



CIMR COPERNICUS IMAGING MICROWAVE RADIOMETER

CIMR MISSION: AOCS CONTROLLED RE-ENTRY STRATEGY AND CHALLENGES



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PRESENTATION OUTLINE



CIMR Project Overview



AVS/AOCS Architecture



Controlled Re-entry Mode









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CIMR Project Overview: Introduction

/// Copernicus Imaging Microwave Radiometer project:

- / within the European Copernicus Expansion (CopExp) program
- *I* implemented by the European Space Agency (ESA) and the European Commission (EC)
- I currently in the C/D phase with Thales Alenia Space as prime contractor



Observations:

- Sea Ice Concentration/Extension (SIC/SIE)
- Sea Ice Thickness (SIT)
- Sea Surface Temperature (SST)
- Sea Surface Salinity (SSS)

I Performances:

- Multi-frequency, simultaneous acquisitions
- Unrivaled spatial resolution \rightarrow 5 to 60 km
- Excellent radiometry accuracy/resolution
- Global coverage \rightarrow 95% daily
- sub-daily revisit \rightarrow 6h













CIMR Project Overview: Mission concept

/// Orbit and Payload characteristics:

- / Sun-synchronous dawn/dusk operational orbit with:
- semi-major axis is such that the ground track is repeatable (orbital cycle duration of 29 days)
- frozen eccentricity and average altitude of ~ 817 km
- / Off-Zenith Angle (OZA): ~ 55 deg
- Instrument rotation **speed**: 7.8 rpm
- / Ground Swath: 1900 km















CIMR Project Overview: Spacecraft Multibody Layout



CIMR Project Overview: Space Debris Mitigation

/// Space Debris Mitigation:

- I CIMR Satellite design complies to Space Debris Mitigation Requirements (ISO 24113 – 2019)
- Casualty Risk Analysis results for Uncontrolled Re-entry are not compliant with the standard
- I Need for a Controlled Re-entry at EOL
- /// Design impacts:
- I Propulsion system capabilities (thrust level and propellant)
- Implementation of AOCS dedicated mode
- Subsystems reliability for additional functionalities and environment









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AVS/AOCS Architecture: Avionics Subsystem

Cofunded with

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1553 Bus



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CAN Bus Space Wire RF Signal		MTB: 400 Am ²	
	AVS Units		N. Items
	Gyroscope (GYR)		2
	Magnetometer (MAG)		2
	Multi-Head Star-Tracker (MHSTR)		3
	Cosine Sun Sensor (CoSS)		8
	GNSS Antenna (GNSS-A)		2

/// Actuators Sizing:

RWS: 0.2 Nm 50 Nms

GNS Reaction Wheel System (RWS) 4 Magnetic Torque Bar (MTB) 3 Momentum Compensation Assembly (MCA)



AVS/AOCS Architecture: Propulsion Subsystem

/// Reaction Control Thrusters:

- 6 x 1 N thrusters (3 main + 3 redundant) directed towards ±X axis and +Y axis \rightarrow used for **Orbital Correction Manoeuvres** (OCM)
- 8 x 20 N thrusters (4 main + 4 redundant) directed towards +Z axis with a tilt angle (to obtain torque authority around all the axis) \rightarrow used for High-Rate Damping Safe Mode and Re-Entry Mode

/// Propellant tanks:

- **Auxiliary tanks:** 2 x 104 I tanks, used in parallel for the satellite operational life and the first phase of perigee lowering
- Main tank: 177 I tank, entirely dedicated to re-entry for the second phase of perigee lowering and the last burn.

/// 20N THR performances (blowdown mode):

- / Thrust level: 24.5 N @ 24 bar, 7.8 N @ 5.5 bar
- **Specific Impulse**: 231 s @ 24 bar, 223 @ 5.5 bar







European Union







AVS/AOCS Architecture: AOCS Modes & Phases





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Controlled Re-entry Mode

/// THRUST_REM Mode:

- implements a robust technique to perform the re-entry manoeuvre, given **Delta-V program** uploaded by ground (resulting from trajectory optimization)
- I it can be entered only from NOM by ground tele-command
- I on-control units:
- MHSTR and GYR for attitude estimation (kinematic filter)
- 20N THR for attitude and orbital control during firing phase
- RWS for attitude control and MTB for momentum unloading during slew, cruise and drag phases

/// SAFE_REM Mode (FDIR):

- I guarantees the platform stability, solar illumination of solar panels and communications with ground
- I on-control units:
 - MAG/CoSS triad or MHSTR/GYR for attitude estimation
 - RWS low bandwidth attitude control and MTB for momentum unloading

/// Re-entry Reference attitude

- spacecraft –Z axis (thrusters' force) towards velocity
- spacecraft +Y axis (solar panels) towards orbital momentum (close to the Sun direction)













Controlled Re-entry Mode: Reference Trajectory

/// Perigee lowering:

- I series of short (efficient) controlled retro-burn manoeuvers at apogee for perigee lowering
- / perigee altitude from 800 km to 180 km
- I all manoeuvers last about 5 minutes



/// Last burn:

- *I* final **long** (inefficient) firing phase (FDIR inhibited)
- **/ perigee** altitude from 180 km to 50 km
- manoeuvre duration is about 40 minutes
- South Pacific Ocean inhabited area **splashdown**











Controlled Re-entry Mode: Slew phase

/// To change the spacecraft attitude in order to reach the firing pointing

- *I* pitch manoeuver of -90 deg (predefined time profile)
- I disturbance torque (mainly gravity gradient) counter-reacting \rightarrow RWS torque/momentum verified \checkmark

I internal angular momentum **unloading** \rightarrow MTB command verified \checkmark











Controlled Re-entry Mode: Orbital phases

/// Orbital phases \rightarrow AOCS Phases:

- *I* Apogee passages → retro-burn firing (FIRE)
- I Perigee passages → high drag torque (DRAG)
- I Coasting \rightarrow maintaining the attitude (CRUISE)

/// During the entire re-entry phase:

- / 27 manoeuvers are performed
- I the **payload** is off (no pointing accuracy requirements)
- I the instrument is controlled to a constant angular position (no rotation) → to minimize drag effects
- I always the same reference attitude is adopted → to minimize slew maneuvers and operation complexity















Controlled Re-entry Mode: Trajectory Simulation Test

/// Environmental disturbances analysis:

- *I* drag torque gives the main contribution especially at low altitudes
- *I* hypothesis for conventional attitude control:
 - RWS low control frequency (0.001 Hz)
 - unloading through MTB

results:

- MTB not able to fully de-saturate internal angular momentum at low altitudes
- internal angular momentum cumulates during the orbital period
- I the outcome is the need of the DRAG phase













Controlled Re-entry Mode: Critical Drag phase

/// Drag handling during perigee passages

- *I* the thrusters are not used, AOCS needs are related to **solar power and commun**ication
- I high disturbance drag torque reached during perigee passages is **controlled through RWS**
- I tuning through a **PID controller** with a preliminary control frequency of 0.001 Hz
- /// Last manoeuvers: drag becomes too high
- I attenuation of controller gains through a smooth switch function to avoid internal angular momentum saturation ✓
- ${\it I}$ target attitude is quickly restored within requirements \checkmark













Controlled Re-entry Mode: Firing phase

/// Thruster torque:

- *I* a **disturbance** torque is produced because of
- spacecraft mass properties knowledge
- spacecraft center of mass offset (variable with propellant mass)
- mounting position and orientation error
- RWs are not able to compensate it (> 1 Nm)
- *I* is **counteracted** by using a portion of the thrust force, tuning a PID controller, where:
- preliminary control frequency is 0.01 Hz
- integral term is able to find and compensate the disturbance torque ✓

/// Thruster force:

I follows the blow-down model: decreases with the pressure inside the tanks

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last burn lasts around 40 minutes









Controlled Re-entry Mode: Final Simulation Results

/// RWS requested torque:

- I feed-forward contributions:
 - estimated gyroscopic torque
 - estimated gravity gradient torque
 - angular momentum unloading (through MTB)
- I feed-back contribution:
- switching function for critical drag management
- disabled during firing

/// THR requested torque:

I PID attitude control during firing













Controlled Re-entry Mode: Final Simulation Results



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Controlled Re-entry Mode: Deployment Failure

/// Failure during deployment at BOL

/ Worst case scenario chosen in terms of higher center of mass displacement during the deployment phases

boom 2 stuck at 90 deg from stowed position



/// Assumptions for this analysis:

- **SCM angle** equal to zero (stowed default angle)
- Hinges blocked with infinite stiffness
- Perfect knowledge of **thrusters** position and orientations
- Perfect knowledge of center of mass position











Controlled Re-entry Mode: Deployment Failure

- **I** S/C center of mass position offset (X and Y axis) \rightarrow 200-300 mm towards –Y axis
- Single **thruster force** \rightarrow decreases in accordance with the blow-down model
- Produced disturbance torque with THR in a full firing mode \rightarrow up to 20 Nm on X-axis







- Thrusters modulation command \rightarrow fully compensate the unbalance
- I Manoeuver **thrust efficiency** \rightarrow the ratio between the real applied force and the nominal force











Conclusions: re-entry challenges and solutions

/// Propellant consumption

- I To minimize the propellant mass \rightarrow solution: to extend perigee lowering phase
- I but attitude control cannot withstand with high drag torque → solution: trade-off result is 180 km as min perigee altitude

/// Drag management

- I Disturbance drag torque at perigee passages \rightarrow solution: tuning PID controller using RWS
- I Internal **angular momentum** saturation → solution: controller gains' attenuation through a smooth switch function

/// Firing management

I Thrusters disturbance torque during firing phase \rightarrow solution: tuning PID controller using THR















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THANK YOU!











