

Challenges in Modeling Hollow Objects in the Transition Flow Regime

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(1) HX5 – Jacobs JETS Contract

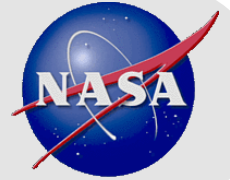
(2) GeoControl Systems – Jacobs JETS Contract

(3) Jacobs JETS Contract

NASA Orbital Debris Program Office

ATD³

2 December 2021

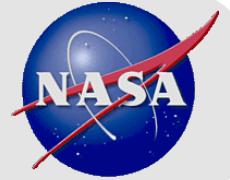


Introduction

- The Object Reentry Survival Analysis Tool (**ORSAT**) is the primary NASA computer code for predicting the reentry survivability of satellite and launch vehicles
- ORSAT assumes primitive shapes to compute drag and heating coefficients for orbital debris re-entry analysis
 - Most re-entry analysis includes hollow bodies
 - ORSAT does not currently account for flow through hollow bodies

Initial Objective:

- Use high fidelity computational tools to determine drag and heating coefficients for hollow bodies
- Determine a “hollowness” criterion that can be used in engineering model



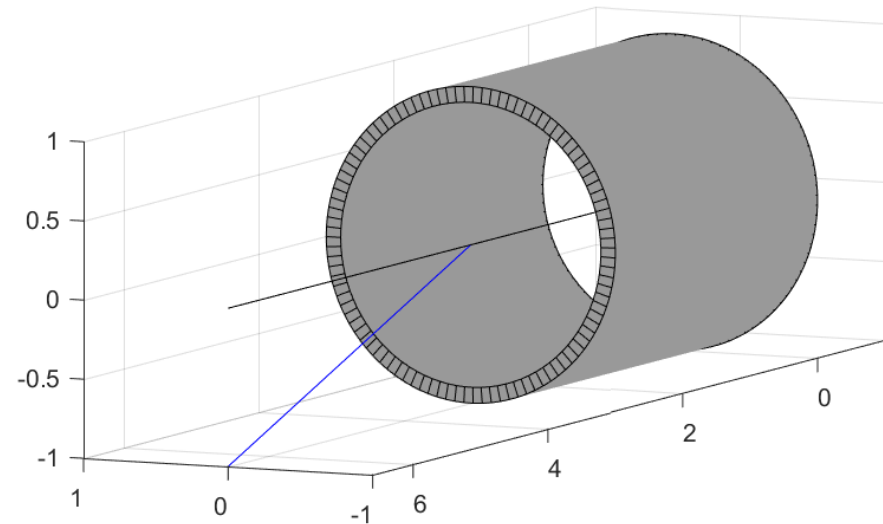
Background

- **Drag and aeroheating coefficients in the transition flow regime are extremely difficult to verify and validate**
 - Wind tunnel time is expensive and may not accurately capture all desired flow characteristics
 - CFD inaccurate for ‘high’ Kn; TPMC inaccurate for collisional flows
 - DSMC is also expensive (wall clock and CPU cycles)
 - We typically use transition functions
 - Sigmoid, log-sine, others common
- **If solid objects are difficult enough to model, how do we deal with hollow objects?**
- **And what does “hollow” mean?**



Background

- **We frequently deal with hollow objects in reentry simulations (pipes, telescopes, etc)**
 - Typically model these using same “solid” shape primitive, just with less surface area for drag and heating
- **But!**
 - Blockage due to leading edge shocks can increase drag on hollow objects
 - Heating on inner surface needs to be accounted for





Approach (Phase I)

- Use NASA JSC Direct Simulation Monte Carlo (DSMC) Analysis Code (DAC) to simulate hollow-bodied cylinders and prisms in rarefied flow
 - Determine drag and heating coefficients from results
 - Establish a “hollowness” criterion:

$$HC_1 = \frac{\dot{m}_{thru}}{\rho_{\infty} V_{\infty} A_{inner}}$$

$$HC_2 = \frac{\dot{m}_{thru}}{\rho_{\infty} V_{\infty} A_{outer}}$$

Input Quantity	Value
Altitude (km)	111.375
Freestream Speed (m/s)	7800
Freestream Density (kg/m ³)	7.61E-08
Freestream Temperature (K)	256.5
Wall Temperature (K)	300
Knudsen Number	0.2, 1, 10
Outer Diameter (m)	0.1, 1, 5
ID/OD ratio	0.1, 0.5, 0.95
Angle of attack (°)	0, 45, 90
Finess ratio (Length/Diameter)	0.1, 0.5, 1

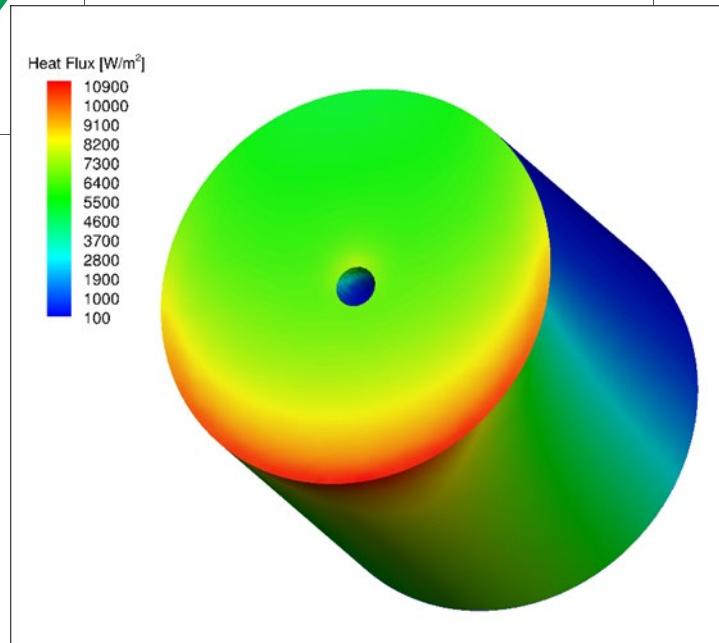
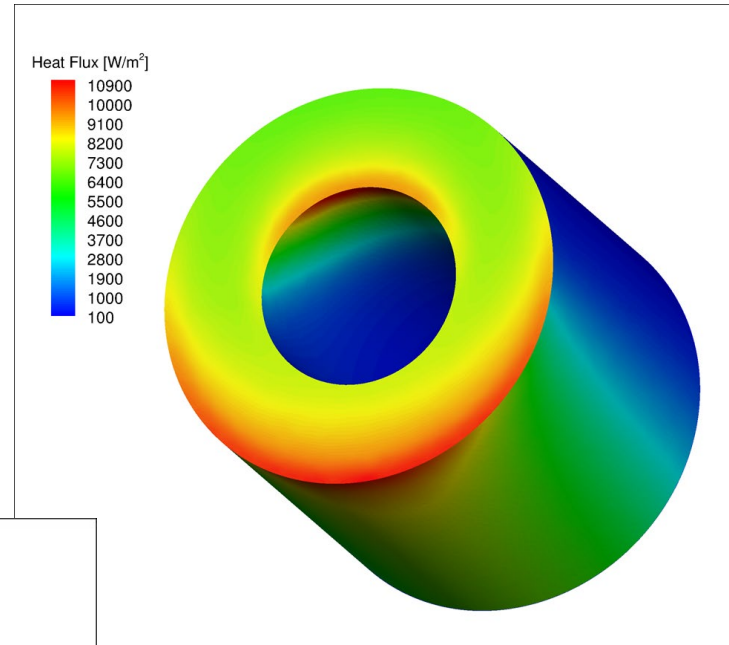
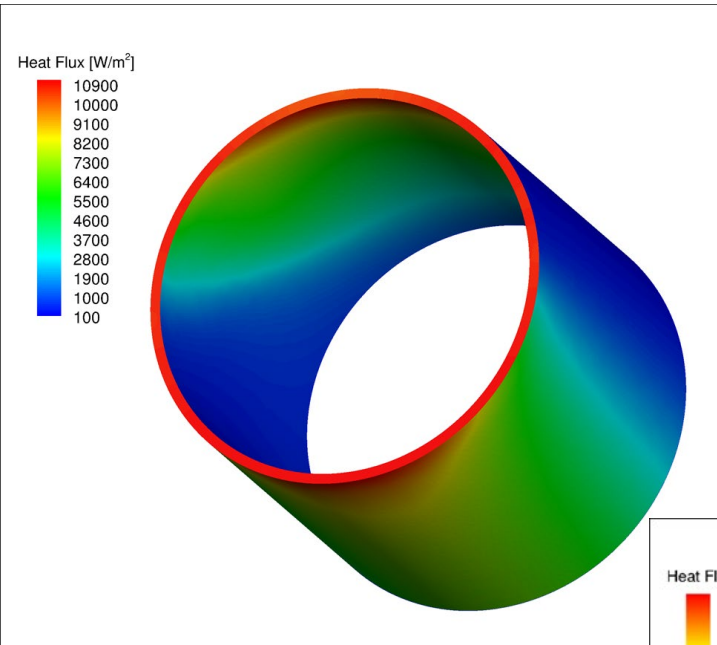


Results (1/7)

- Current total of 81 cases
- DAC simulations results shown:
 - Cylinder and Square Prism
 - 45° AoA
 - ID/OD = 0.1, 0.5, 0.95
 - Fineness ratio (L/D) = 1.0, 0.5, 0.1
 - Drag Coefficient carpet plots (function of ID/OD and L/D)
 - Kn = 10, 1.0, 0.2
 - Velocity contours (centerline slices) for Cylinder at 0° AoA
 - ID/OD = 0.1, 0.5, 0.95



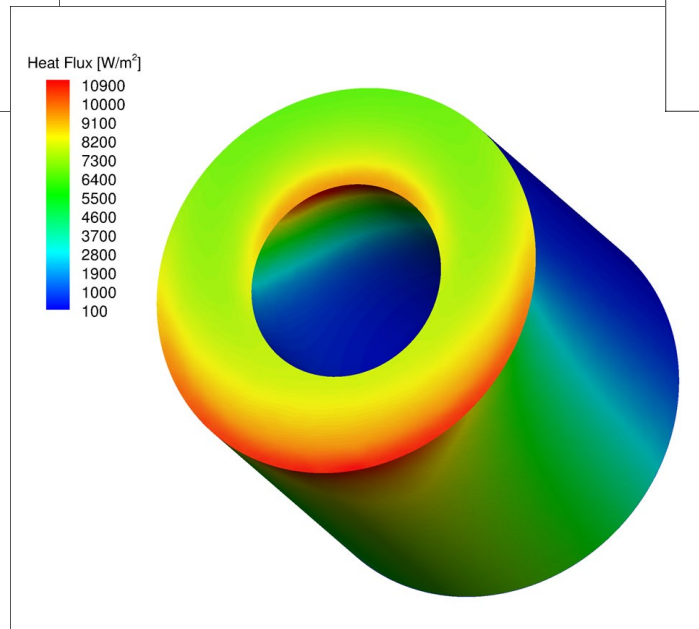
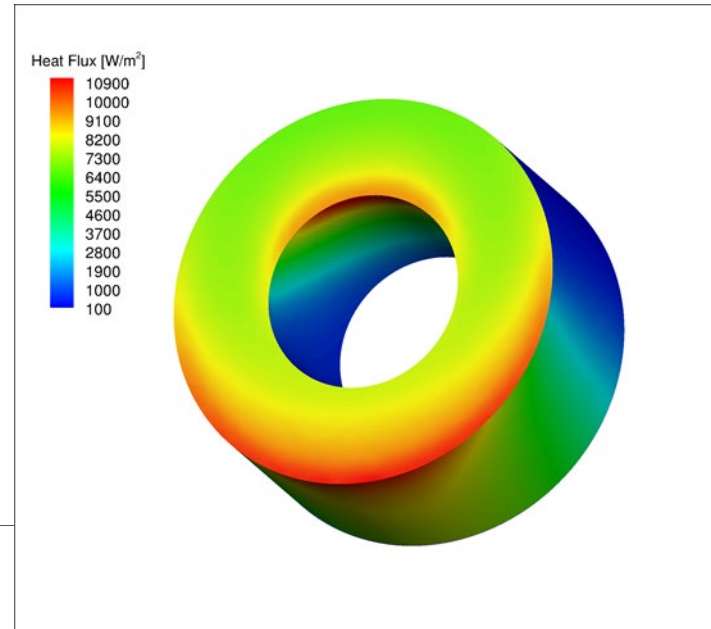
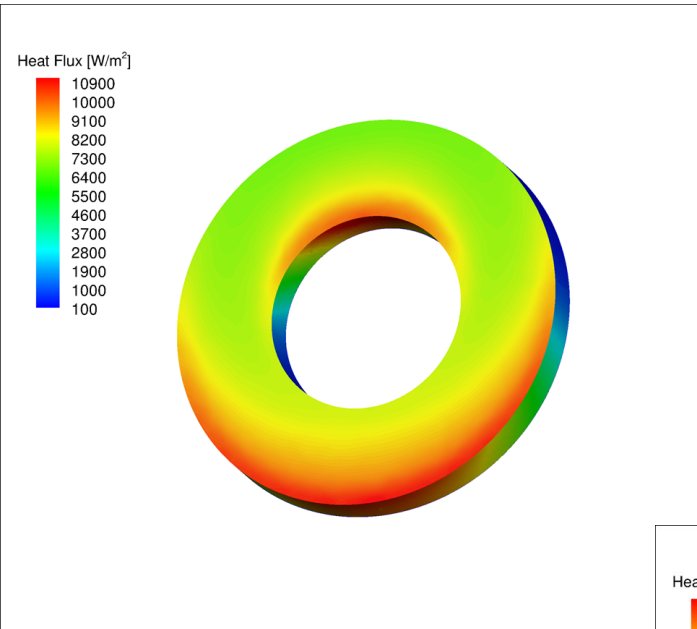
Results (2/7)



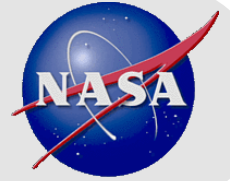
Same Kn
Same L/D
Varying ID/OD



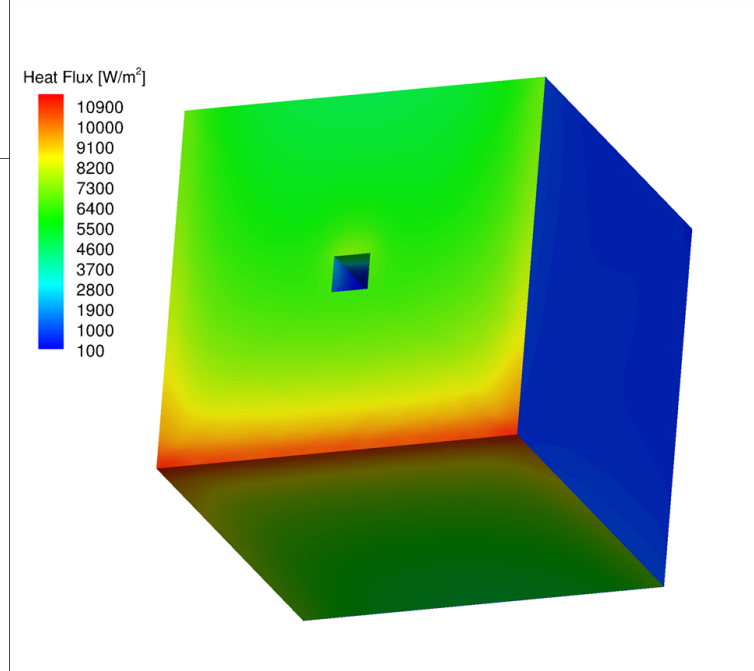
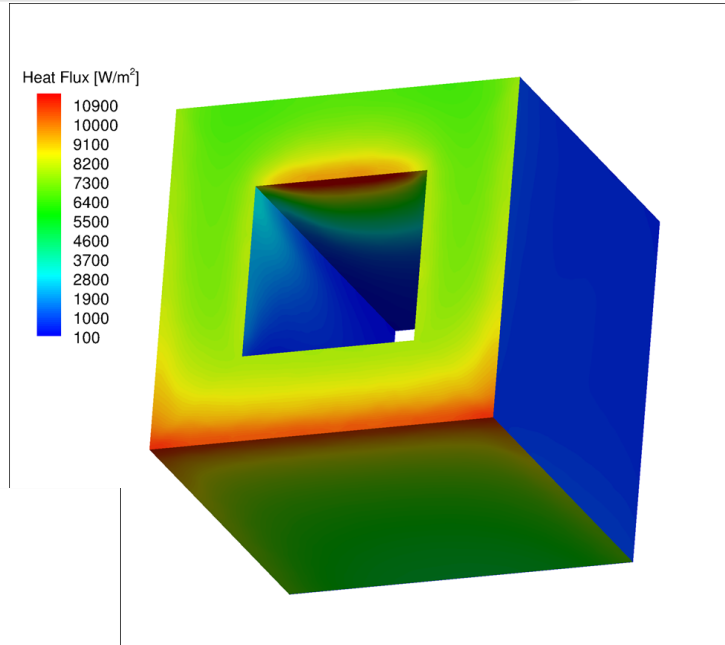
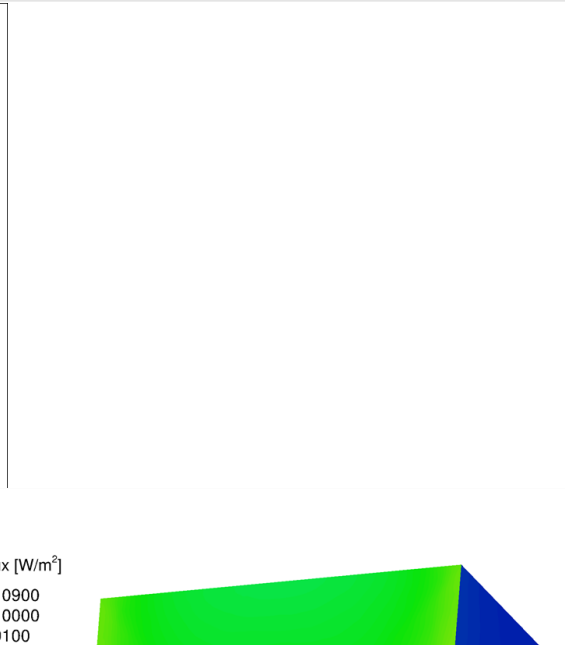
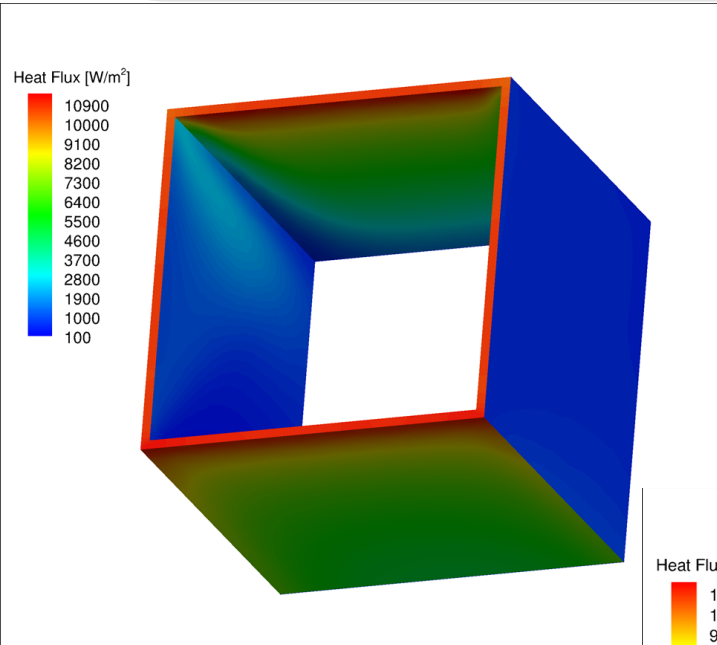
Results (3/7)



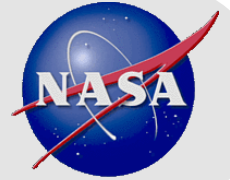
Same Kn
Same ID/OD
Varying L/D



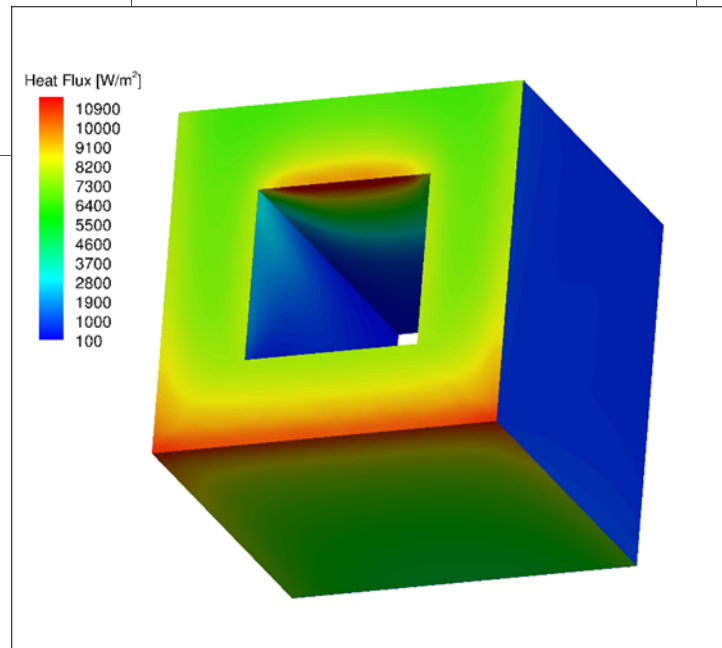
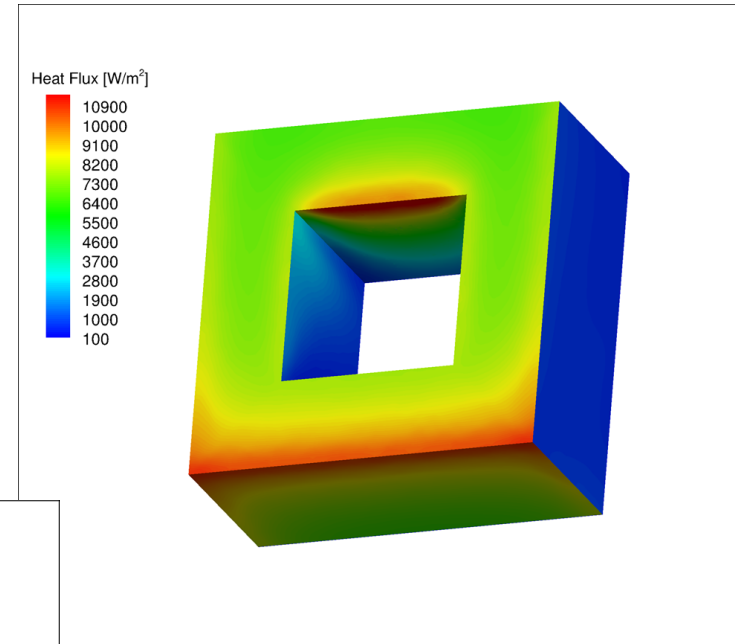
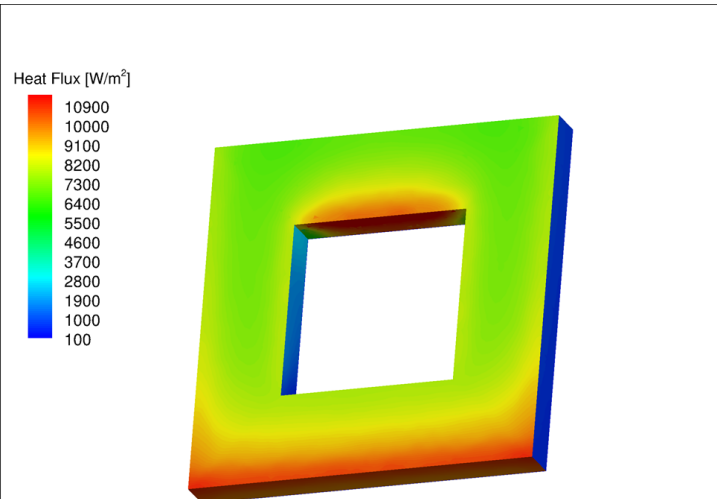
Results (4/7)



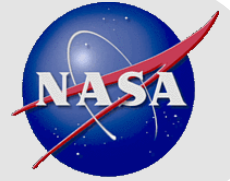
Same Kn
Same L/D
Varying ID/OD



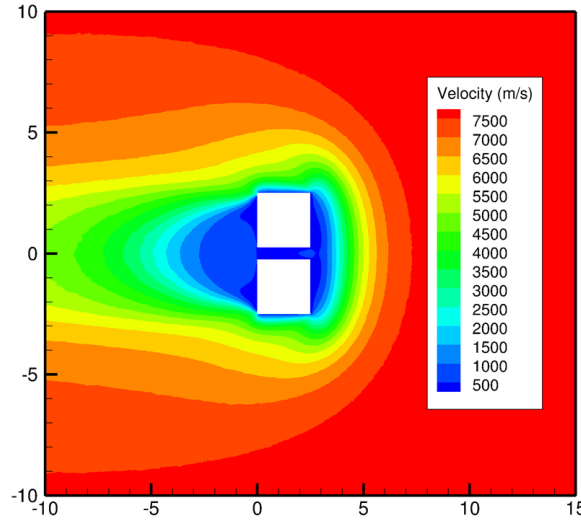
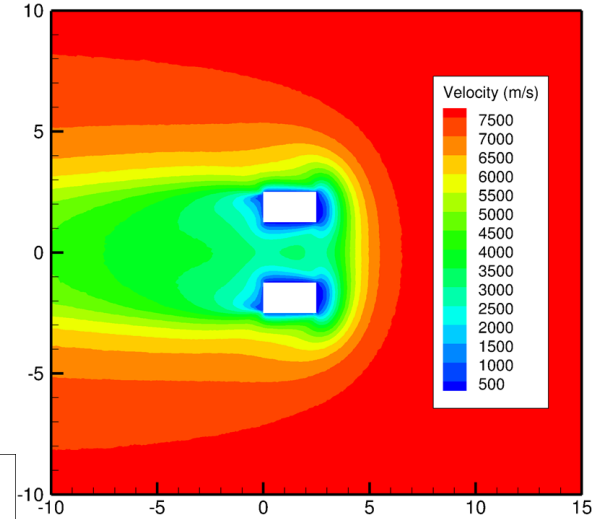
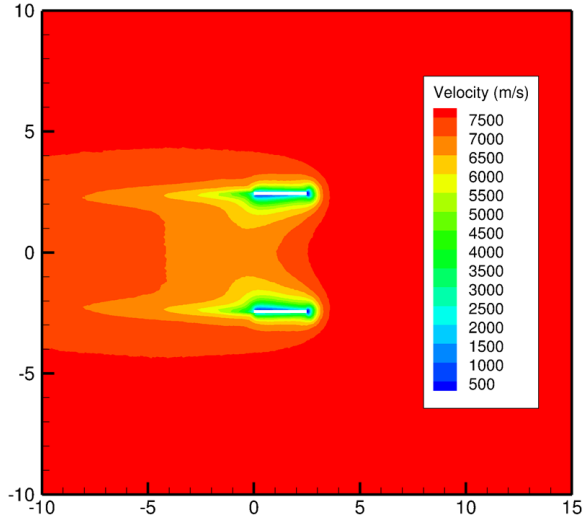
Results (5/7)



Same Kn
Same ID/OD
Varying L/D



Results (6/7)

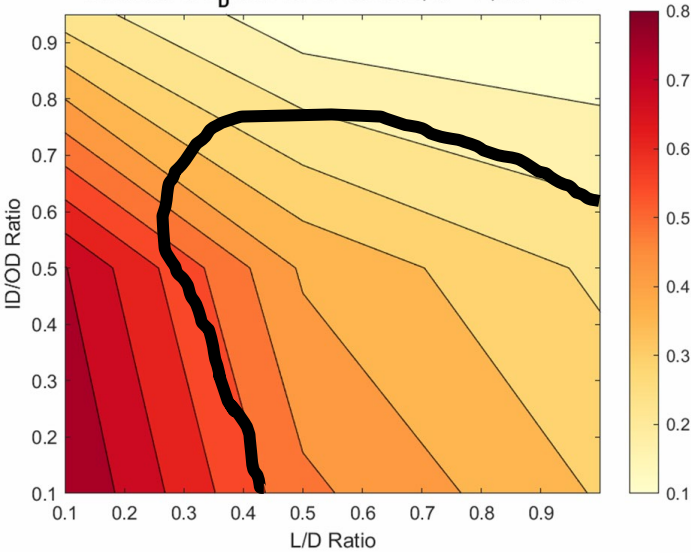


Same Kn
Same L/D
Varying ID/OD

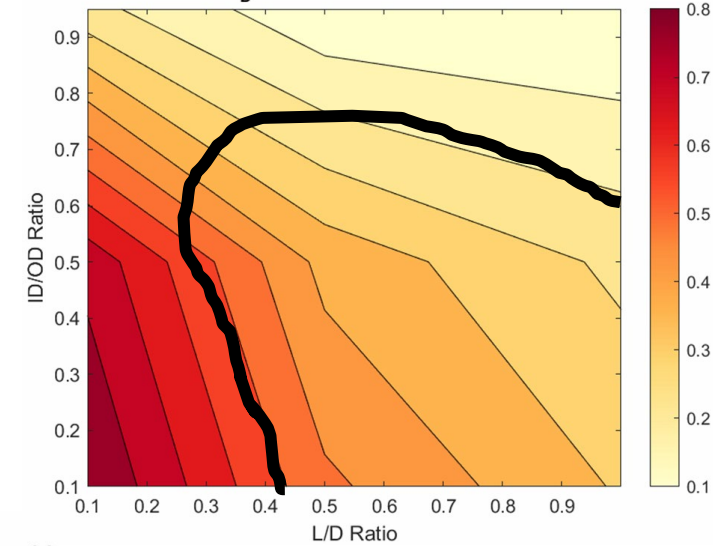


Results (7/7)

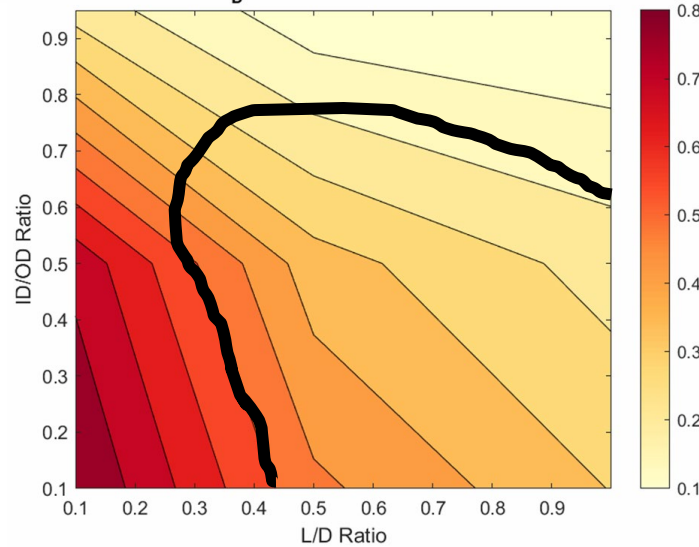
Variation of C_D with ID/OD and L/D, $\alpha = 0^\circ$, $Kn = 0.2$



Variation of C_D with ID/OD and L/D, $\alpha = 0^\circ$, $Kn = 1.0$



Variation of C_D with ID/OD and L/D, $\alpha = 0^\circ$, $Kn = 10$





Approach (Phase II)

- Continue DAC simulations of solid and hollow-bodied cylinders and prisms in rarefied flow
 - Determine drag and heating coefficients from results
 - Validate current transition flow model for solid bodies, expand hollow body model
 - Implement multi-dimensional database for use in ORSAT 7.0

Input Quantity	Value
Altitude (km)	95-112 km
Wall Temperature (K)	300
Knudsen Number	0.1, 0.5, 1, 5, 10
Outer Diameter (m)	1
ID/OD ratio	0.1, 0.5, 0.95
Angle of attack (°)	0, 22.5, 45, 67.5, 90
Fineness ratio (Length/Diameter)	0.1, 0.5, 1, 2, 5

1000 DAC simulations to be run

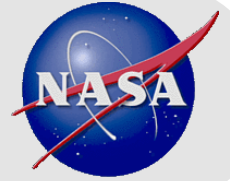


Summary

- DAC simulations were used to determine drag and heating coefficients for hollow bodied cylinders and square prisms with varying parameters
- Began quantifying effect of flow through hollow body to establish a “hollowness” criterion
- Developed sparse data tables to be used in the ORSAT aerodynamic and aerothermodynamic models
- Phase II includes new Knudsen numbers, geometric ratios and object orientations



Questions?



References

- **See Marichalar, J. and C. Ostrom (2019)**
 - <https://www.hou.usra.edu/meetings/orbitaldebris2019/orbital2019paper/pdf/6019.pdf>
- **Scanlon et al. 2015:**
 - "Simulations of rarefied and continuum hypersonic flow over re-entry objects," 8th European Symposium on Aerothermodynamics for Space Vehicles, Lisbon, Portugal, ESA Conference Bureau, 2015.