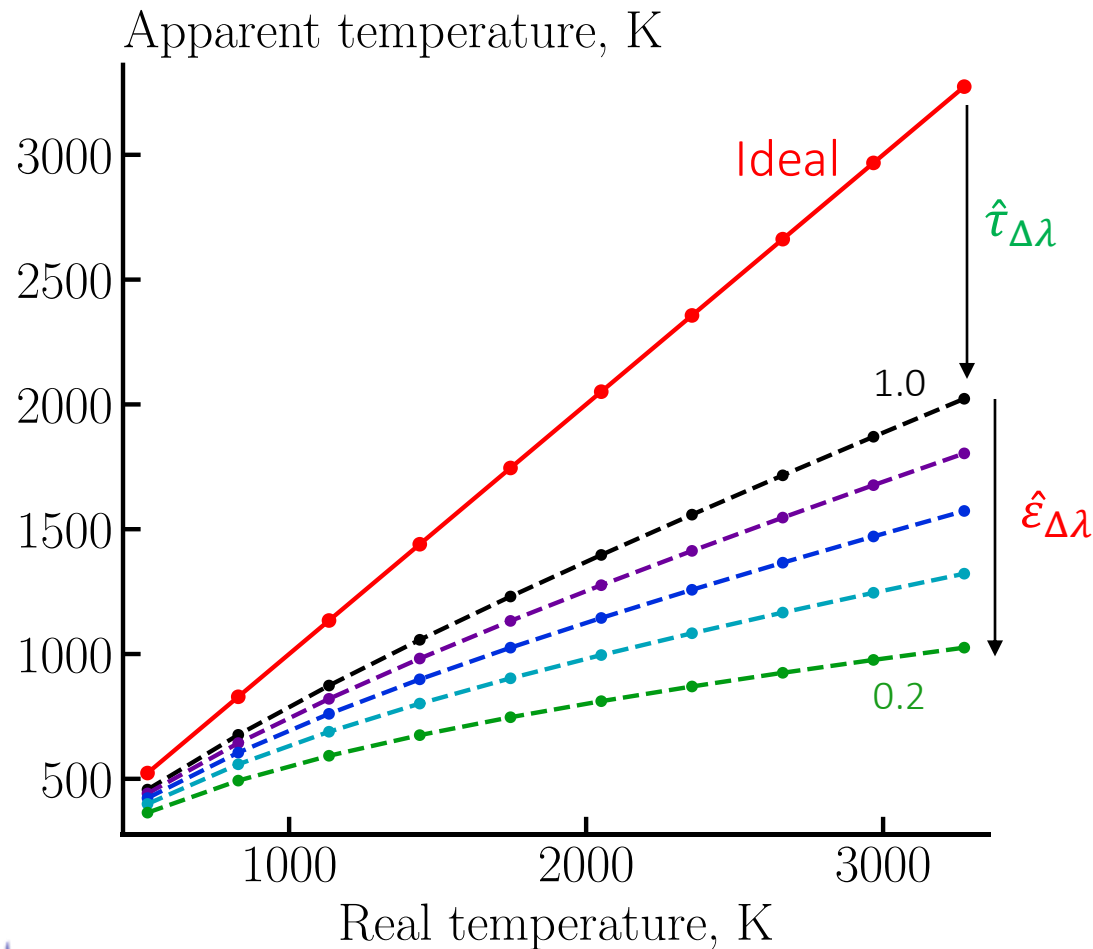
Balat-Pichelin, M., De Sousa Meneses, D., and Annaloro, J.  
*Infrared Phys. Technol.*, 101, 2019 (68–77)

# IR radiometry: calibration and emissivity measurements

1) The instrument response can be simulated for different grey-body emissivities

2) the grey-body emissivity can be measured once the real temperature is known

$$I_{\text{det}}^{\text{RB}} = \hat{\tau}_{\Delta\lambda} \hat{\epsilon}_{\Delta\lambda} \int_0^{\text{inf}} \tilde{R}_{\lambda} L_{\lambda}^{\text{BB}}(T)$$



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Mutation<sup>++</sup>

1D-stagnation line code with melting model

High-fidelity *ARGO* simulations



# Quartz-HS30-A: no recession

injection

crack appearing

surface steady state

test end

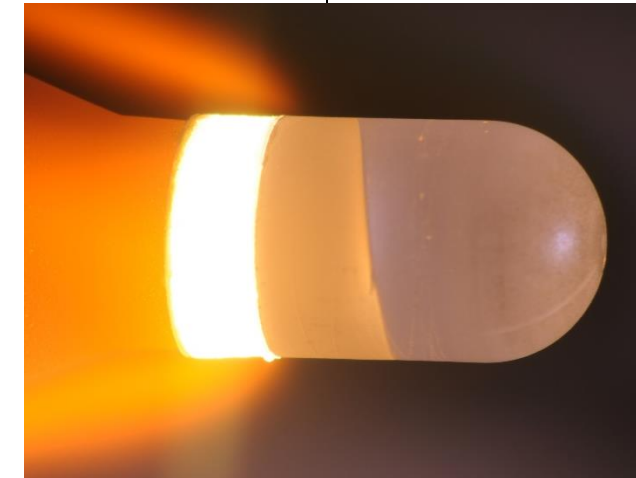
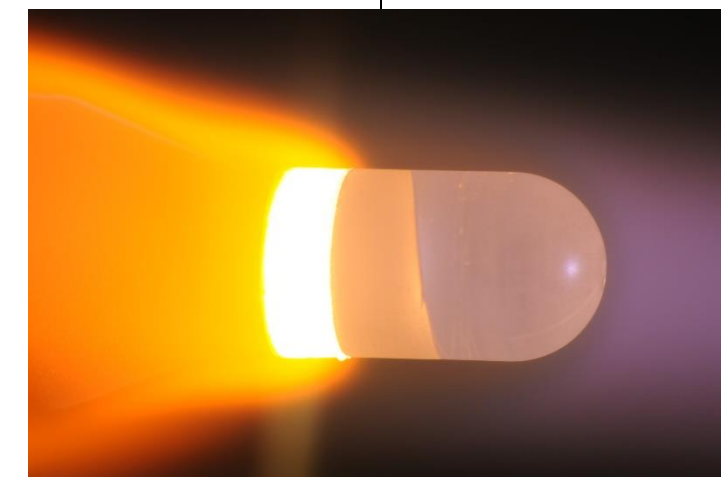
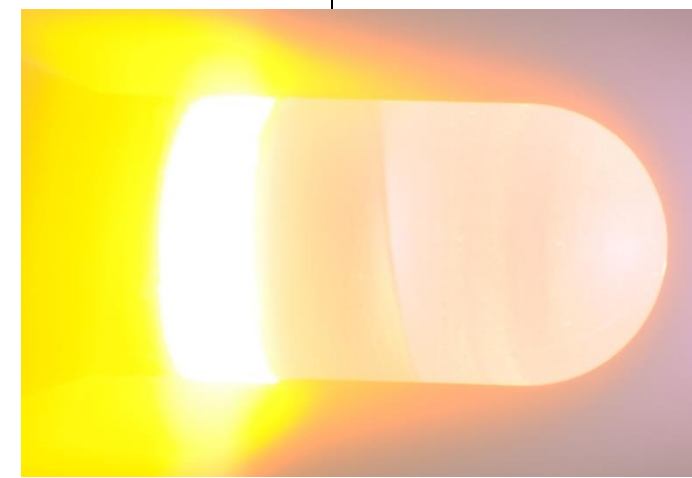
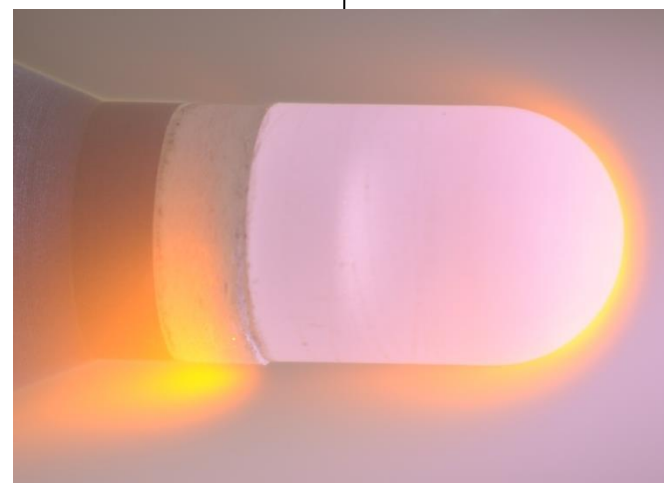
0s

17s

180s

385s

time, →



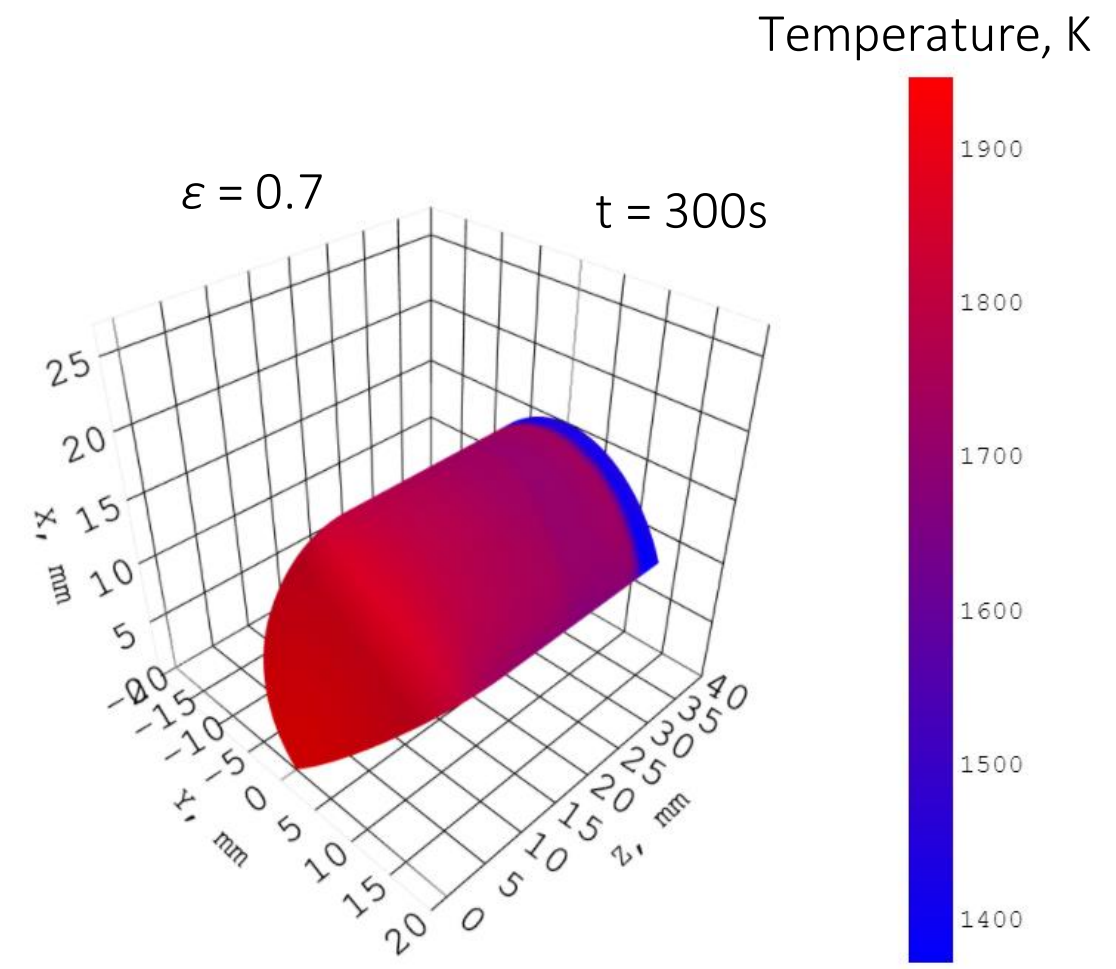
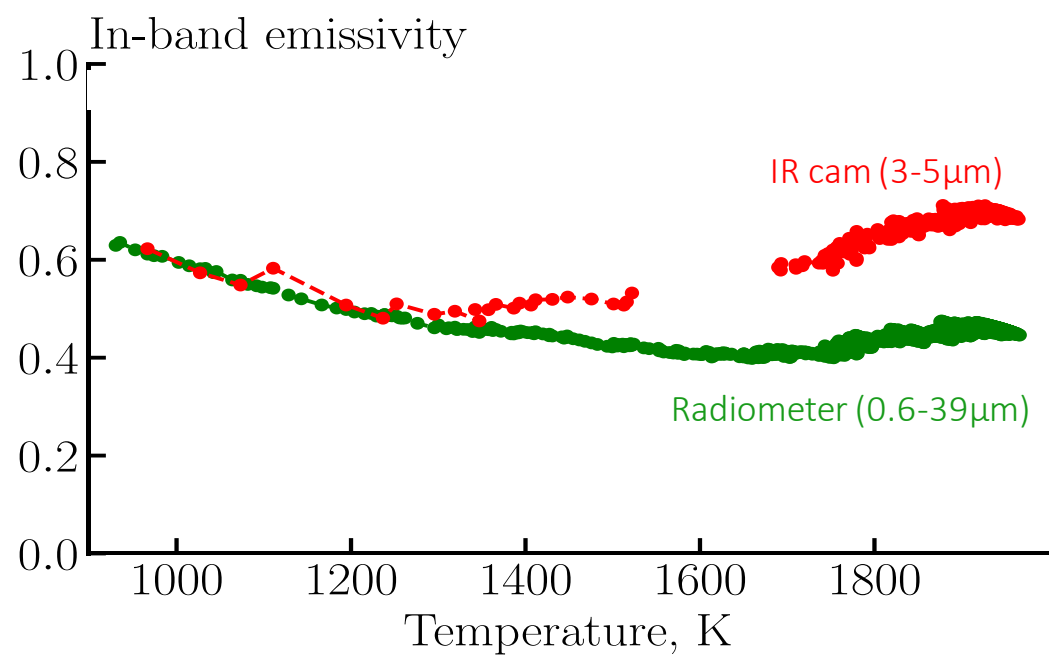
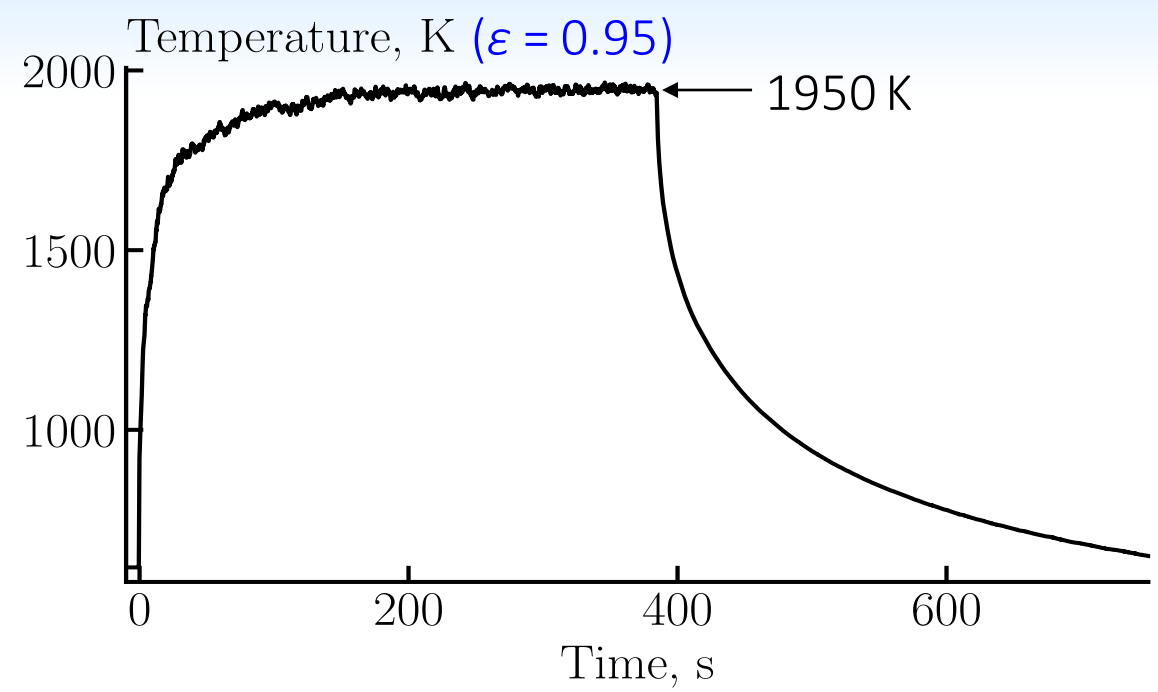
virgin



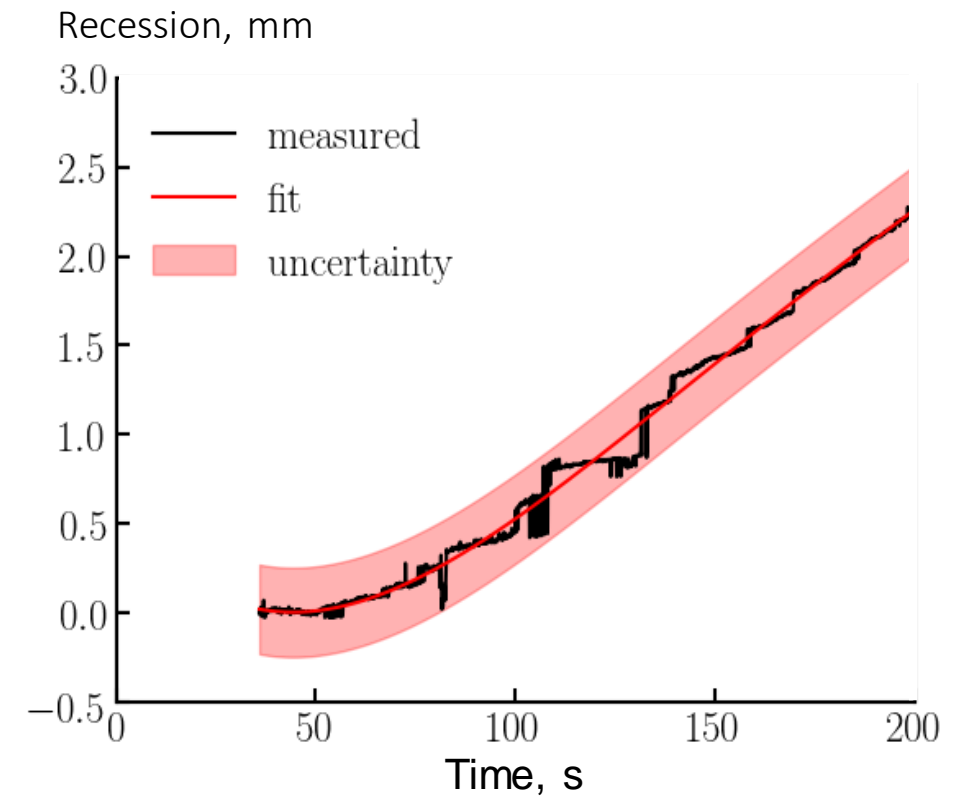
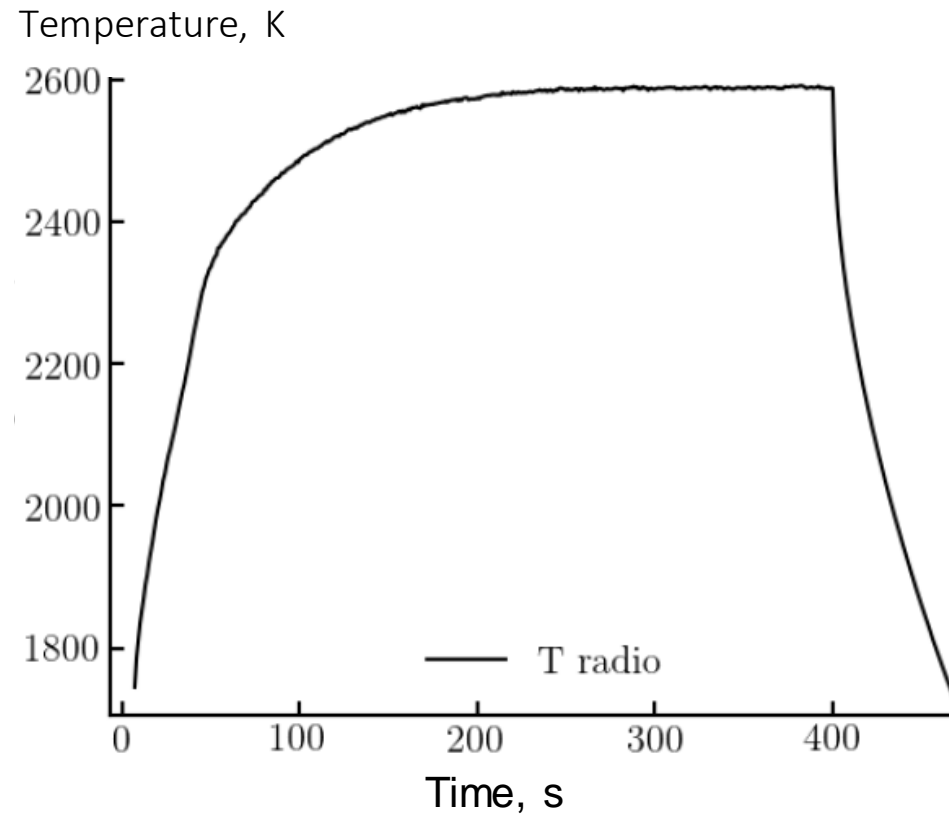
tested



# Quartz-HS30-A: Surface radiometry



# Quartz-HS50-A: High recession





# ZERODUR demise testing

air 16 g/s, 50 mbar, 150 kW

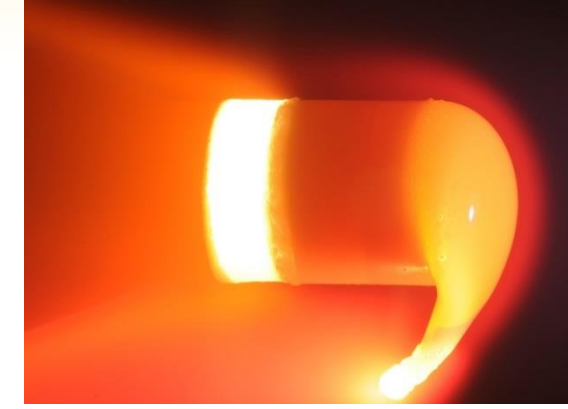
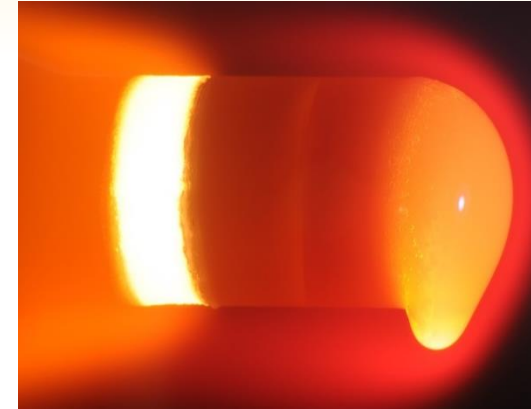
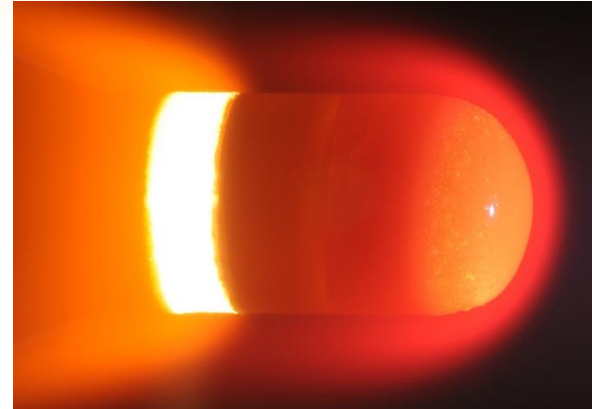
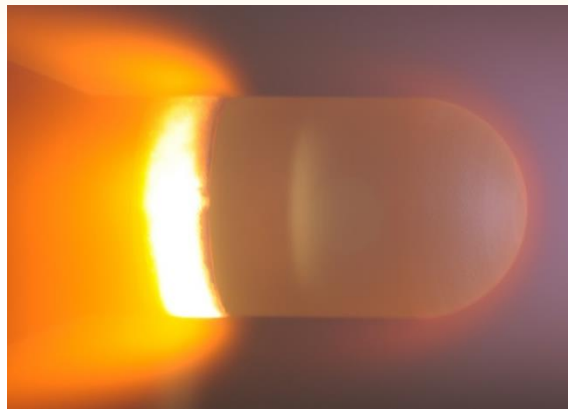
injection

boiling starts

formation of droplet

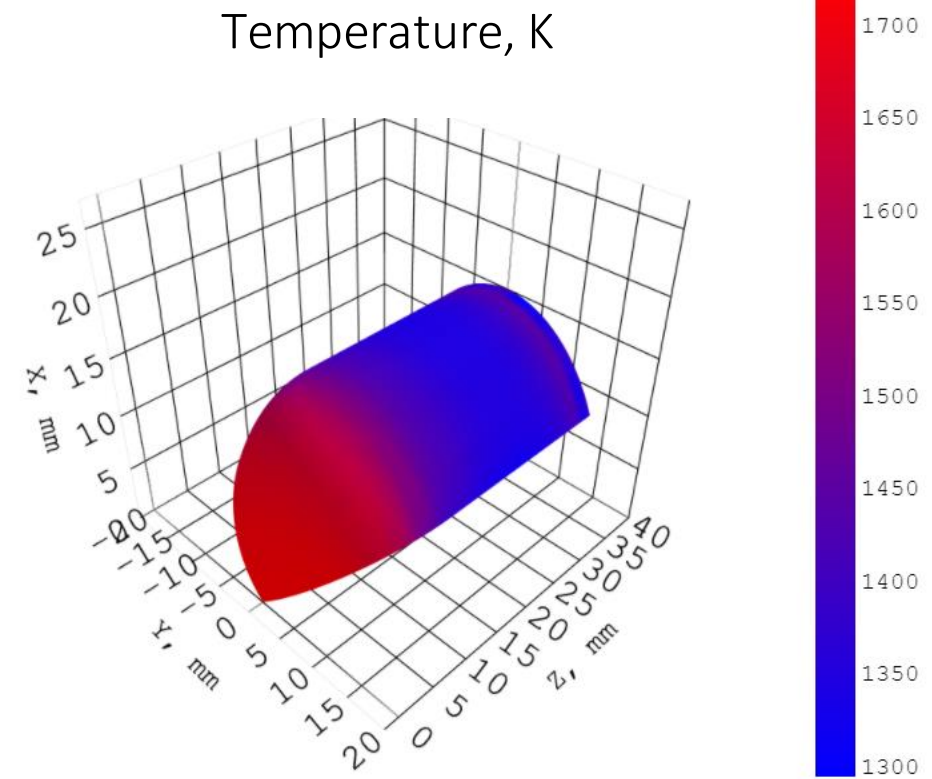
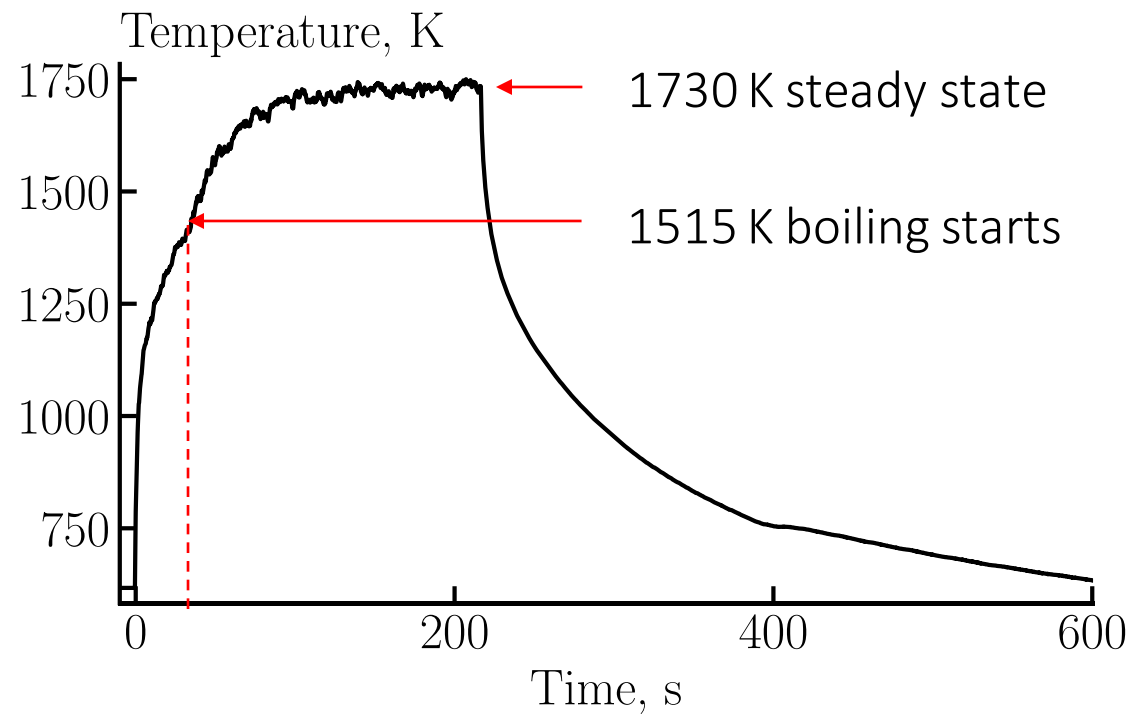
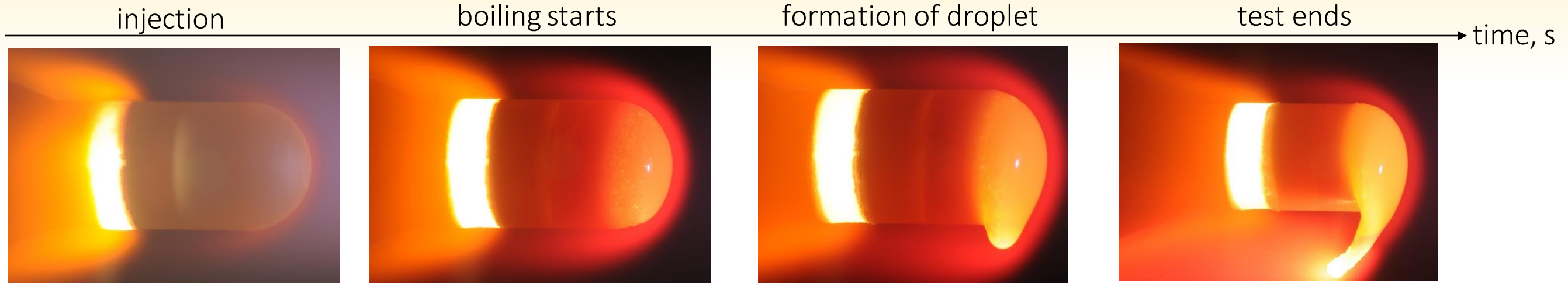
test ends

time, s

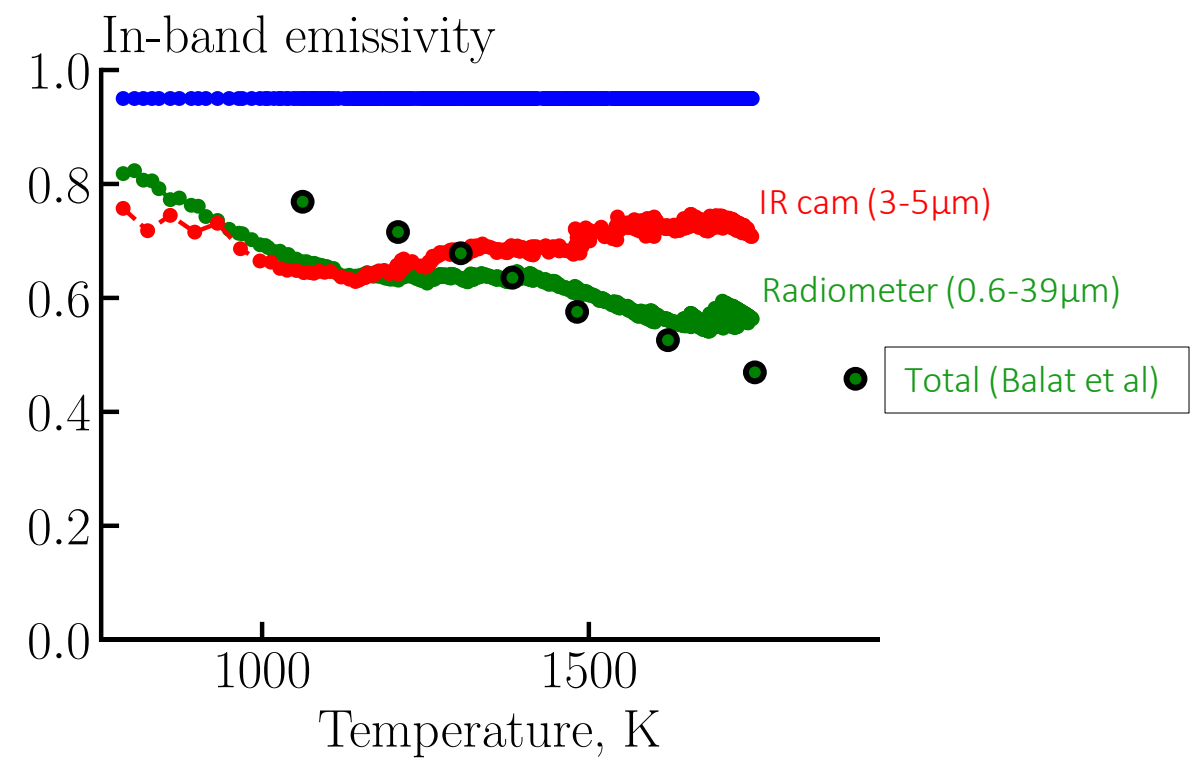
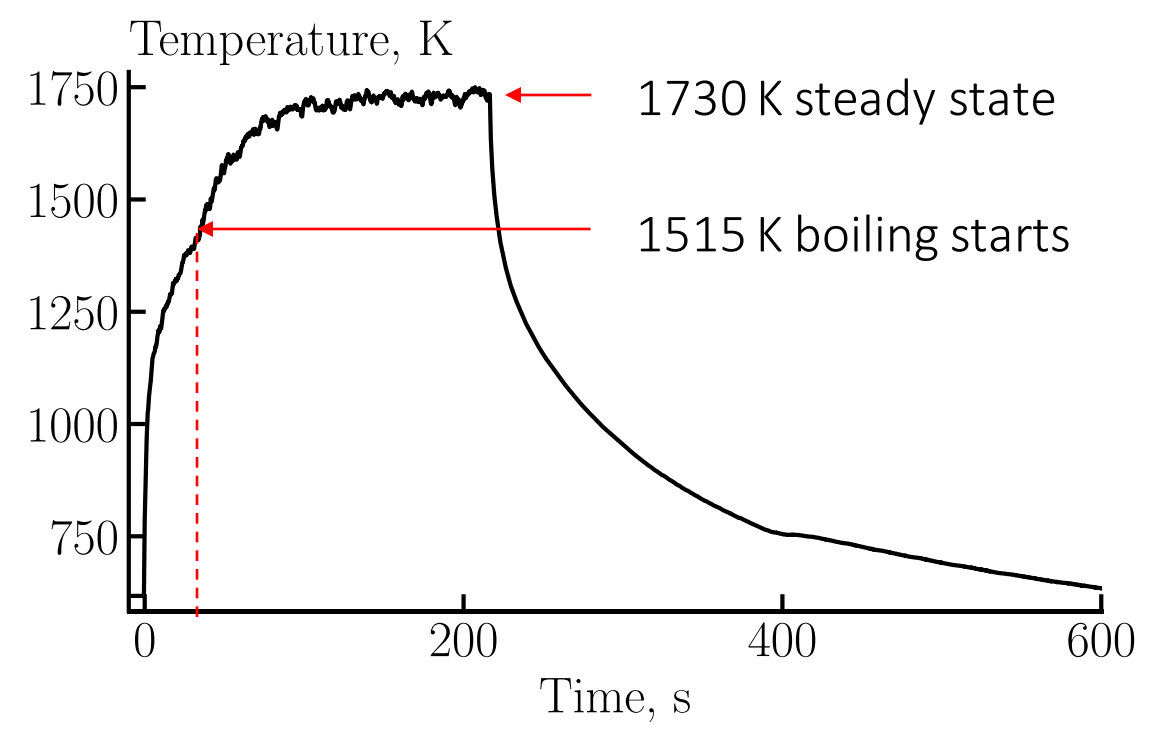
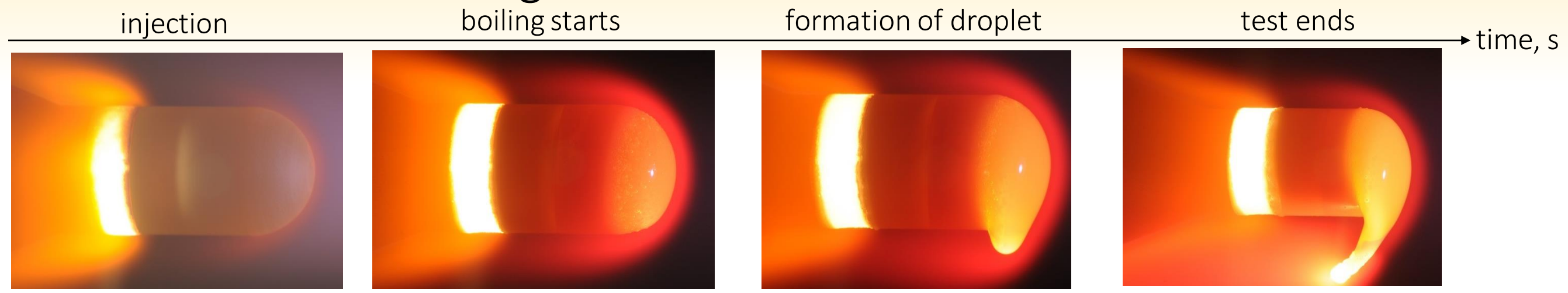


# ZERODUR demise testing

air 16 g/s, 50 mbar, 150 kW

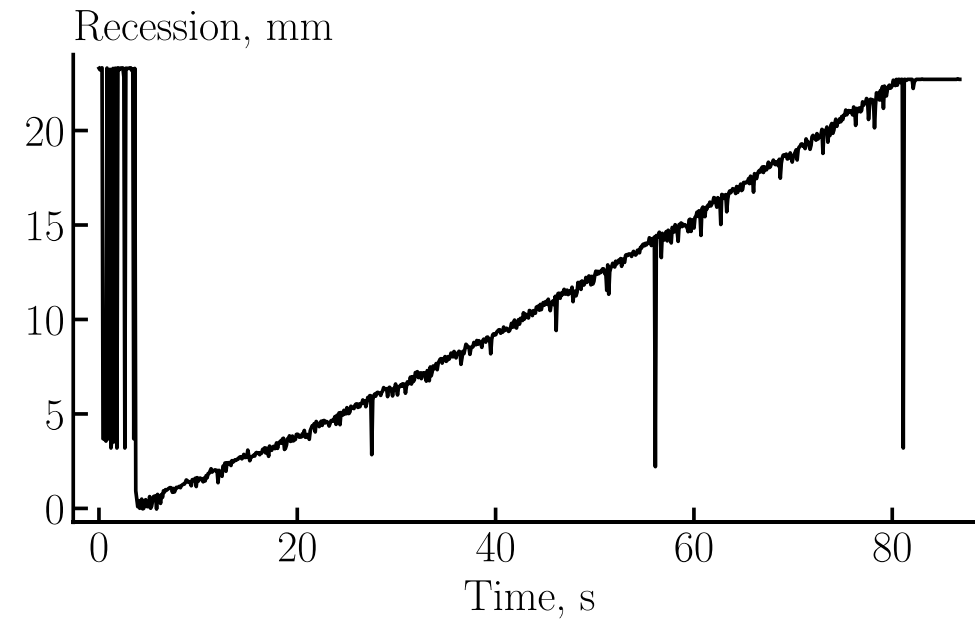
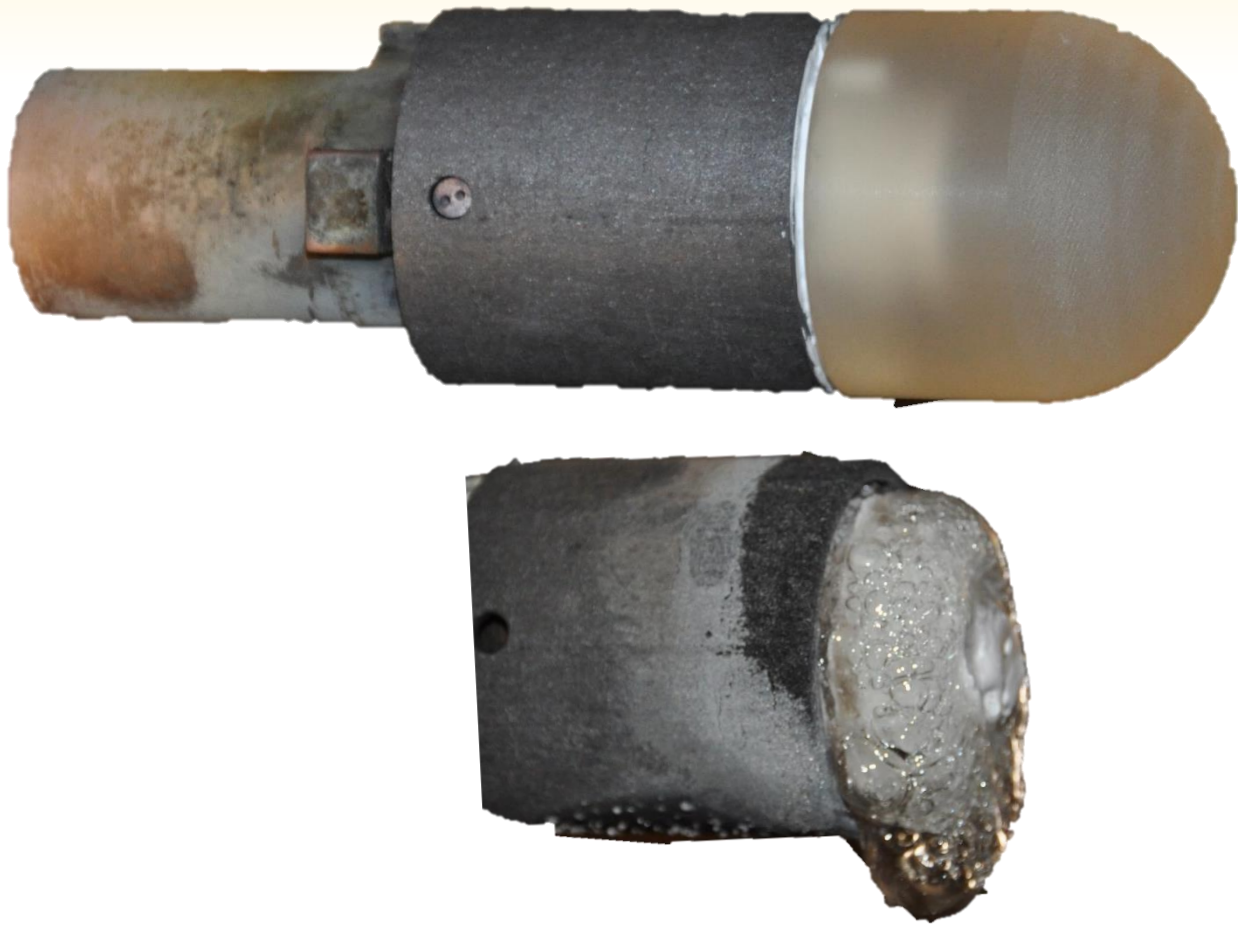


# ZERODUR demise testing

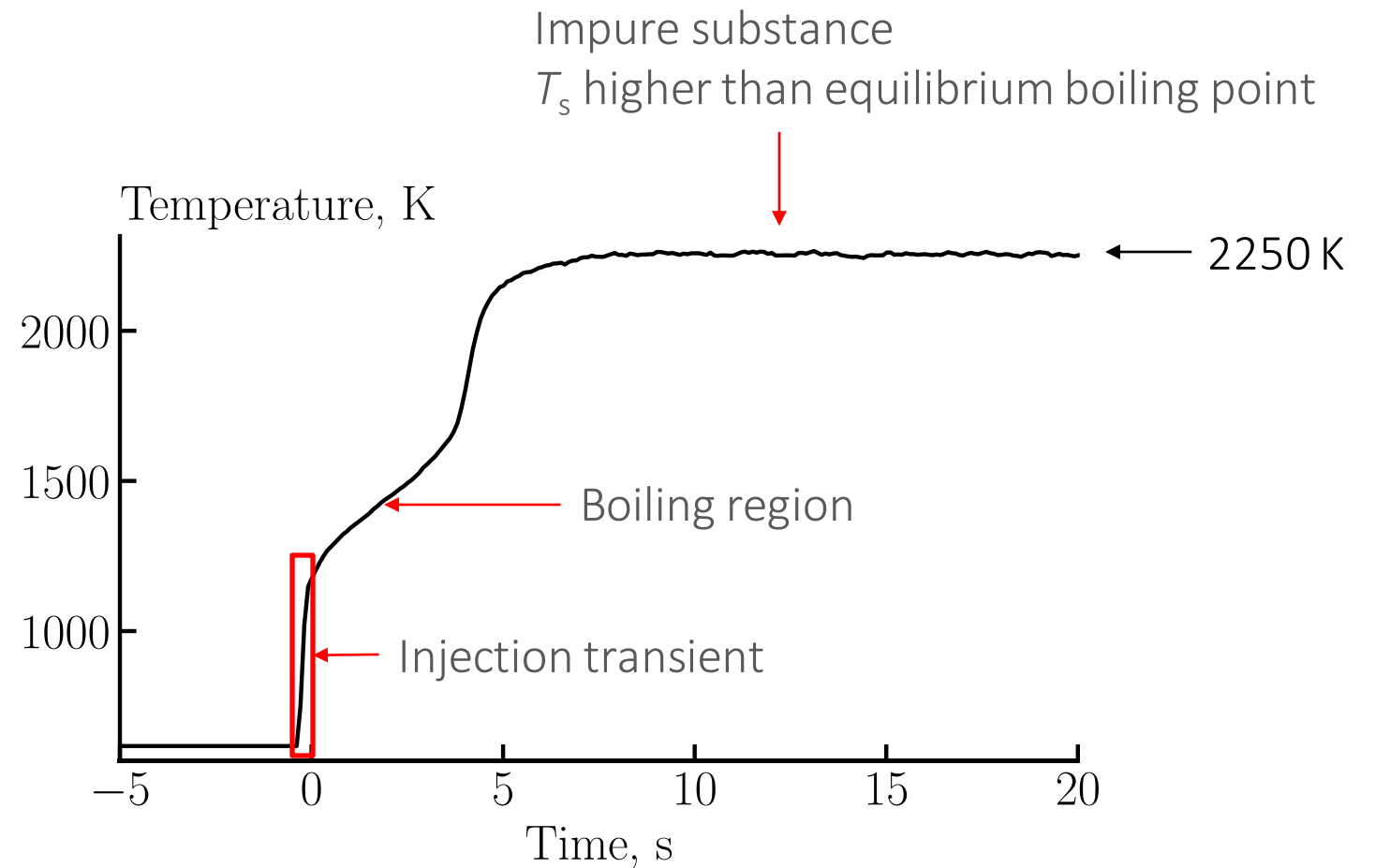
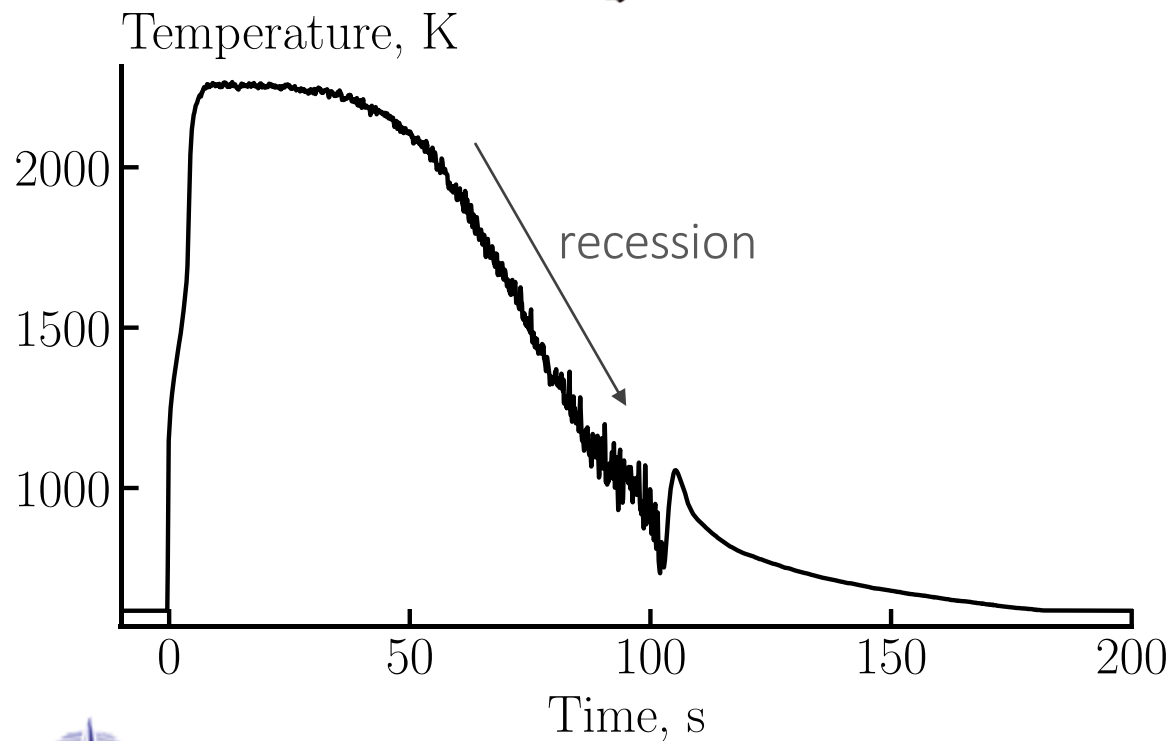


# ZERODUR demise testing

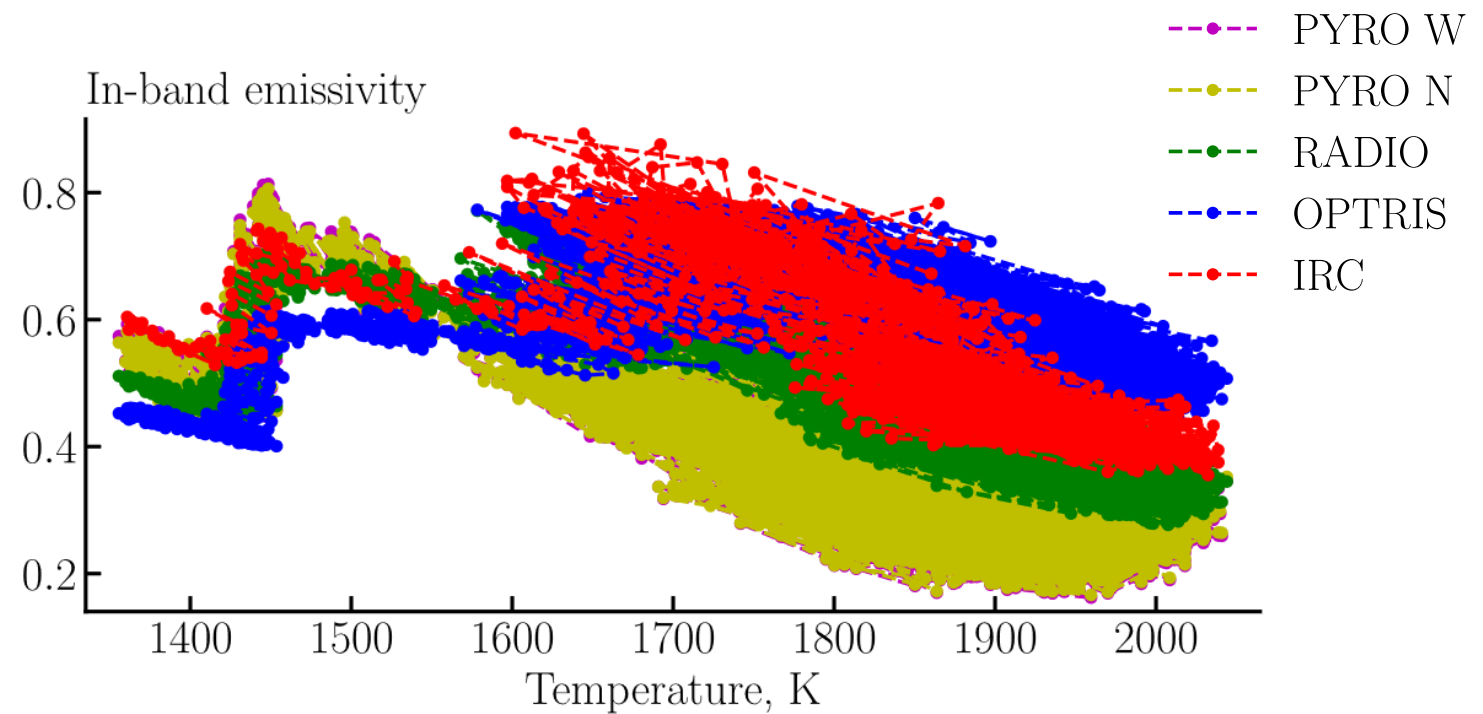
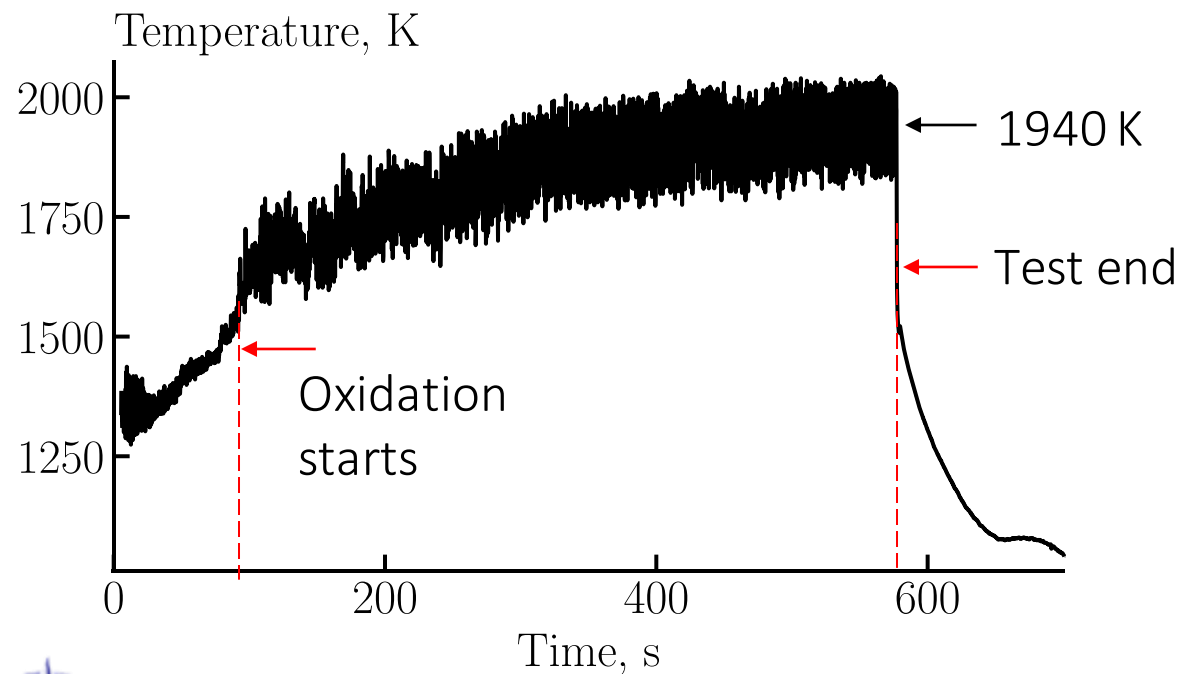
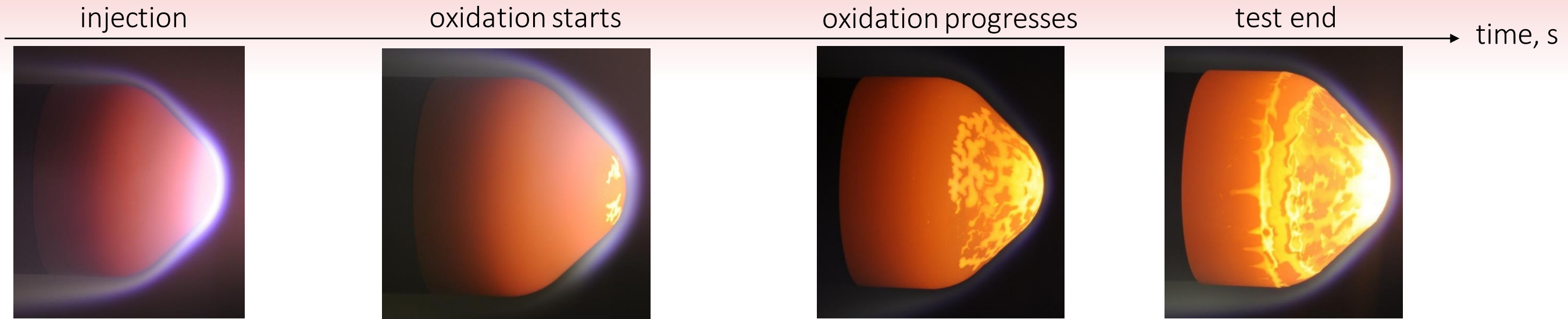
air 16 g/s, 100 mbar, 390 kW



# ZERODUR demise testing

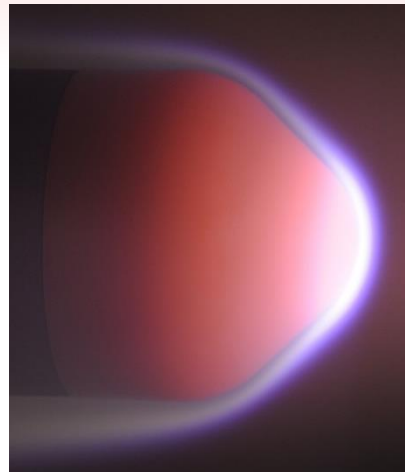


# Titanium oxidation: difficult to demise and difficult to simulate



# Titanium oxidation: difficult to demise and difficult to simulate

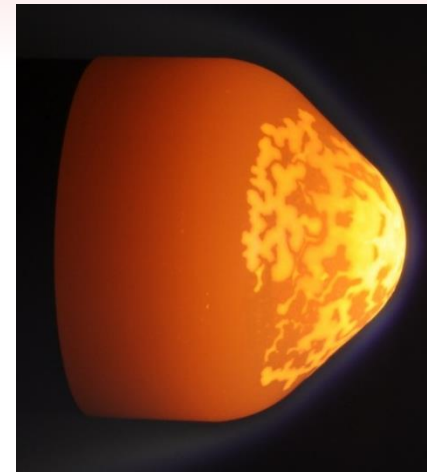
injection



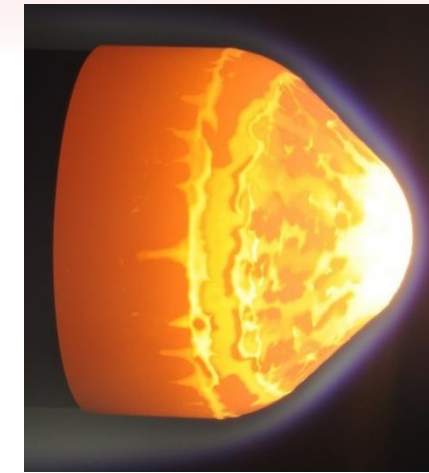
oxidation starts



oxidation progresses



test end

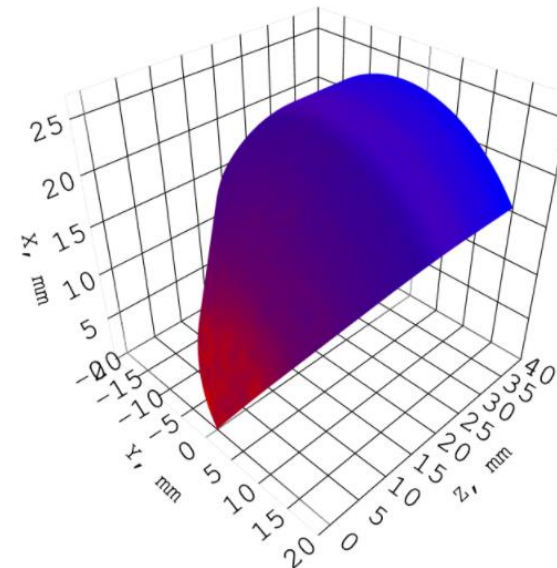


time, s →

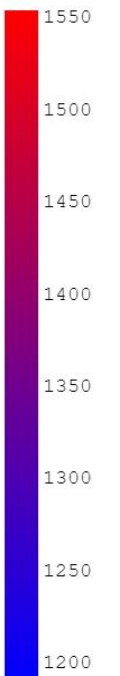
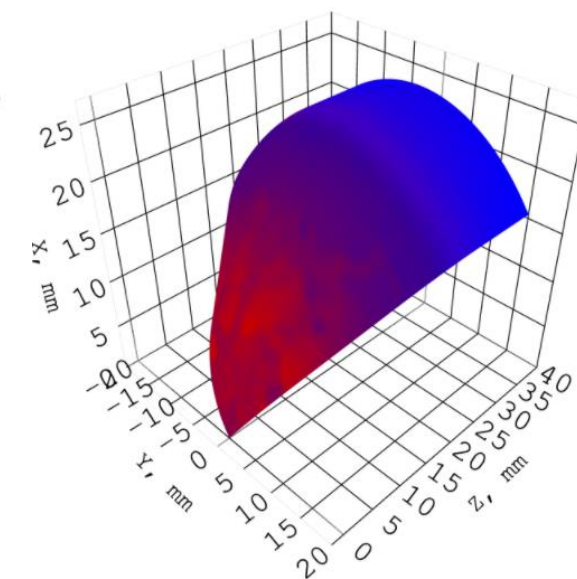


mass gain 0.36 g  
No oxide peel-off during test  
oxide layer looks brittle

200s



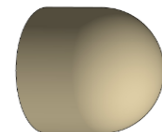
550s



# Demise material testing overview

	Run	Gas	$p_{\text{static}}$ [hPa]	$P_{\text{el}}$ [kW]
Quartz	Qz-HS50-A	Air	100	290
	Qz-SC50-A	Air	50	290
	QZ-HS30-A	Air	50	150
	QZ-SC40-A-SS	Air	5	500
Zerodur	Ze-HS30-A	air	50	150
	Ze-HS50-A	air	100	392
Titanium	TiG2-HS30-A	Air	100	160
	TiG2-HS50-N	N <sub>2</sub>	50	?
	TiG5-HS30-A	Air	50	125
	TiG5-Sc50-A	Air	50	125

HS50: 50 mm hemisphere-cylinder



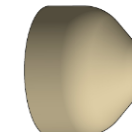
Non-equilibrium gas chemistry  
Low shear

HS30: 30 mm hemisphere-cylinder



Frozen gas chemistry  
High shear

SC50: 50 mm sphere-cone



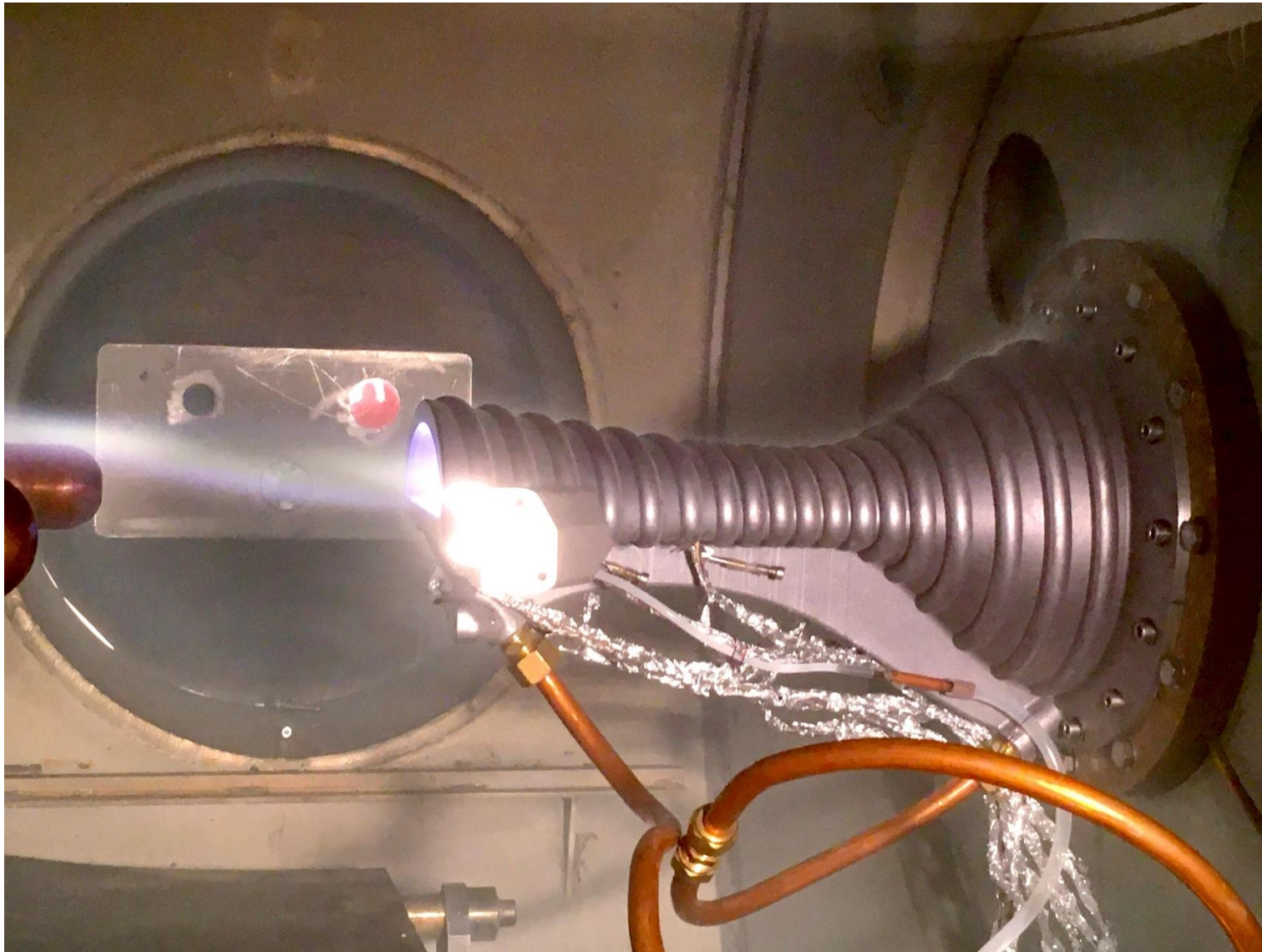
Non-equilibrium gas chemistry  
Uniform melt thickness



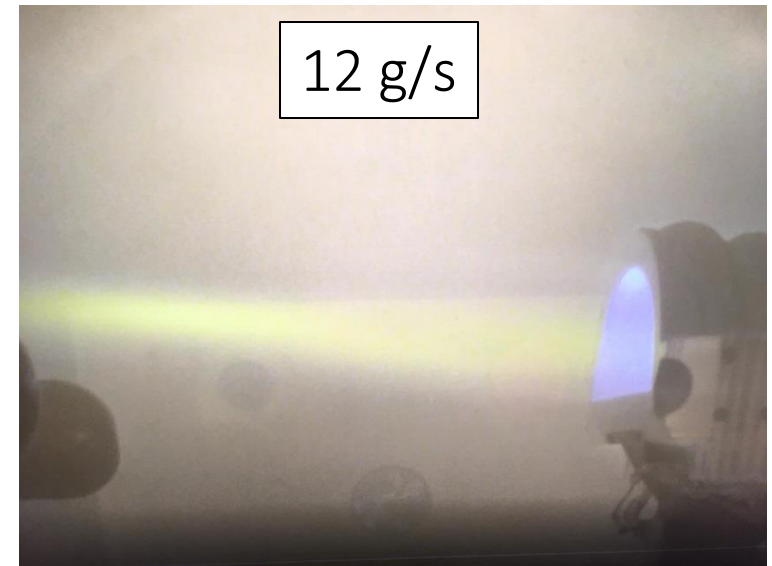


# Supersonic nozzle commissioning and characterization

Semi-elliptical nozzle for flat plate testing



5 g/s

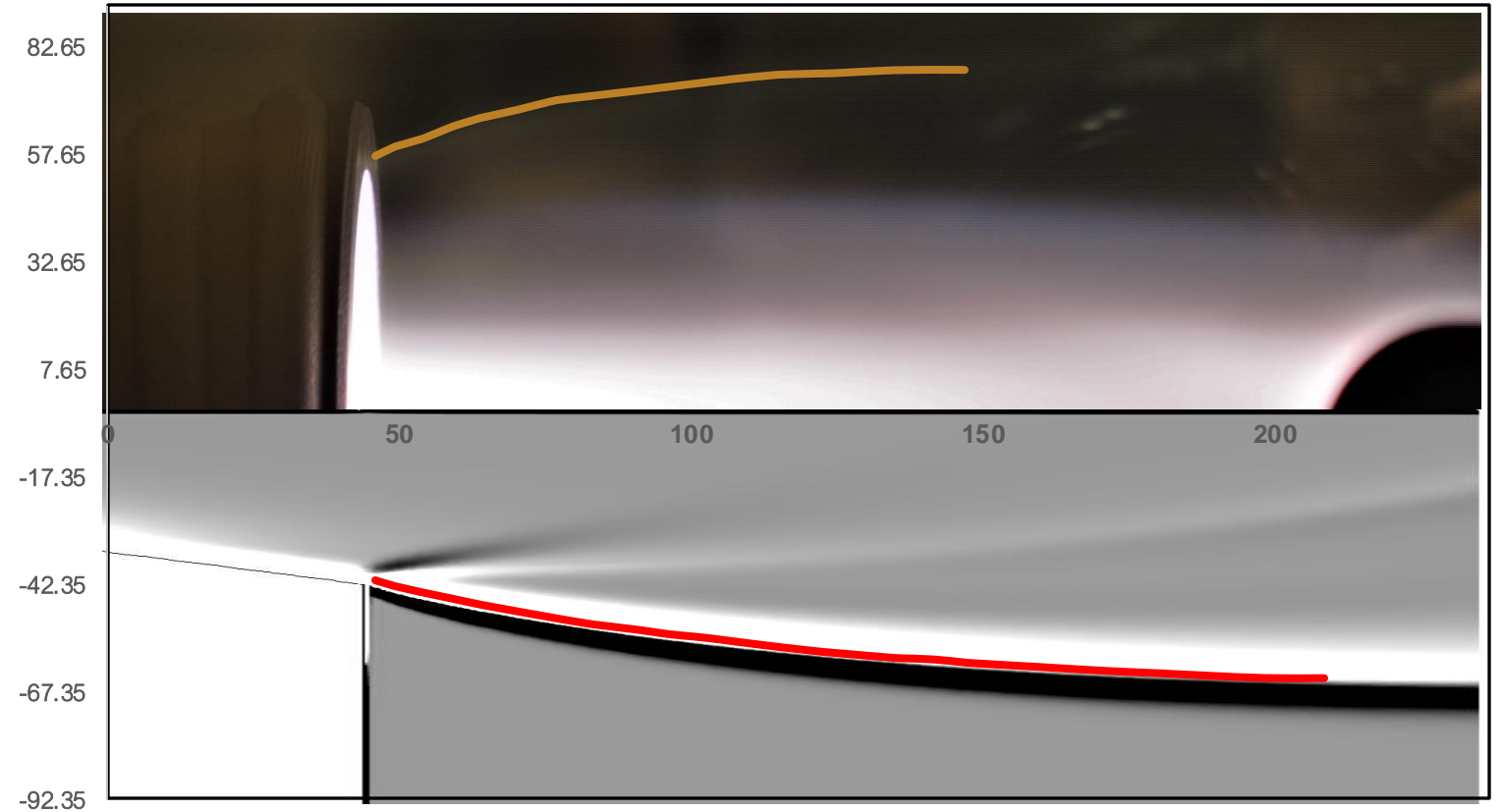
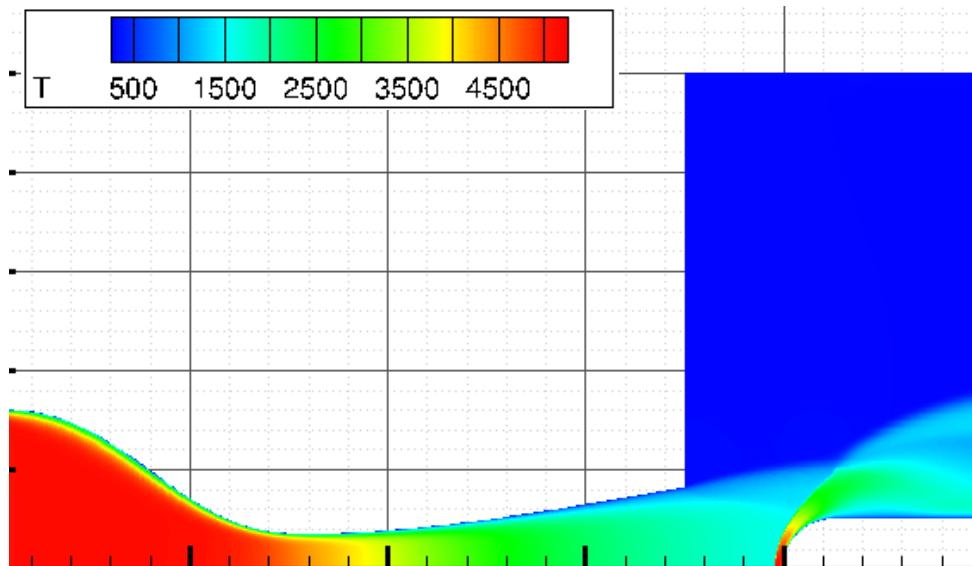
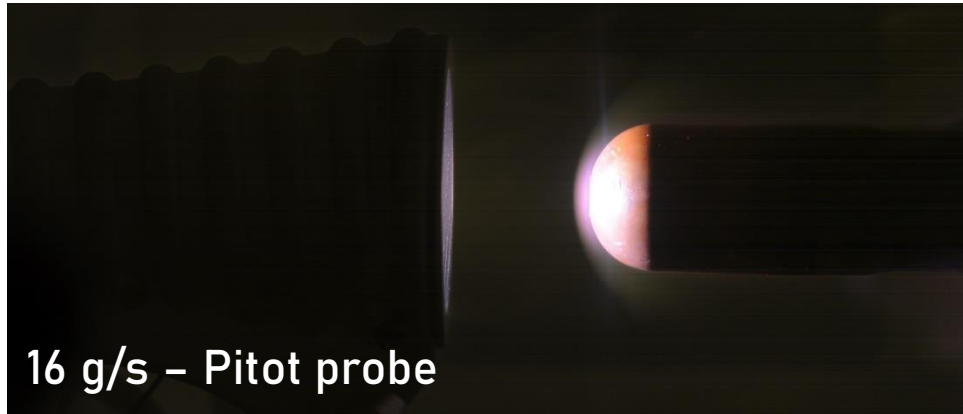


12 g/s



# Supersonic nozzle commissioning and characterization

Conical nozzles for stagnation point testing



# Overview

## Experimental methods

Plasmatron facility

Instrumentation setup and new hardware

## Experiments

Quartz

Zerodur

Titanium

Supersonic

## Numerical simulations outlook

Mutation<sup>++</sup>

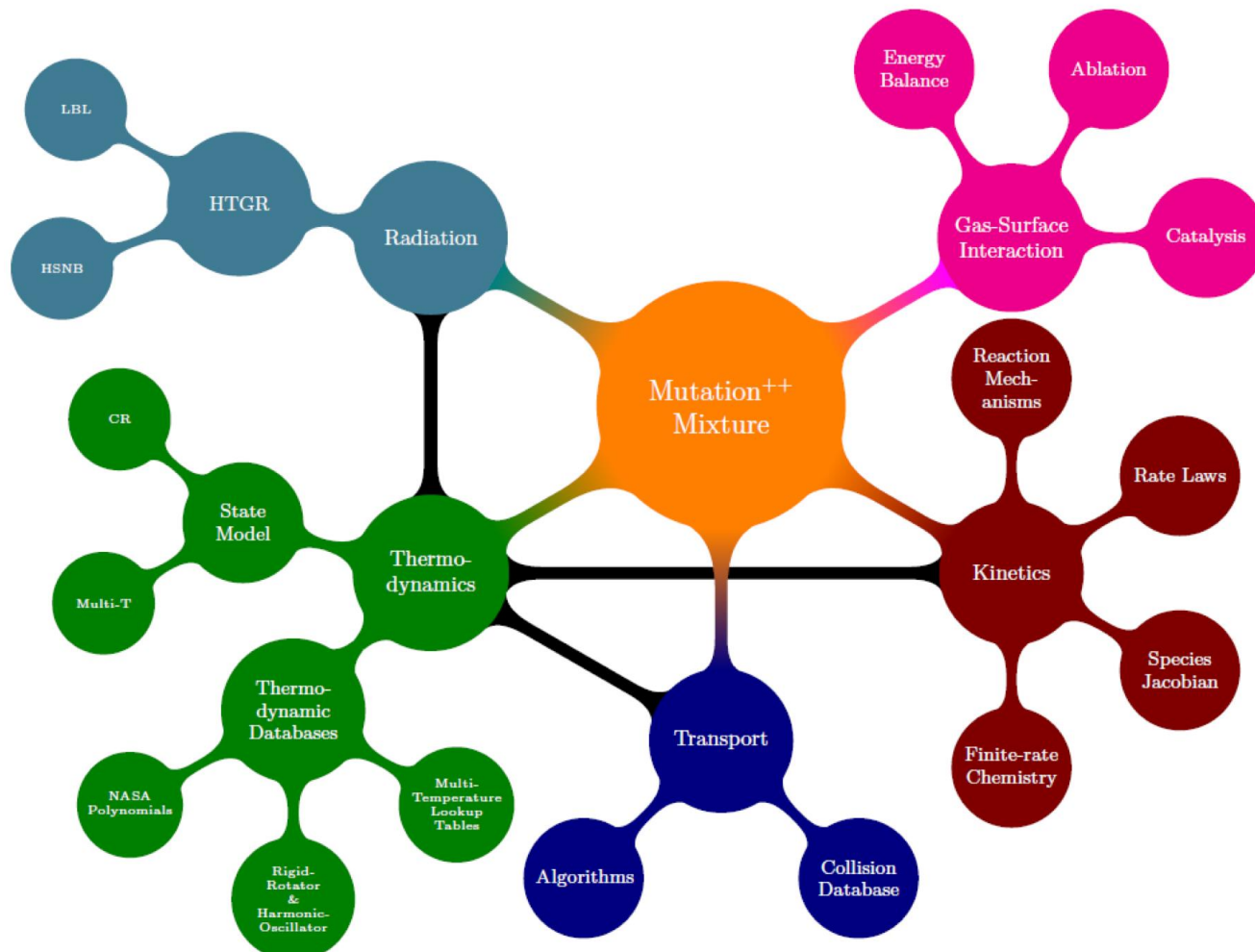
1D-stagnation line code with melting model

High-fidelity *ARGO* simulations



# Mutation<sup>++</sup>

MULTicomponent Thermodynamic And Transport properties/chemistry for IONized gases



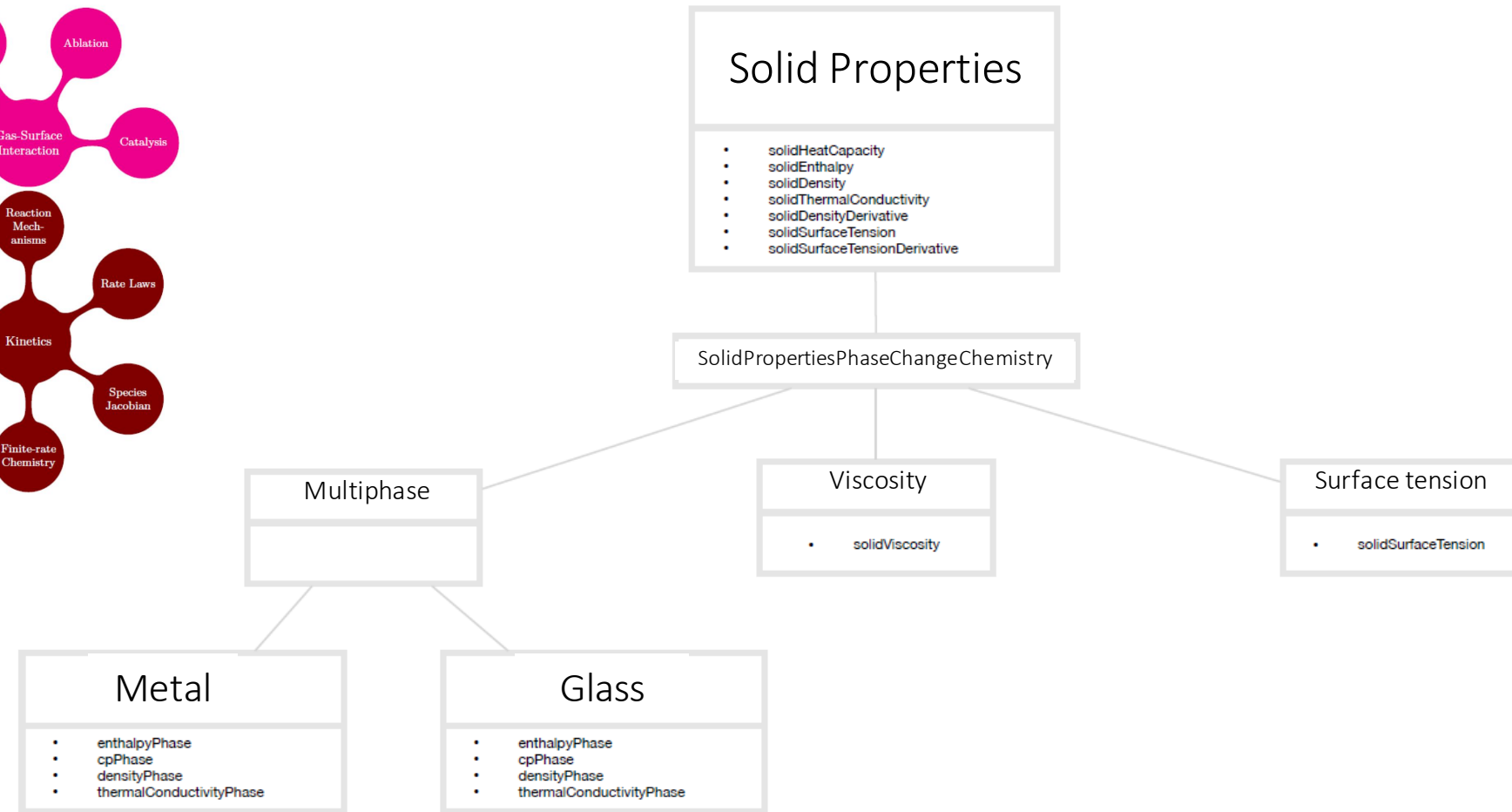
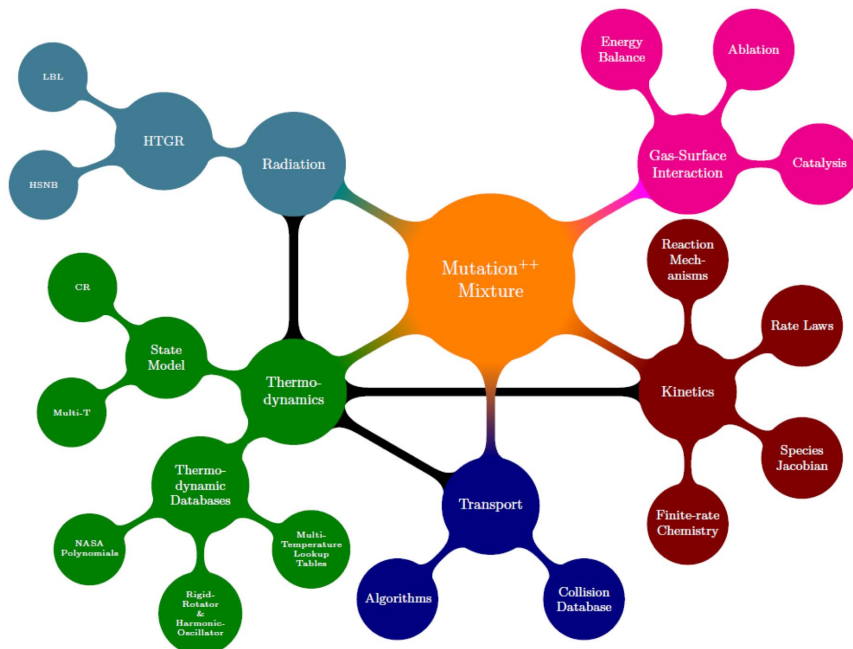
Include Phase-change material properties  
- Zinc (test case)  
- silica

Coupling with any material solver (*ARGO*)



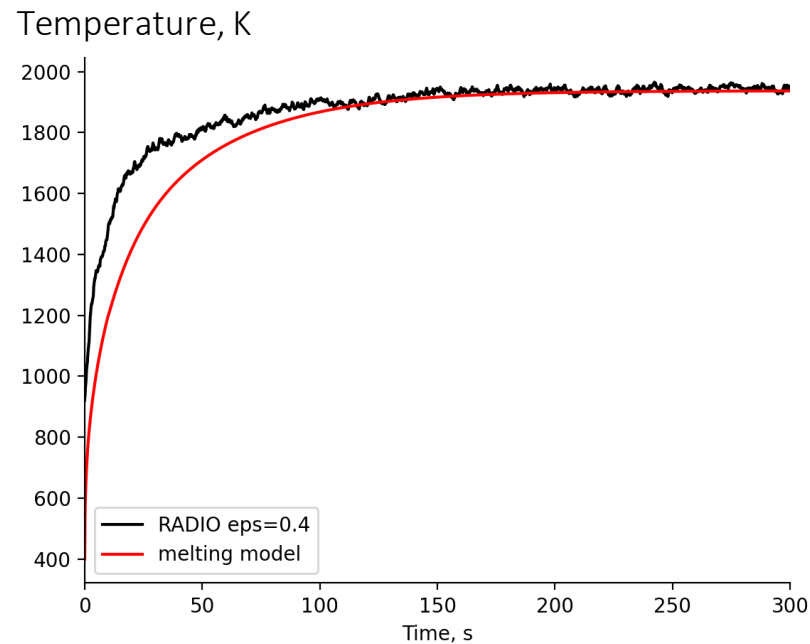
# Mutation<sup>++</sup>

MULTicomponent Thermodynamic And Transport properties/chemistry for IONized gases



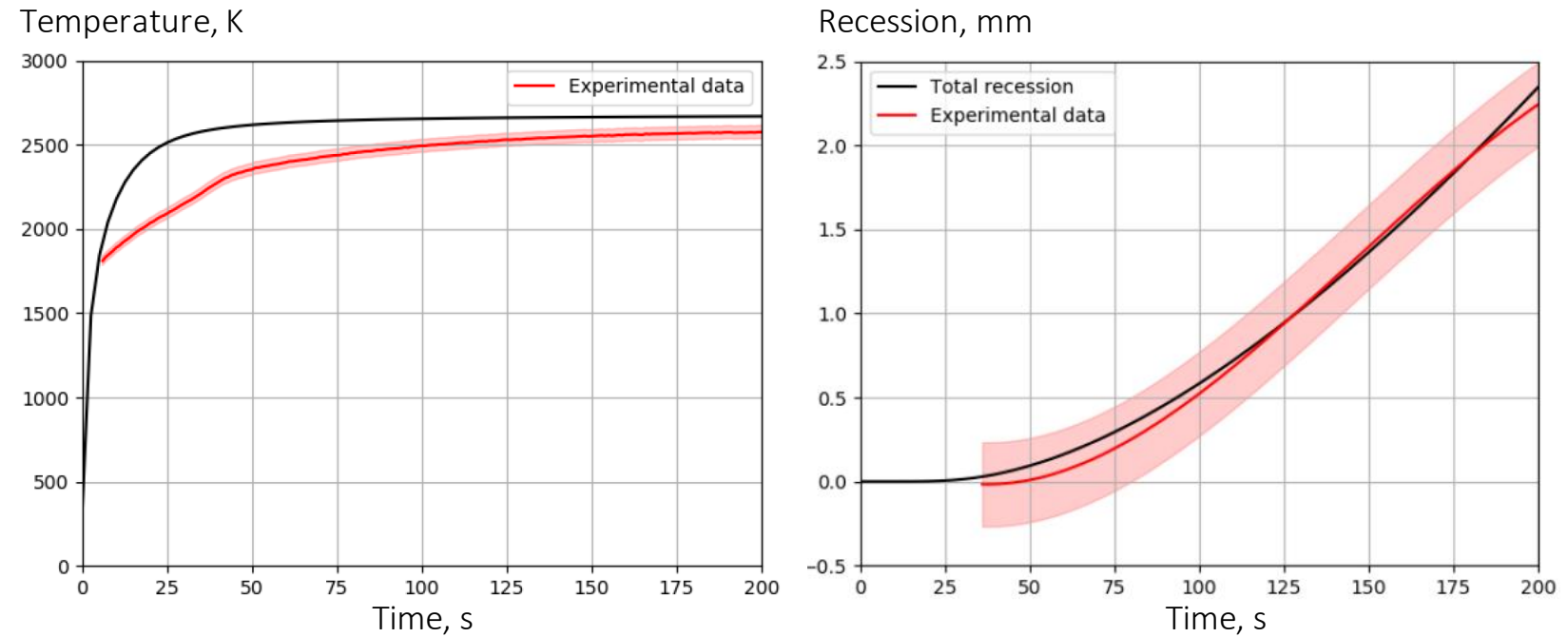
# Numerical 1D approach: Design of experiments and post-test comparison

Quartz, 50 hPa, 150 kW



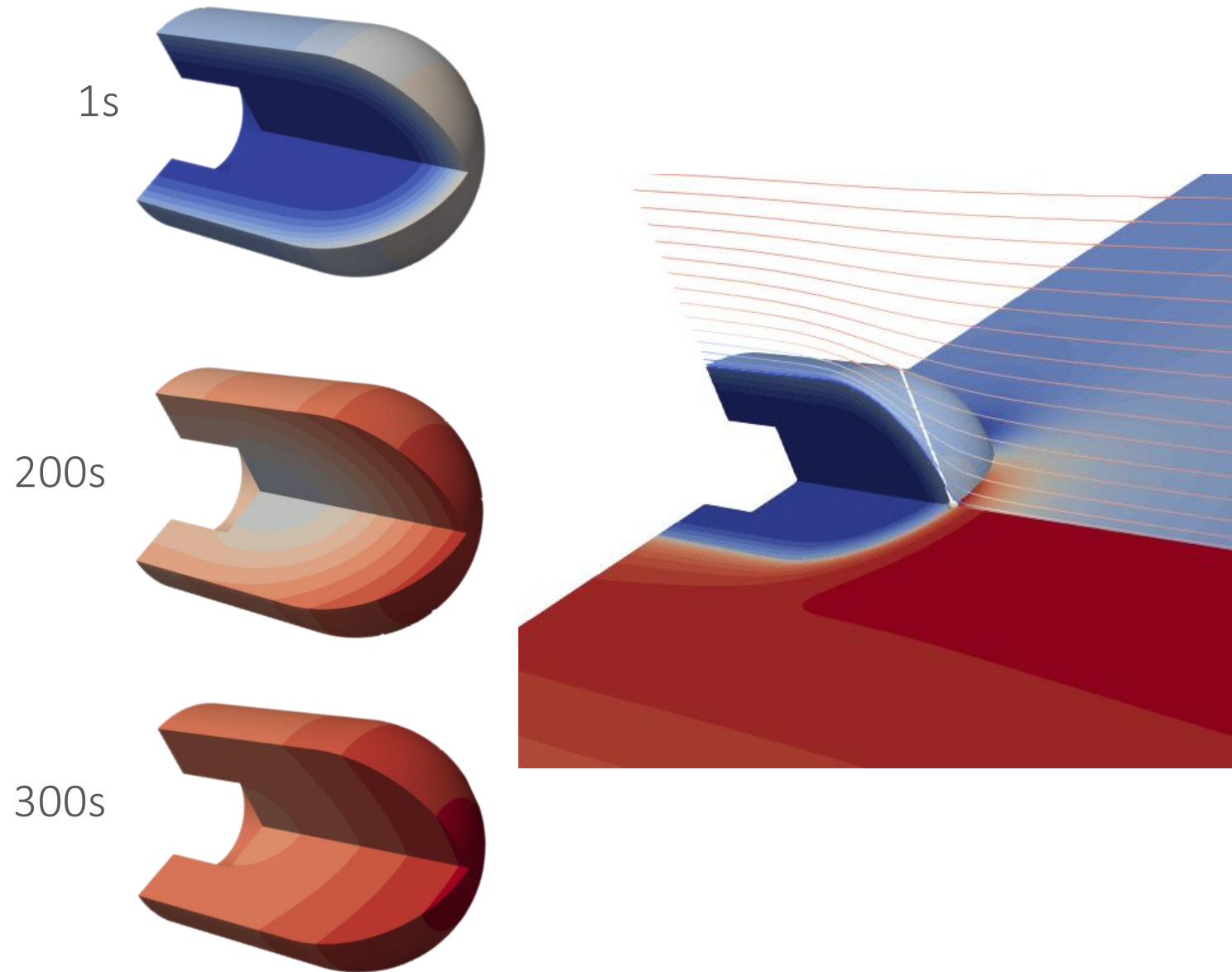
Focus on surface energy balance

Quartz, 100 hPa, 290 kW

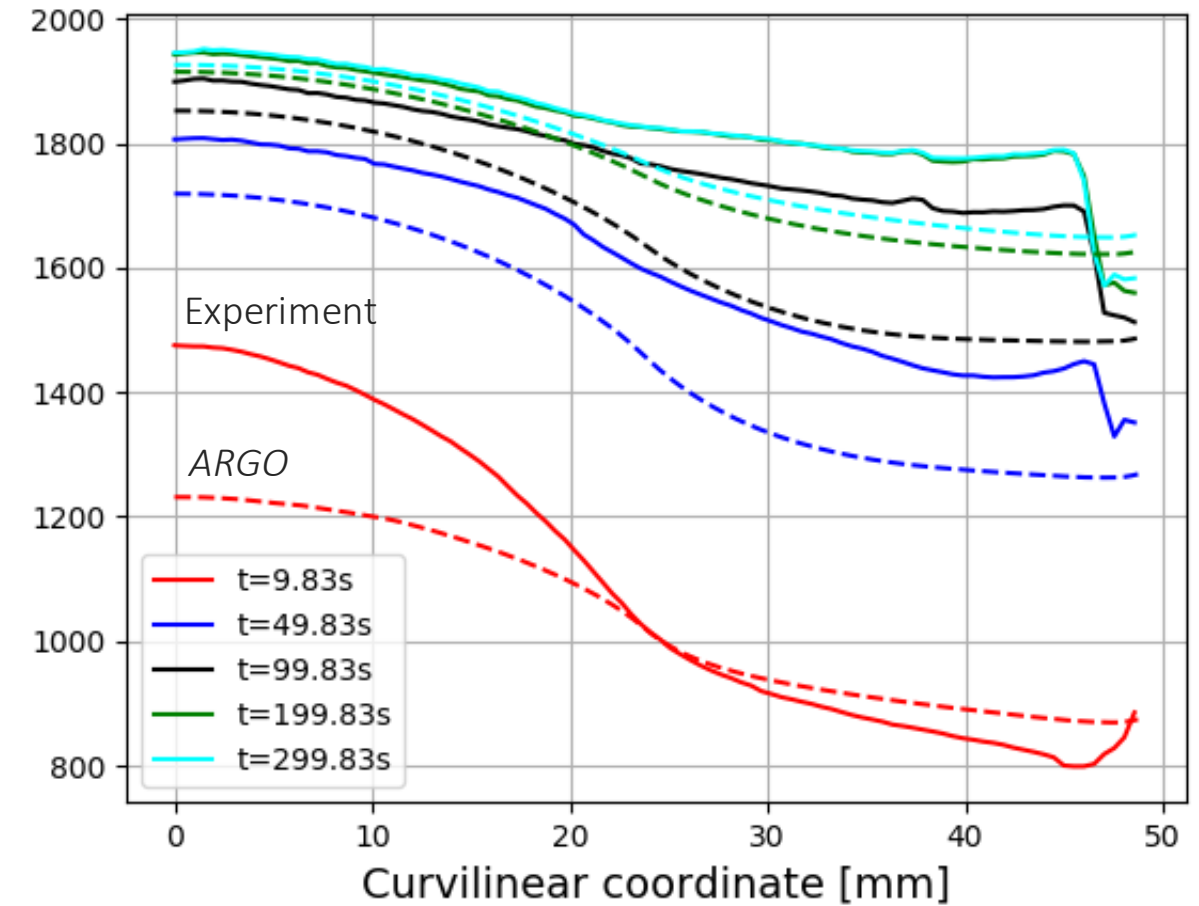


Adding evaporation and shear ablation

# High-fidelity simulations with *ARGO* (coupled material-flow solver)



Surface temperature, K



# Summary and Outlook

Subsonic experiments on quartz, ZERODUR<sup>®</sup>, Titanium finalized

- from basic to more complicated test cases, high-quality data for model validation
- in-band emissivities determined with detailed instrument error analysis
- ongoing 1D-modelling by VKI
- ongoing high-fidelity modelling with *ARGO* (extended to melting materials)
- ongoing surface analysis for oxidation (varying with test condition)
- future detailed oxidation study (?)

Semi-elliptical and conical nozzles commissioned

- characterization for conical nozzles completed
- first stagnation point experiment finalized (quartz)
- ongoing SE-nozzle flat plate characterization early 2022 (dummy sample + calorimeter)
- ongoing simulation with *ARGO* (extended to treat supersonic flow)
- future SE-nozzle flat plate experiments, including GSTP R.TECH

