

ESA's Space Debris Mitigation Requirements

Space Debris Mitigation Team

07/10/2024

ESA-TECQI-HO-2024-002968

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What to expect from today



A general lecture on space debris



A detailed engineering session

What to expect from today



A general lecture on space

Detailed engineering session

A (hopefully useful) overview of
ESA's Space Debris Mitigation
Requirements and related
verification methodologies

What to expect from today



Francesca Letizia



Emma Stevenson



Marco Papa



Daniele Bella



Calum Turner



Ines De Chiclana

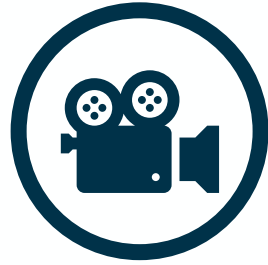


Sergio Ventura

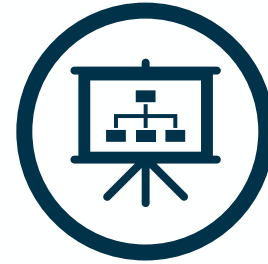


Stijn Lemmens

Housekeeping rules



This session is recorded



The slides will be distributed

On-site



Please keep questions for the end of the presentation



Online



Put your questions in the Q&A section of WebEx



The chat section is not monitored

Zero Debris Approach development

“*In ESA we are implementing a policy that, by 2030, we have a ‘**net zero pollution**’ strategy for objects in space, by consistently and reliably removing them from valuable orbits around Earth immediately after they cease operations. We need to **lead** by example here.*”

Josef Aschbacher, ESA Director General

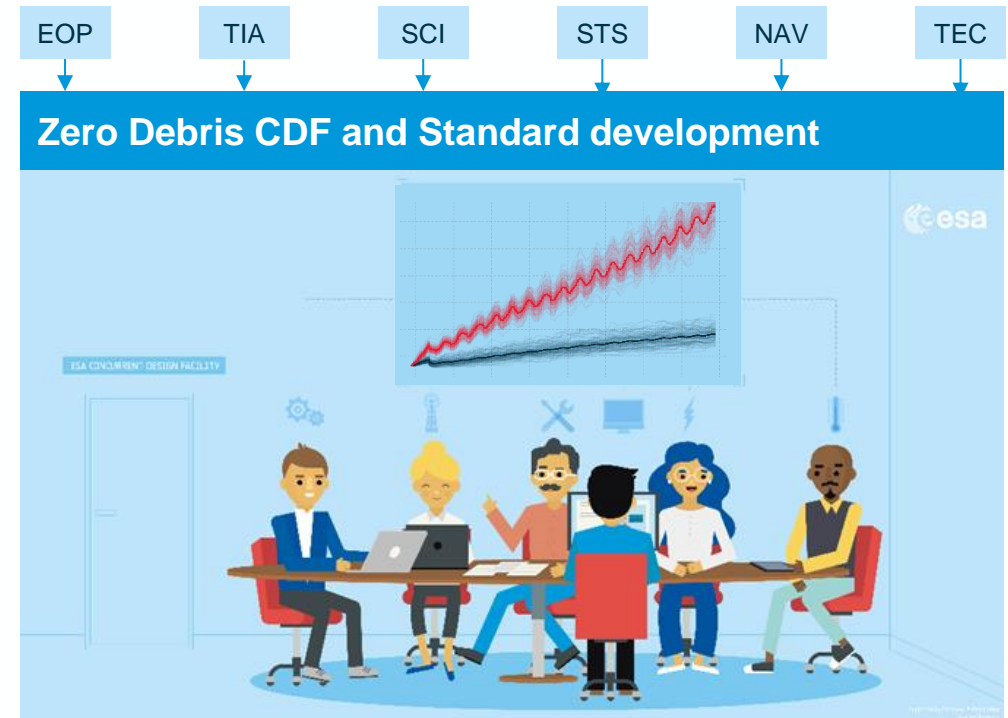


Policy update recommendations

considering environmental needs and impact on future missions, informed by an extensive **simulation campaign**



Roadmap for technical developments & standards, providing an estimation of the **resources** needed and a **phase-in schedule**



Developing ESA Zero Debris approach

Engaging partners, building a community

ESA SDM Policy & Standard



Technical requirements for ESA missions and contributions

ESA Technical Developments



ESA support to industry's transition and compliance to SDM standards

Zero Debris Technology Booklet



Crowd-sourced technical solutions to reach Zero Debris targets by 2030

Zero Debris Charter



Jointly defined principles and targets for long term space sustainability



Developing ESA Zero Debris approach

Engaging partners, building a community

ESA SDM Policy & Standard



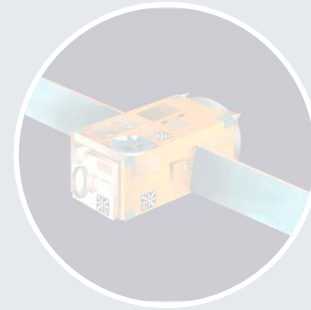
Technical requirements for ESA missions and contributions

ESA Technical Developments



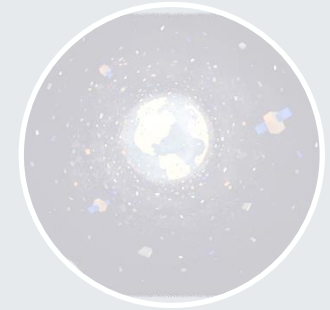
ESA support to industry's transition and compliance to SDM standards

Zero Debris Technology Booklet



Crowd-sourced technical solutions to reach Zero Debris targets by 2030

Zero Debris Charter



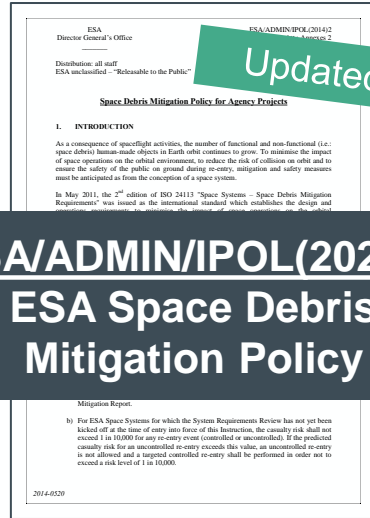
Jointly defined principles and targets for long term space sustainability



ESA Space Debris Mitigation Regulation status



- Policy
- Standard
- Handbook



Updated in 2023

ESA/ADMIN/IPOL(2023)1
ESA Space Debris Mitigation Policy



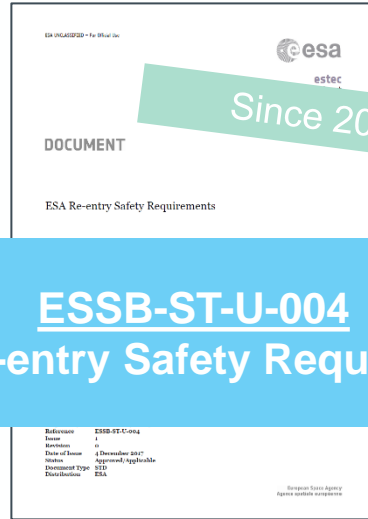
Born in 2023

ESSB-ST-U-007
ESA Space Debris Mitigation Requirements



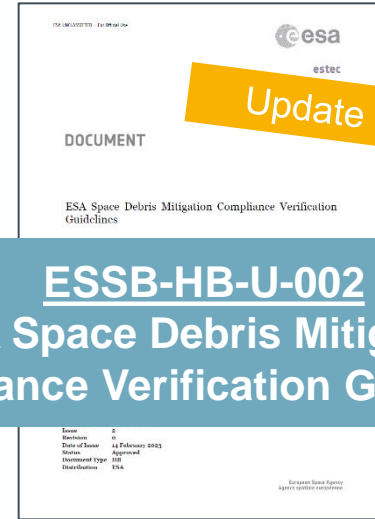
Updated in 2024

ECSS-U-AS-10C
Space sustainability - Adoption Notice of ISO 24113



Since 2017

ESSB-ST-U-004
ESA Re-entry Safety Requirements



Update in 2024

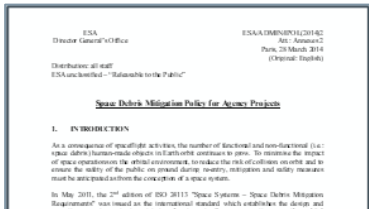
ESSB-HB-U-002
ESA Space Debris Mitigation Compliance Verification Guidelines



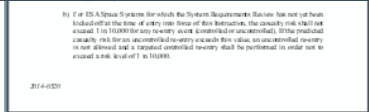
ESA's Space Debris Mitigation Policy



Who?



ESA/ADMIN/IPOL(2023)1
ESA Space Debris Mitigation Policy



Definition of the perimeter of applicability

ESA space systems, operations under ESA's responsibility, contribution to international activities, procurement of launch services



Applicable to all missions regardless of their phase



Introduction of the Space Debris Mitigation Assessment Board

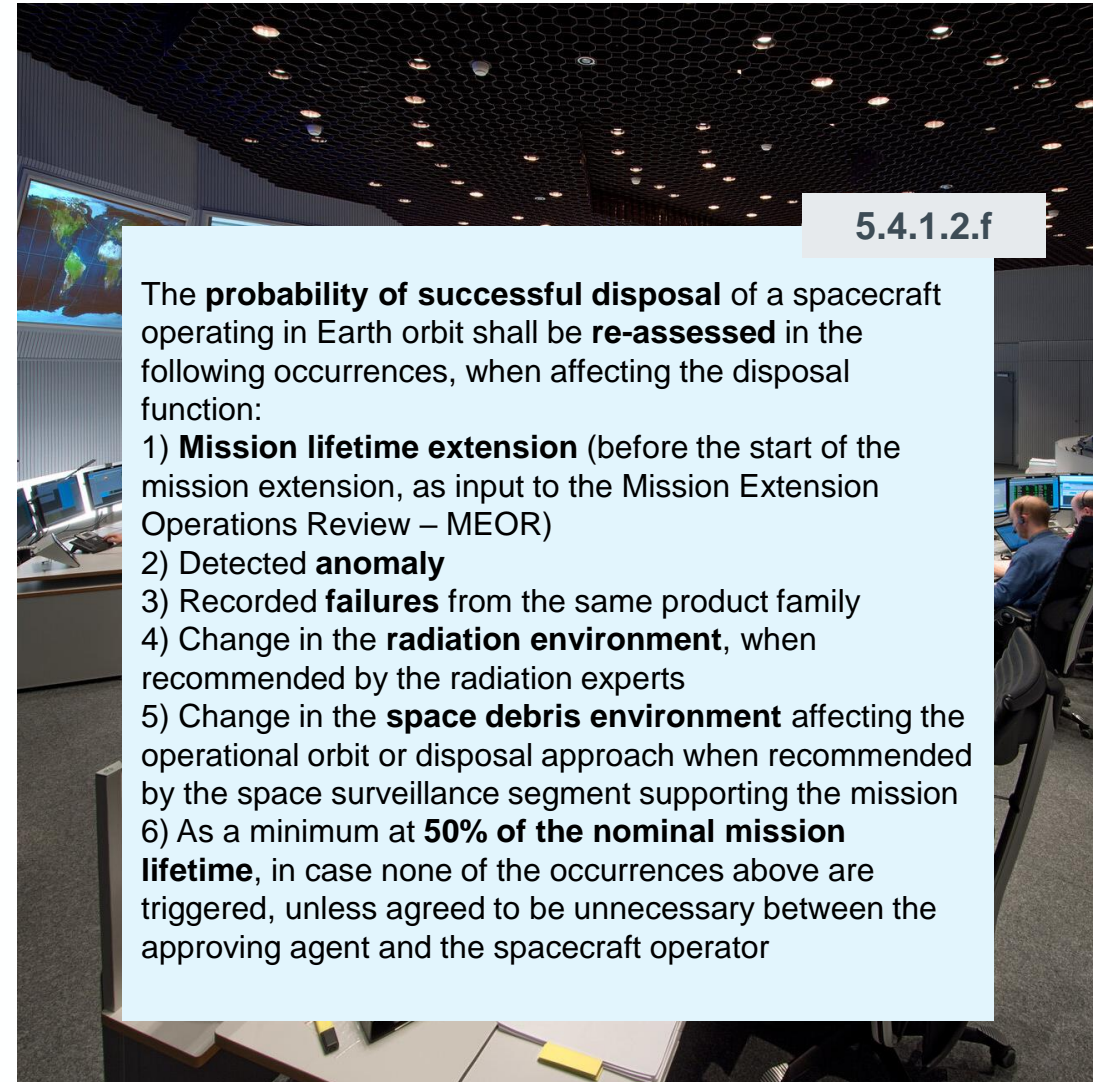
It provides recommendations in case of Mission Extension Reviews, anomalies affecting space debris mitigation measures, and requests for deviations/waivers

<https://technology.esa.int/upload/media/ESA-ADMIN-IPOL-2023-1-Space-Debris-Mitigation-Policy-Final.pdf>



If ESA's role is expected to end with the support to the mission development, then it is not our responsibility/role to monitor the implementation of operational requirements, and they are to be interpreted as

- **constraints** for the space/ground segment **development** i.e. the space segment has to have all the features/capabilities required to implement the operational requirements
- **guidelines/recommendations** for the **operators** on how to conduct operations in line with ESA's space debris mitigation principles.



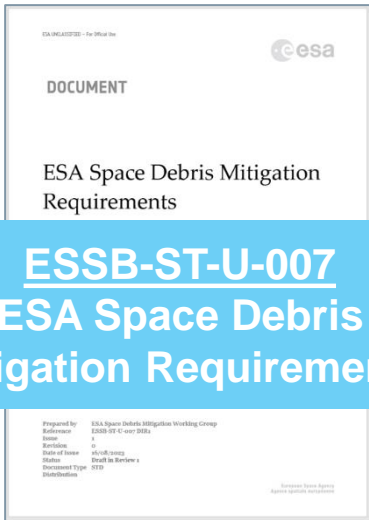
5.4.1.2.f

The **probability of successful disposal** of a spacecraft operating in Earth orbit shall be **re-assessed** in the following occurrences, when affecting the disposal function:

- 1) **Mission lifetime extension** (before the start of the mission extension, as input to the Mission Extension Operations Review – MEOR)
- 2) Detected **anomaly**
- 3) Recorded **failures** from the same product family
- 4) Change in the **radiation environment**, when recommended by the radiation experts
- 5) Change in the **space debris environment** affecting the operational orbit or disposal approach when recommended by the space surveillance segment supporting the mission
- 6) As a minimum at **50% of the nominal mission lifetime**, in case none of the occurrences above are triggered, unless agreed to be unnecessary between the approving agent and the spacecraft operator

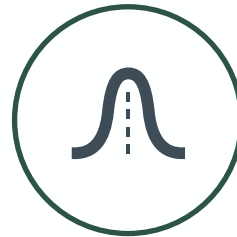
ESA's Space Debris Mitigation Requirements

What's new



Clearance criteria

- + **5 years in LEO**
- + Collision probability threshold
- + Apogee below 375 km for constellations
- + If graveyard, no crossing with known constellations



Probability of successful disposal

- + $\geq 90\%$ considering both **internal** (reliability) and **external** (impacts) factors
- + $\geq 95\%$ for large constellations
- + Monitoring and reassessment



COLA & STM

- + Encoding of current best practices (e.g. data sharing)
- + Recurrent manoeuvre capability in GEO, in LEO for high and very high-risk objects, and for constellations
- + Collision probability threshold for action $\leq 1:10000$



Design for removal

- + Preparation for removal for high-risk objects in the protected regions

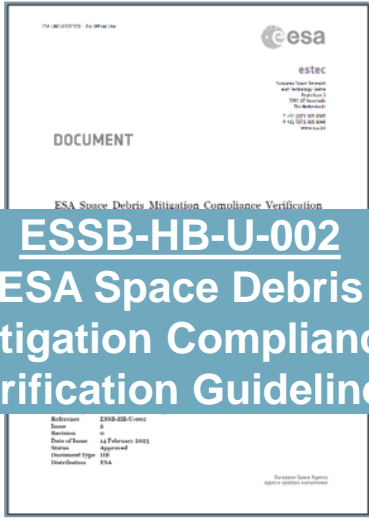
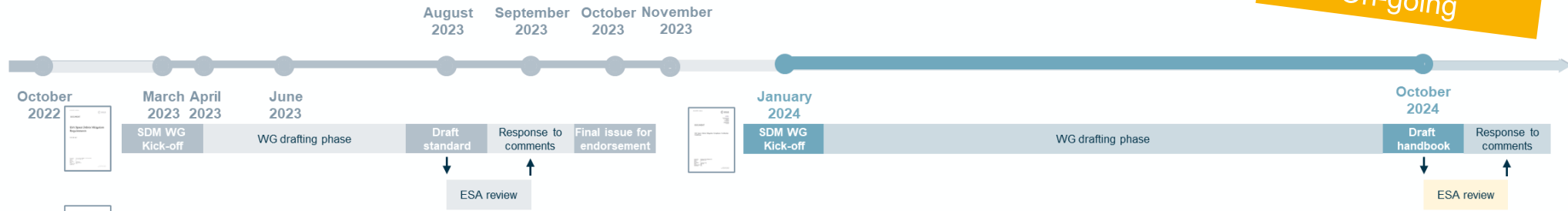
<https://technology.esa.int/upload/media/ESA-Space-Debris-Mitigation-Requirements-ESSB-ST-U-007-Issue1.pdf>

COLA: Collision Avoidance | STM: Space Traffic Management

ESA's Space Debris Mitigation Compliance Verification Guidelines

On-going

How?



ESSB-HB-U-002
ESA Space Debris Mitigation Compliance Verification Guidelines

Guidelines on suitable methodologies for verification

Indication of what's expected at the different mission phases

Revision of ESA's available tool for compliance analysis

Update/coordination of/with related documents

drama

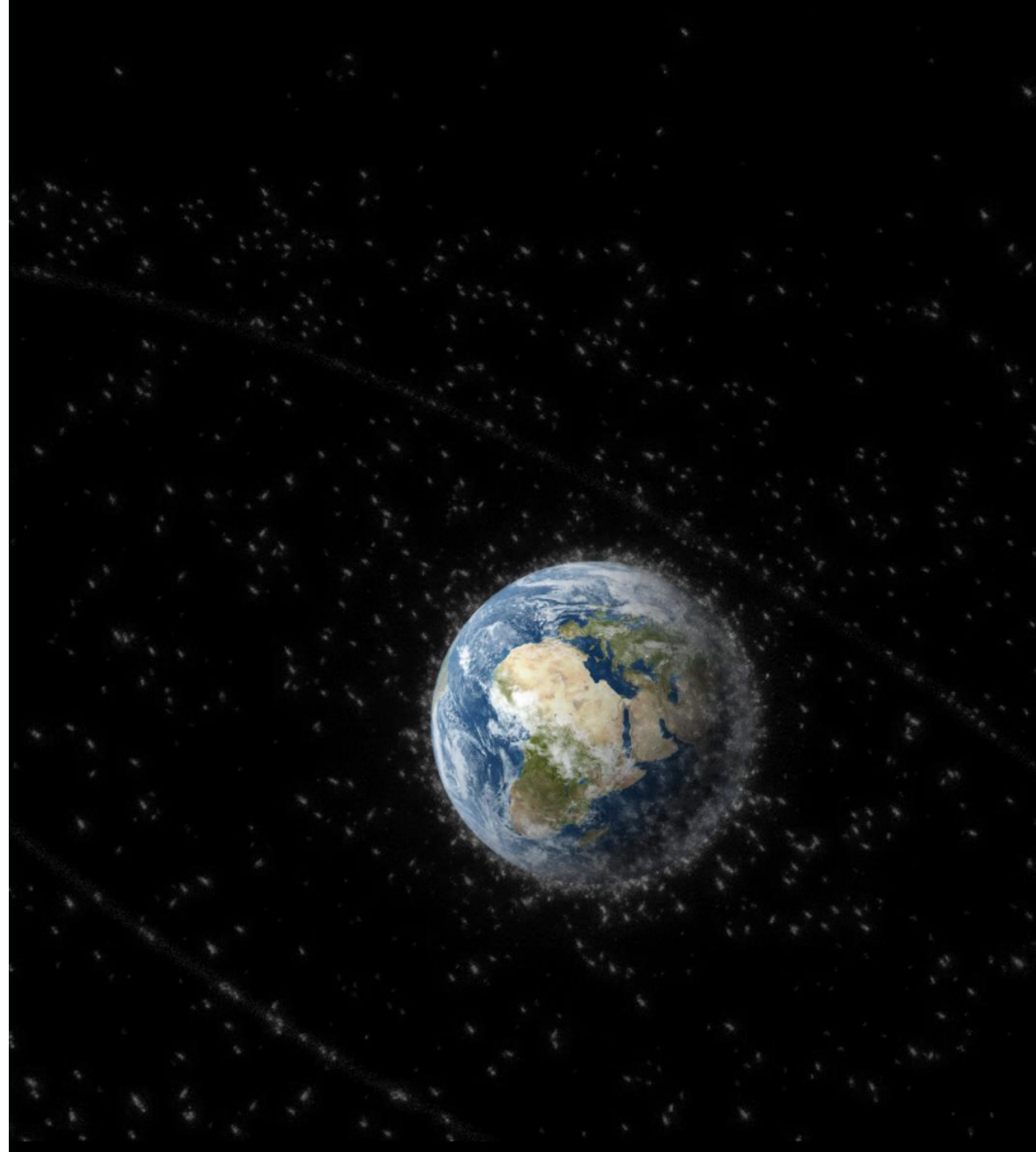
Update & planned releases to support analyses

Design-for-Demise, Close Proximity Operations

ESA's Space Debris Mitigation Toolkit

SPACE DEBRIS MITIGATION REQUIREMENTS

a bit more in detail



The Document



Frontmatter
Introduction, scope, definitions

Verification & Validation requirements

Indications on key models and data inputs for the required analyses

(complementing ESSB-HB-U-002 ESA Space Debris Mitigation Compliance Verification Guidelines)

Documentation requirements
Including expected content for reporting

Principles
Rationale for each requirement

Space Debris Mitigation Requirements
Space debris release, Avoid breakups in Earth orbit, Disposal, Re-entry, Dark and quiet skies, Lunar orbits

Requirement Applicability Matrix
Requirement mapping based on orbital region and object type
Comparison wrt ISO24113:2023 and ECSS-U-AS-10

The collage displays several pages from the document, including:

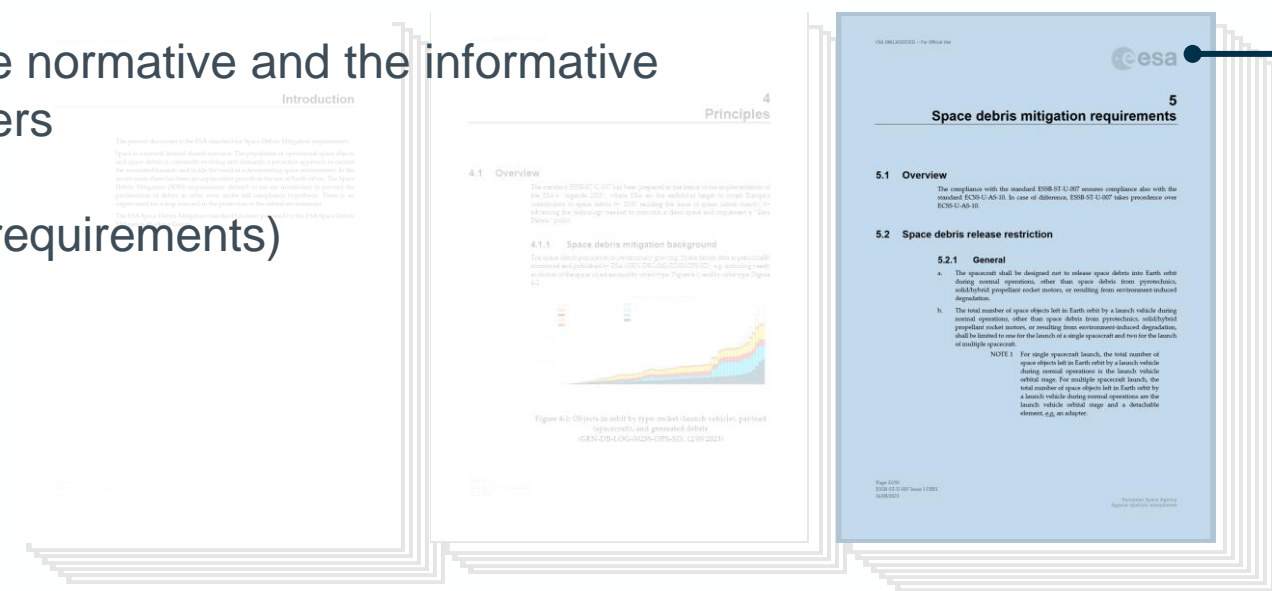
- Page 4: Introduction** - The present document is the ESA standard for Space Debris Mitigation requirements. It is a natural logical shared resource. The population of operational space objects and space debris is constantly evolving and demands a proactive approach to control the associated hazards and reduce the level of a deteriorating space environment.
- Page 5: Principles** - The ESB-S1-007 standard defines the space debris mitigation requirements based on identified space environmental risk conditions, aiming at effectively mitigating the current risk specific to orbital regions, and preventing the future risk increase.
- Page 6: Verification and validation requirements** - This clause provides requirements on the method to perform the compliance verification by analysis of the requirements defined in clause 5, which are based on assessment of the orbit lifetime, and cumulative collision probability. This clause specifies reference data, models, configurations and inputs.
- Page 7: Documentation requirements** - The Space Debris Mitigation documentation shall include:
 - The Space Debris Mitigation Plan (SDMP), that defines how the compliance with the Space Debris Mitigation requirements is planned, and is provided for review and approval by approving agent as specified in Table 2-1.
 - The Space Debris Mitigation Report (SDMR), that defines how the compliance with the Space Debris Mitigation requirements is implemented and verified, and is provided for review and approval by approving agent as specified in Table 7-1.



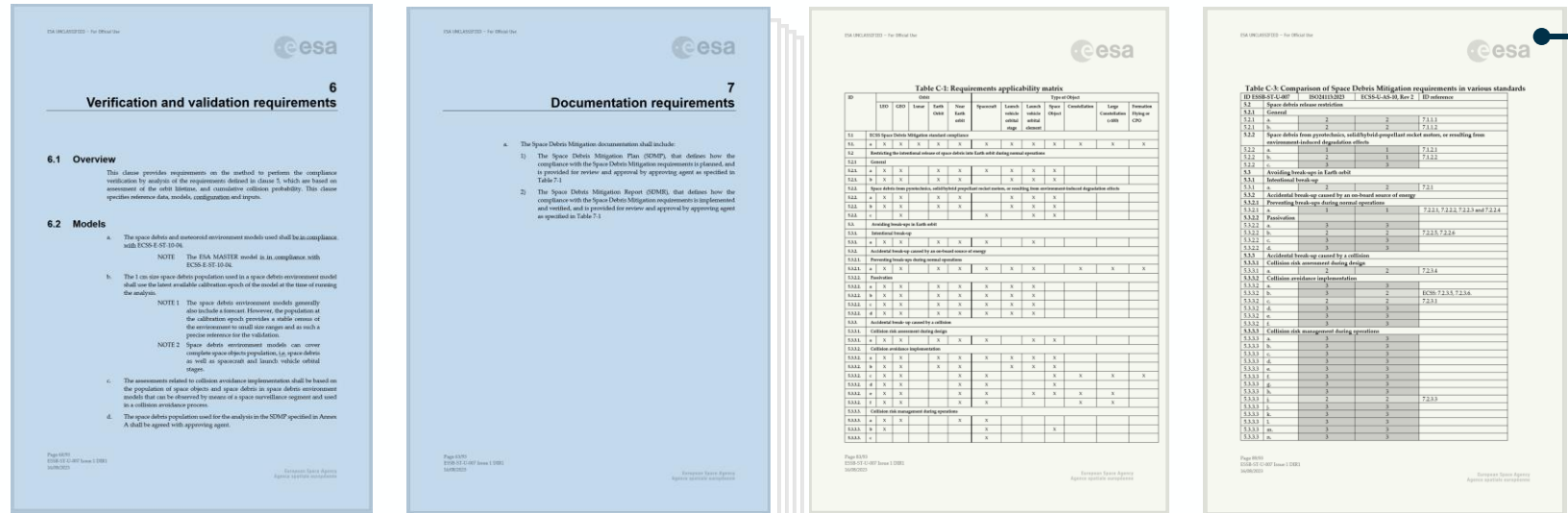
A clarification on the Document



In case of discrepancies between the normative and the informative sections, the normative is what matters (e.g. with respect to the mapping of requirements)



Normative



Informative




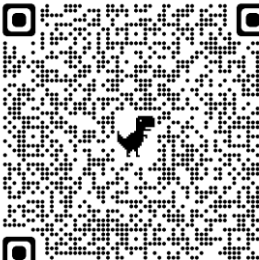
Do you have the requirements in excel/DOORS format?



FREQUENTLY ASKED QUESTION

Yes, both a DOORS version (ESA internal link only) and Excel version are available for download.

The Excel version is a compliance matrix template with already indicated of the apportionment of requirements between space and ground segment/operations.

C	D	E	F	G	H	I	J	K	L	M	N
ESSB Req. Identifier	Requirement	Text of Note of Requirement	Category	Note to category	Owner	Compliance status (C/PC/NC/NA)	Verification method(s)	Justification	Close-out Reference	Close-out Status	Additional Remarks
1	5.2.1a	The spacecraft shall be designed not to release space debris into Earth orbit during normal operations, other than space debris from pyrotechnics, solid or hybrid propellant rocket motors, or resulting from environment-induced degradation.	Design								
2	5.2.1b	The total number of space objects left in Earth orbit by a launch vehicle during normal operations, other than space debris from pyrotechnics, solid or hybrid propellant rocket motors, or resulting from environment-induced degradation, shall be limited to one for the launch of a single spacecraft and two for the launch of multiple spacecraft.	Design								https://technology.esa.int/page/space-debris-mitigation
3	5.2.2a	Pyrotechnics shall be designed not to release space debris larger than 1 mm in their largest dimension into Earth orbit.	Design								
4	5.2.2b	Solid or hybrid propellant rocket motors shall be designed and operated not to release space debris larger than 1 mm in their largest dimension into Earth orbit.	Design								
5	5.2.2c	A spacecraft or launch vehicle orbital element operating in the GEO protected region with a continuous or periodic presence shall be designed not to release space debris larger than 1 mm in their largest dimension resulting from the environment-induced degradation of adhesives and hook and loop fasteners for an orbit lifetime of 50 years including normal operations and after the disposal.	Design								
6	5.3.1a	In Earth orbit, intentional break-up of a spacecraft or launch vehicle orbital element shall not be performed.	Design								
7											

ESA internal link





Classical requirements with specified thresholds/**targets**

Pyrotechnics shall be designed not to release space debris larger than 1 mm in their largest dimension into Earth orbit.

Intentional break-up of a spacecraft or launch vehicle orbital element shall not be performed.

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall be designed to guarantee a probability of successful passivation through to the end of life of:

- 1) At least 0,90
- 2) At least 0,95, when operating in the LEO protected region in an orbit with a natural orbital decay duration longer than 25 years
- 3) At least 0,95, when operating in the GEO protected region



Seed requirements i.e. request of quantification/assessment

During the design, the developer of a spacecraft operating in near Earth orbit with a recurrent manoeuvre capability shall quantify the operational impact during normal operations due to conjunctions.

The developer of a spacecraft or launch vehicle orbital element injected in near Earth orbit shall quantify:

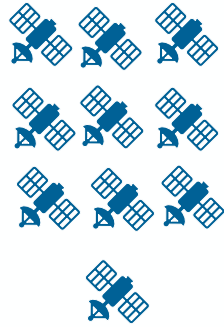
- the expected number of conjunctions at 10^{-4} and 10^{-6} collision probability threshold,
- the estimated number of collision avoidance manoeuvres triggered thereby on other spacecraft during normal operations and after end of life until re-entry or up to 100 years.

ESSB-ST-U-007 scope: space system type



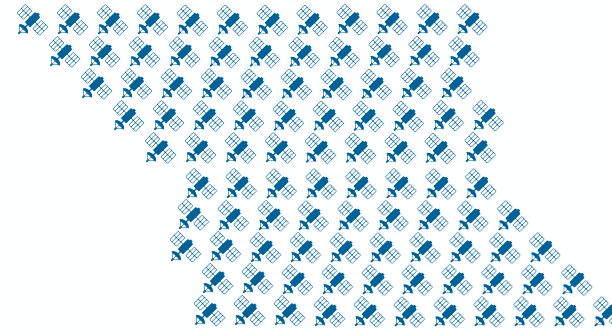
Single spacecraft

Request for collision avoidance capability in GEO and LEO if high or very high risk



Constellation (≥ 10 spacecraft)

Request for collision avoidance capability in near-Earth orbit



Large constellation (≥ 100 spacecraft)

System reliability > 0.95
In LEO, disposal below 375 km and injection orbit with natural decay time < 5 years

Re-entry casualty risk per spacecraft $< 1:10^6$

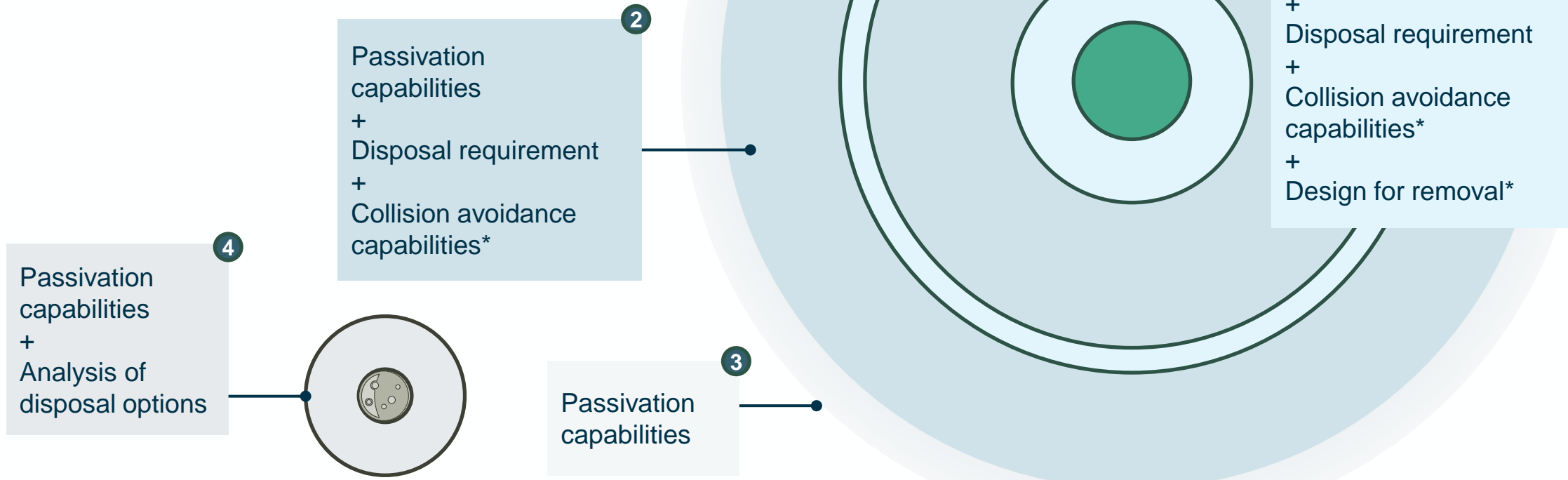


Launch vehicle (including elements, and orbital stages)

ESSB-ST-U-007 scope: orbital regions

examples

- 1 Protected regions (i.e. LEO and GEO)
- 2 Near-Earth orbits (perigee < 100000 km)
- 3 Earth orbits (including Libration Point Orbits)
- 4 Lunar orbits (including Libration Point Orbits)



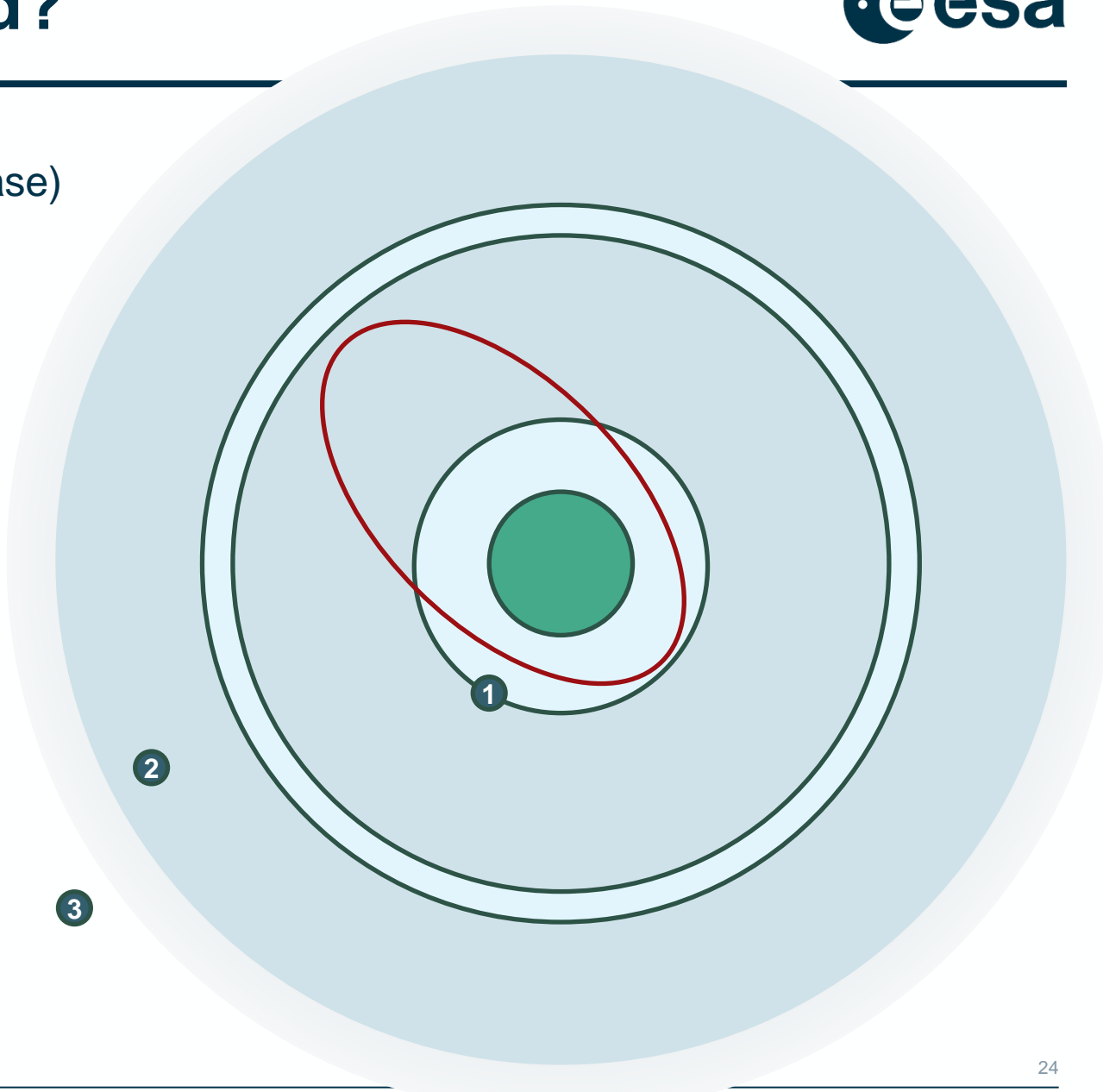
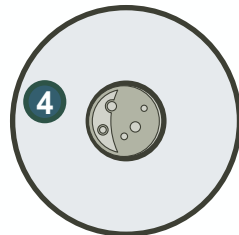
*for objects not at low risk

How are GTOs and HEOs treated?

Distinction between **operating** (active and in the region), **crossing** (inactive and in the region), **injected into** (release)

Example

A spacecraft injected into a GTOs and performing a (low-thrust) orbit raising up to its operational slot in GEO is **operating in LEO** for the initial phase of its mission and the corresponding requirements shall be verified



GTO: Geostationary Transfer Orbit | HEO: High Eccentric Orbits

LIFETIME

High risk

natural orbital decay duration
between 5 and 25 years

Medium risk

natural orbital decay up to 5 years
and crossing altitudes above 375 km

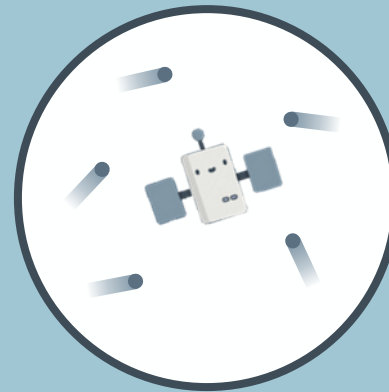


Very high risk

natural orbital decay duration
longer than 25 years

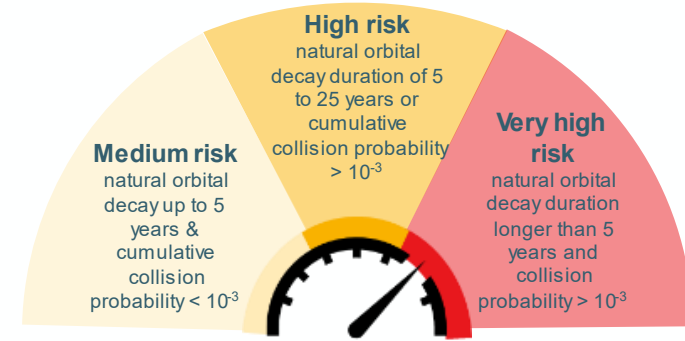
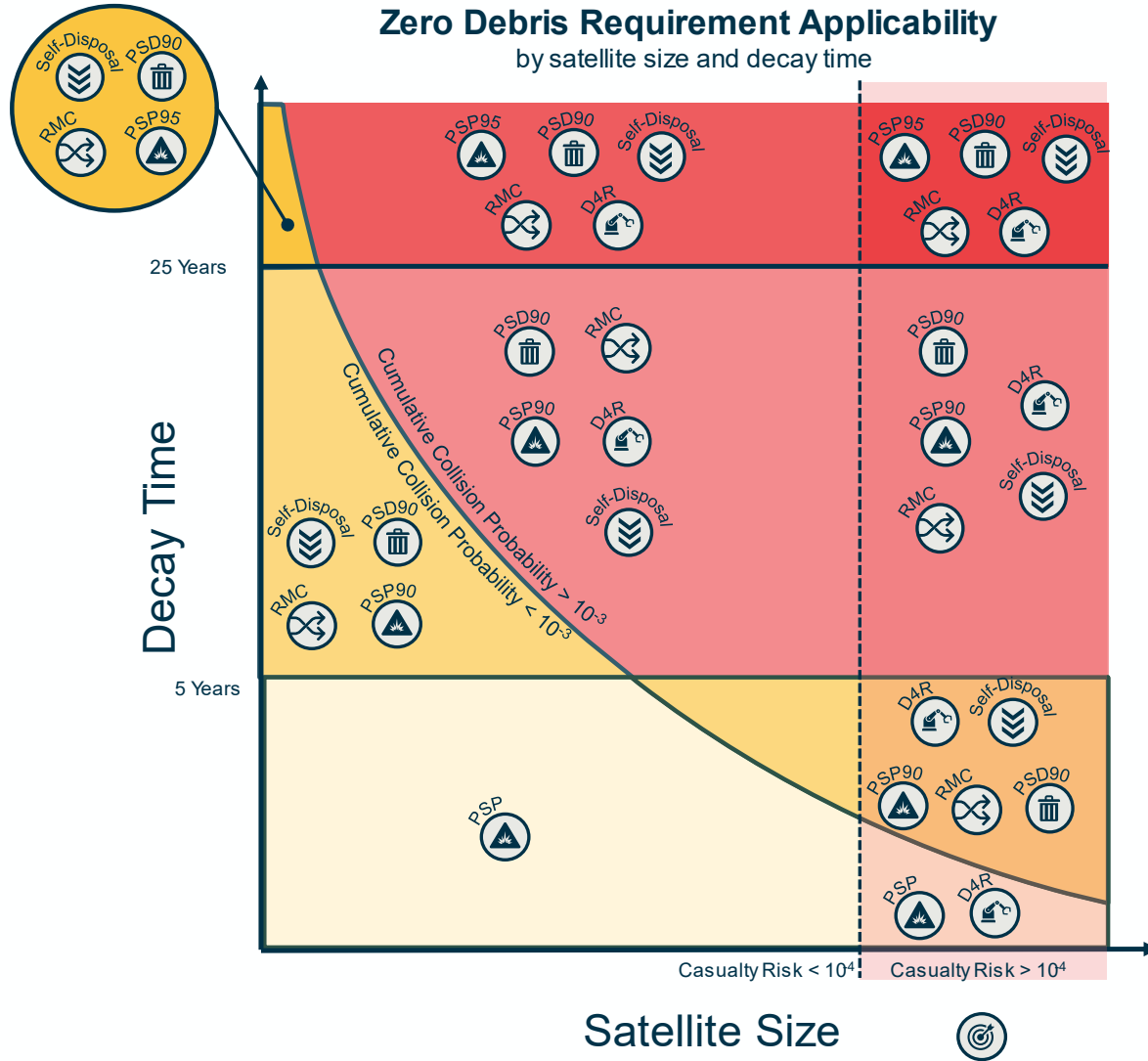
COLLISION PROBABILITY

Collision probability with
space debris objects
larger than **1 cm**



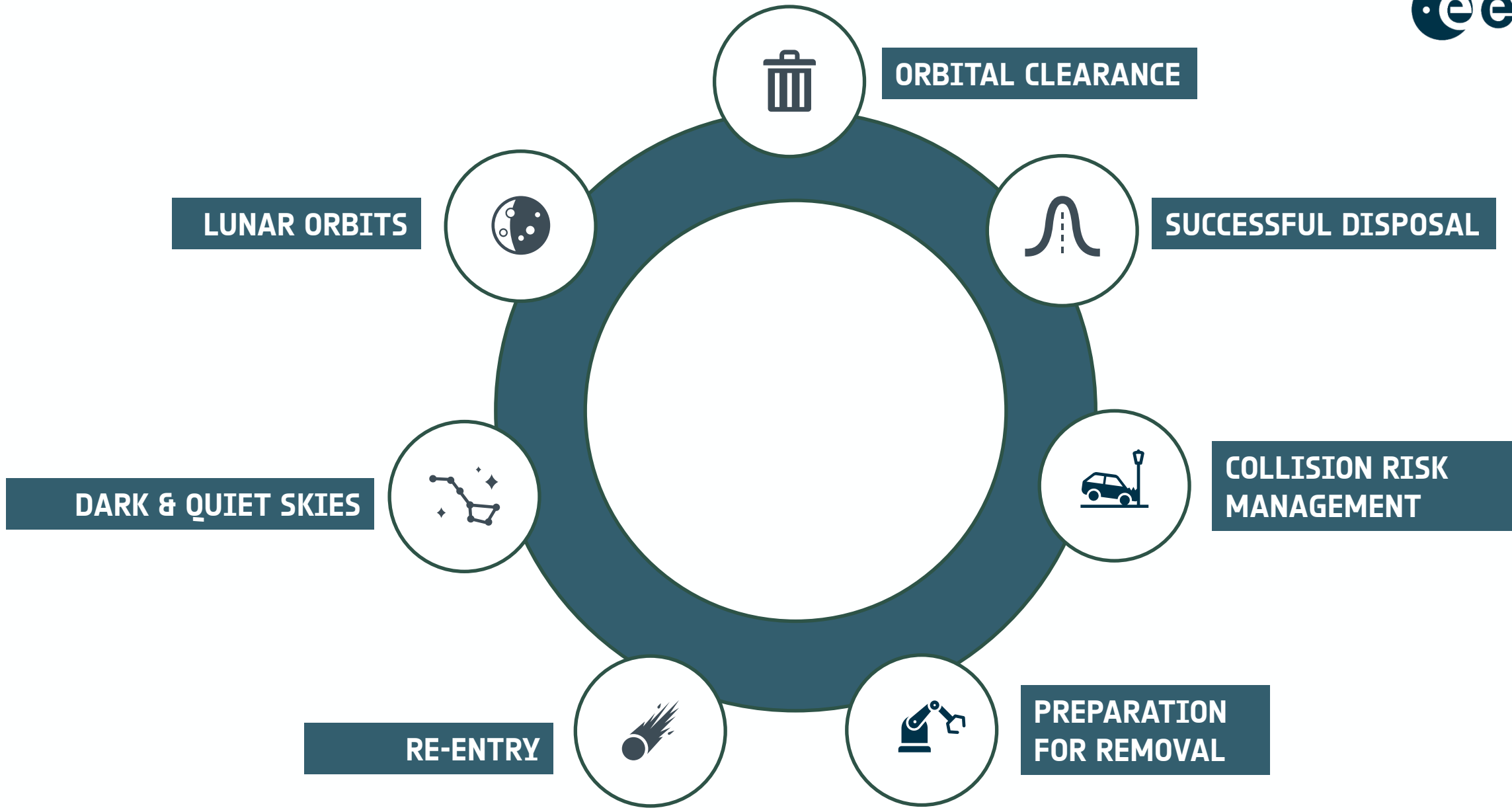
A space object in Earth orbit
without capability of performing
collision avoidance manoeuvres
and with a cumulative collision
probability with space objects
larger than 1 cm above **1 in 1000** is
considered **environmentally
hazardous**.

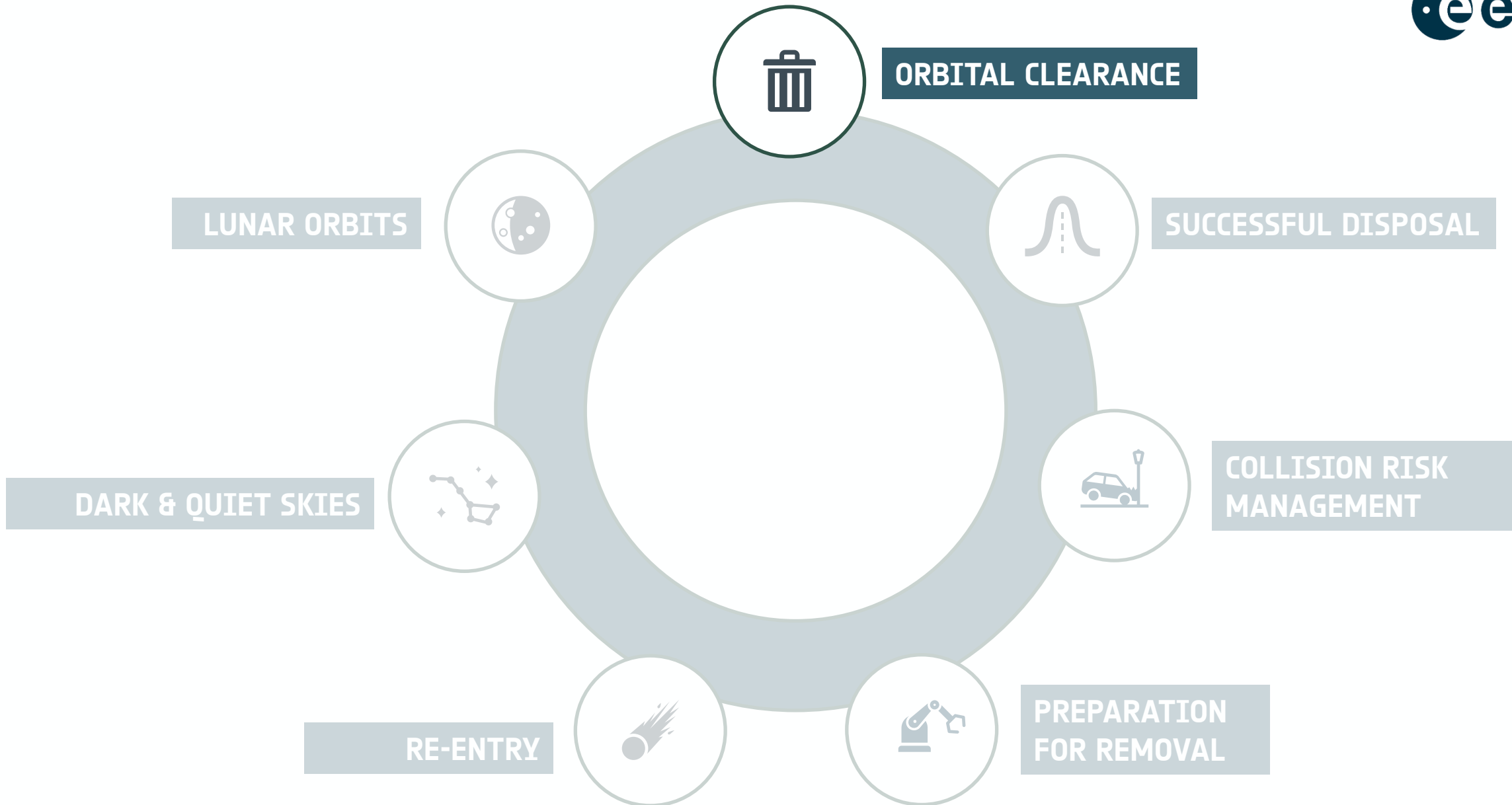
ESSB-ST-U-007 rationale – example for single satellite



Key

- PSD90: Probability of Successful Disposal $> 90\%$
- DAD: Design for Demise
- DAR: Design for Removal
- RMC: Recurrent Manoeuvre Capability
- PSPX: Probability of Successful Passivation $> X\%$
- Self-Disposal: Self-Disposal Capability
- Controlled re-entry





LEO clearance: lifetime limitation



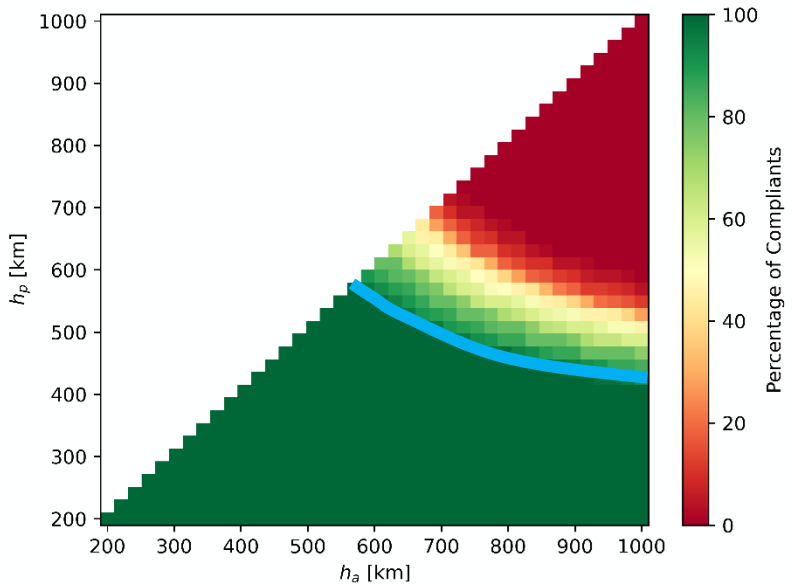
5.4.2.3.a

LEO protected region clearance
 a. The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:
 1) the orbit lifetime is less than 5 years [...]
 [...]

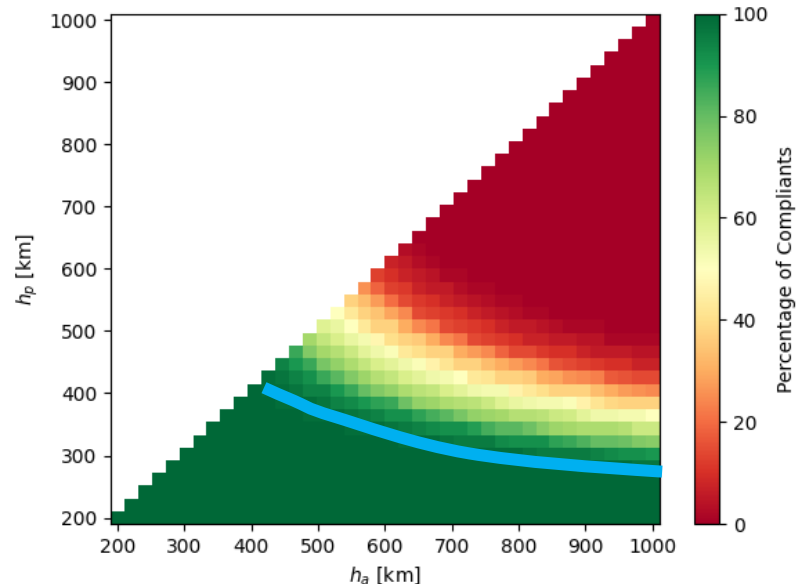


Requiring a faster passive reentry will **lower the orbital altitude needed for disposal**, which depends on the satellite characteristics

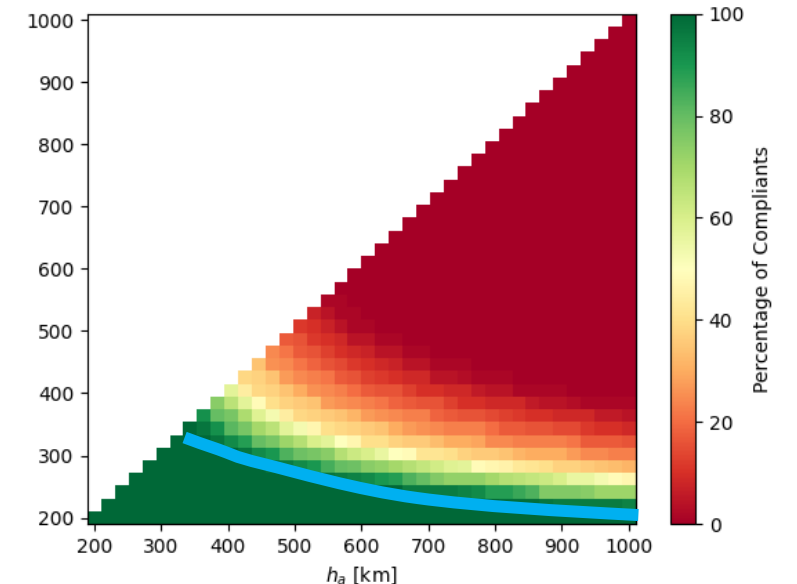
25 Years



5 Years



1 Year



Ballistic coefficient linearly sampled between 10th and 90th percentile of the values seen in LEO | Disposal epoch sampled across solar cycle
 Inclination sampled between 0 and 180 degrees, drag coefficient = 2.2, reflectivity coefficient = 1.3



LEO clearance: lifetime limitation



novelty level



5.4.2.3.a

LEO protected region clearance

a. The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:

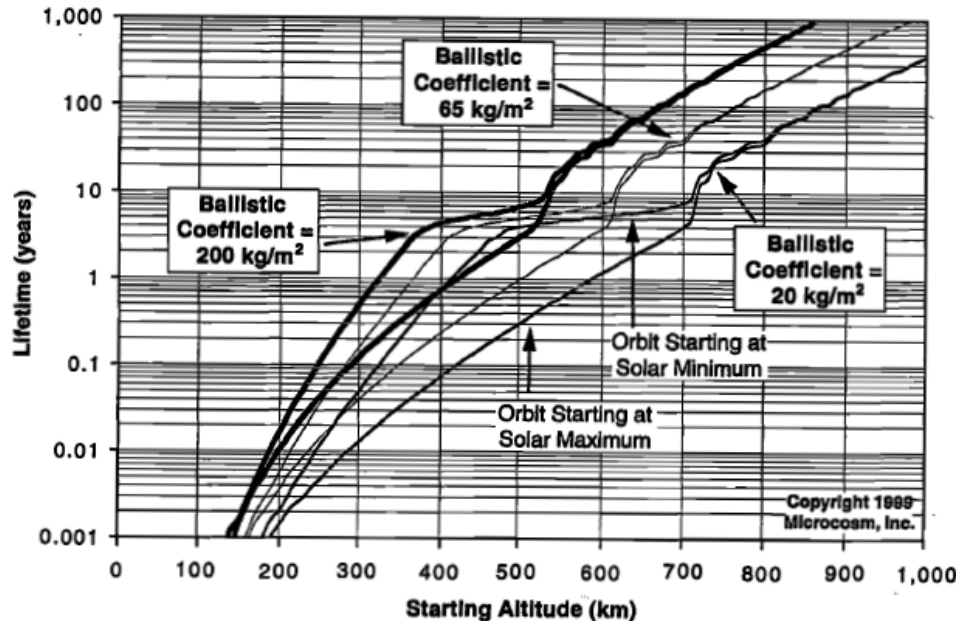
- 1) the orbit lifetime is less than 5 years [...]

[...]

6.2

Verification and validation requirements

- f) The orbit lifetime of a space object shall be assessed **probabilistically**, including at least the variability by moving the starting point through a **full solar cycle** [...]
- g) For the orbit lifetime assessment, [...] the **50th percentile** for orbit with eccentricity below 0,3 at end of life [...]



Larson & Wertz, SMAD, 2005

How to compute

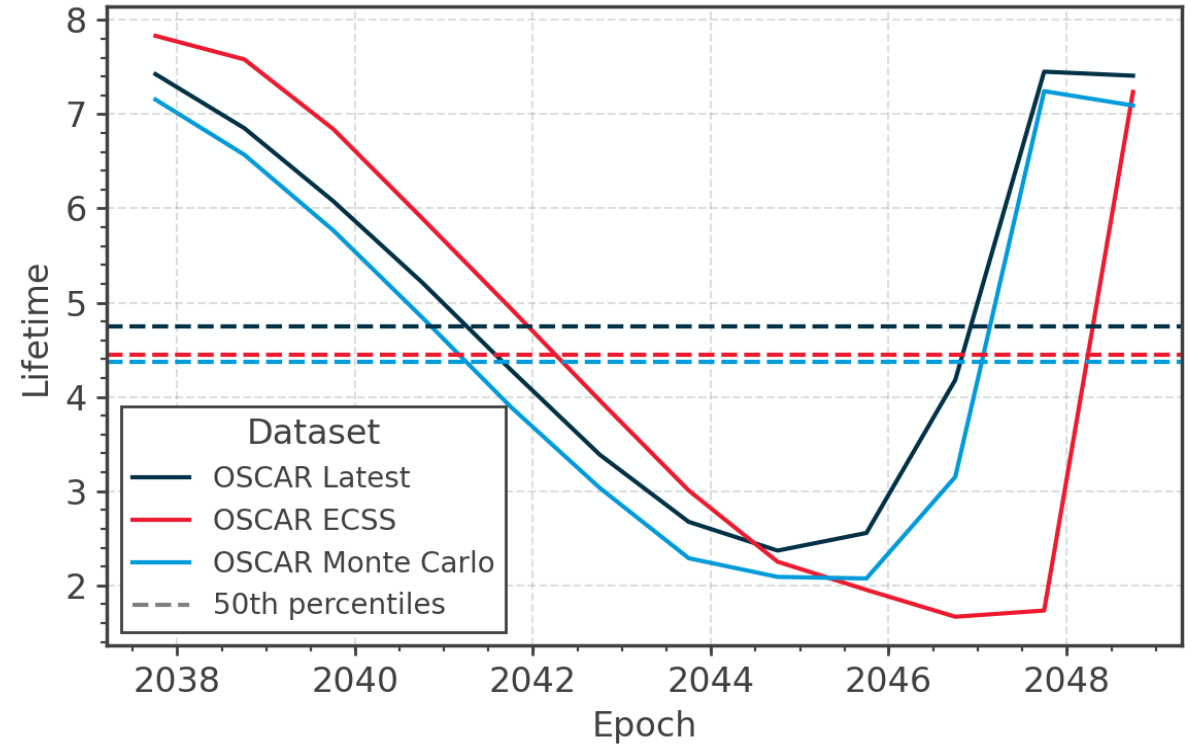
1. Select the end of operation epoch sampling from the solar cycle (yearly steps)
2. Consider additional uncertainties, if relevant (some guidelines in ESSB-HB-U-002)
3. Propagate the trajectory and obtain the distribution of orbital lifetimes
4. Compare the 50th-percentile to the 5-year limit
5. Use multiple solar activity models to increase confidence in the results

I am going to launch in YYYY and the lifetime is > 5 years

Example

Launch in 2039 for a mission without propulsion capabilities

What matters is the median of the distribution, so it is accepted that the predicted natural decay for the selected launch epoch is expected to be > 5 years



LEO clearance: collision probability criterion

novelty level



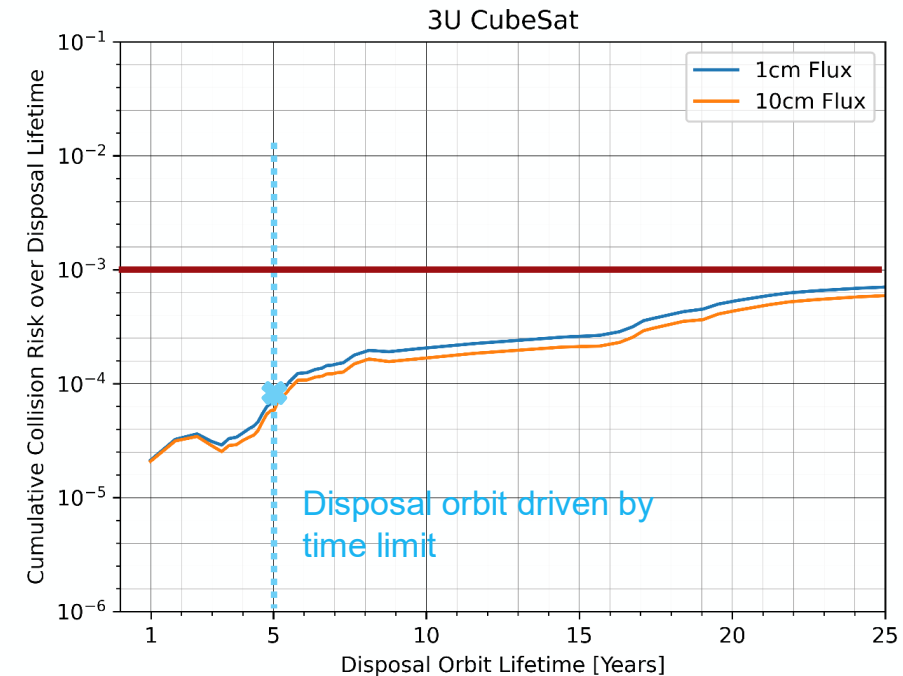
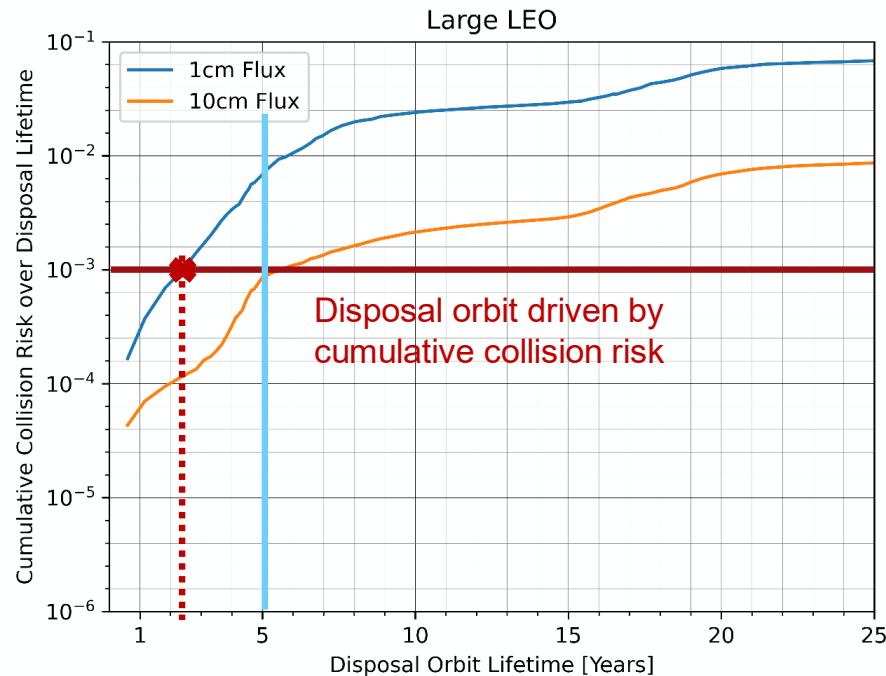
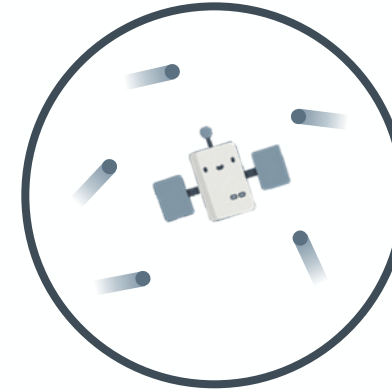
5.4.2.3.a

LEO protected region clearance

a. The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:

- 1) the orbit lifetime is less than 5 years [...]
- 2) the cumulative collision probability from its end of life until re-entry with space objects larger than 1 cm is below 10^{-3}

[...]



LEO clearance: collision probability criterion

novelty level

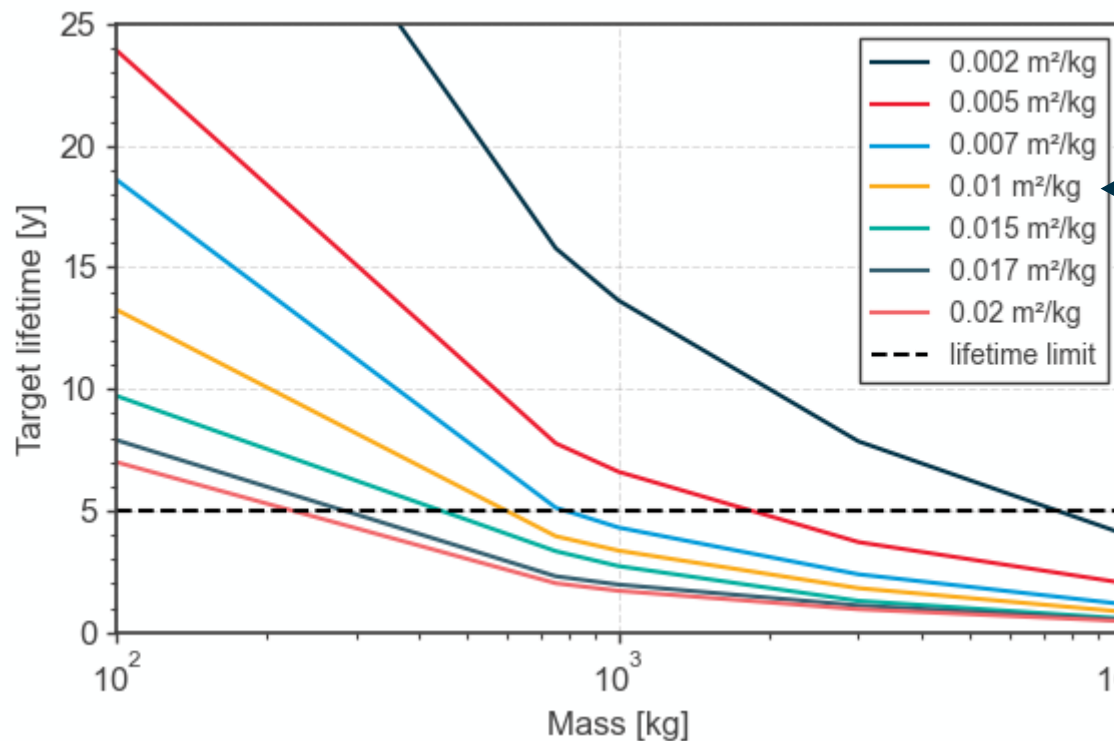
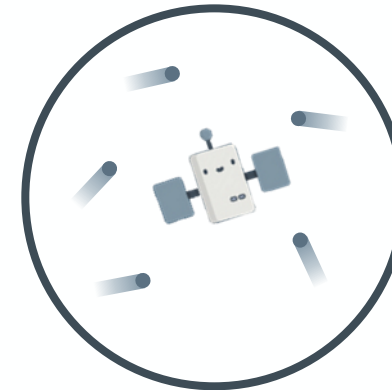


5.4.2.3.a

LEO protected region clearance

- a. The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:
- 1) the orbit lifetime is less than 5 years [...]
 - 2) the cumulative collision probability from its end of life until re-entry with space objects larger than 1 cm is below 10^{-3}

[...]



Example

Mean value for active satellites (non-constellation)

Threshold reached at ~ 600 kg

Much smaller satellites (e.g. CubeSats) can refer to the handbook and do not need to perform a specific analysis

HANDBOOK



LEO clearance: collision probability criterion

novelty level

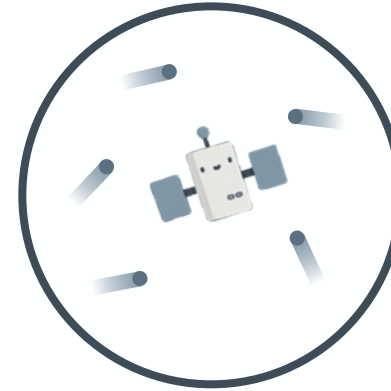


5.4.2.3.a

LEO protected region clearance

- a. The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:
- 1) the orbit lifetime is less than 5 years [...]
 - 2) the cumulative collision probability from its end of life until re-entry with space objects larger than 1 cm is below 10^{-3}

[...]



Included also in 
ECSS-U-AS-10C Rev.2 (2024)

How to compute

1. Use **space debris population** only, with objects ≥ 1 cm
2. Use **calibrated** population (no prediction) (e.g. from ESA's MASTER)
3. Include **solar panels** (i.e. everything for which it is not demonstrated that an impact with a 1 cm object does not result in debris generation) and exclude appendages for which debris generation is not expected (e.g. wire antenna, foils)
4. Compute on a range of epochs or select epoch such that the decay duration is the closest to the **median** computed in the lifetime assessment



Environment conditions frozen at the **Space Debris Mitigation Plan Approval** (usually SRR)

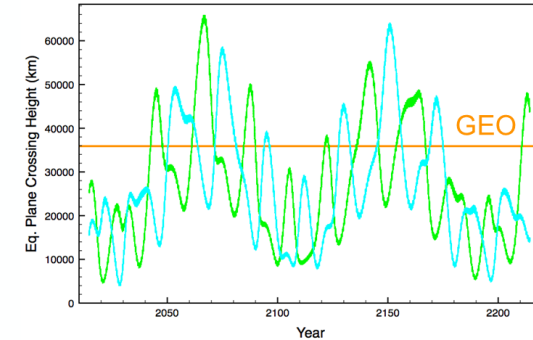


5.4.2.1.a

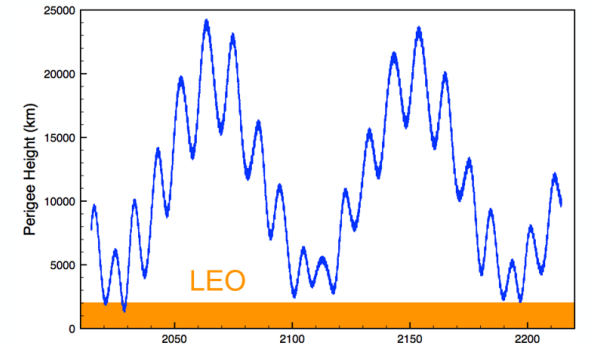
General Earth orbit clearance

The orbit clearance of a spacecraft or a launch vehicle orbital element in Earth orbit at its end of life shall be achieved by one of the following means, in order of preference:

1. Immediate Earth atmospheric re-entry after end of mission
2. Disposal in an orbit with a natural orbital decay that satisfies the orbit clearance requirements for the LEO protected region
3. If not operating in, nor crossing, the LEO protected region, disposal in a **graveyard orbit** that satisfies both following conditions:
 - a. Long-term perturbation forces **do not** cause it to **cross the protected regions** nor the **operational orbits of known constellations** that operate at a fixed operational altitude, within 100 years after its end of life
 - b. Its **cumulative collision probability** with space objects larger than 1 cm is below 10^{-3} for up to 100 years after the end of life



GEO and LEO crossings for the original INTEGRAL orbit (before manoeuvre in 2015)



5.4.2.3.b

LEO protected region clearance

[...]

The orbit clearance of a spacecraft or launch vehicle orbital element not operating in the LEO protected region, but **crossing the LEO protected region** after its end of life shall satisfy the following conditions:

1. the total orbit lifetime after end of life is less than 100 years
2. the cumulative collision probability from end of life until re-entry with space objects larger than 1 cm is below 10^{-3}
3. the orbit lifetime starting from the epoch of first intersection with the LEO protected region is less than 25 years

[...]

General Earth orbit clearance – example: MEO

5.4.2.1.a

General Earth orbit clearance

The orbit clearance of a spacecraft or a launch vehicle orbital element in Earth orbit at its end of life shall be achieved by one of the following means, in order of preference:

1. Immediate Earth atmospheric re-entry after end of mission
2. Disposal in an orbit with a natural orbital decay that satisfies the orbit clearance requirements for the LEO protected region
3. If not operating in, nor crossing, the LEO protected region, disposal in a **graveyard orbit** that satisfies both following conditions:
 - a. Long-term perturbation forces **do not** cause it to **cross the protected regions** nor the **operational orbits of known constellations** that operate at a fixed operational altitude, within 100 years after its end of life
 - b. Its **cumulative collision probability** with space objects larger than 1 cm is below 10^{-3} for up to 100 years after the end of life

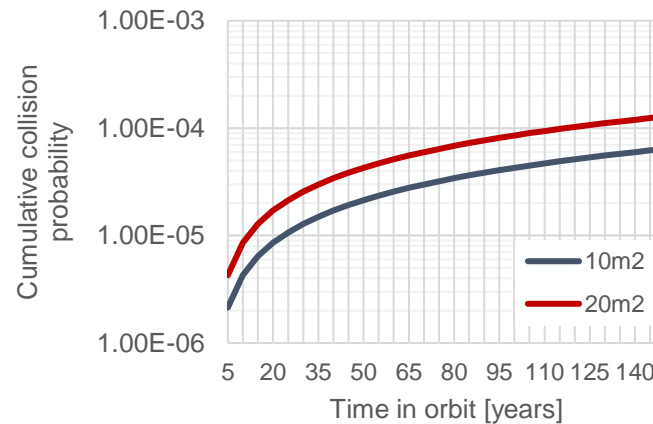
Data for the analysis in (a) available through DISCOSweb

<https://discosweb.esoc.esa.int/constellations>

Constellation ID	Designation ID	No. Obj	No. Planes	Oper SMA (km)	Oper INC (deg)	Oper ECC	Oper Lifetime	Deploy Start	Operation Start	Operation End	Sr
11	Astrosat	25	3	6899	97.5						3
32	Beidou-MEO	27	3	27878	55.3						1
17	BlackSky-i42	30	3	6878	42						2
250	BlackSky-i53	30	3	6878	53						2
12	Capella-Space	30	10	6096	45						1
33	Galileo	30	3	29599.8	56						2
3	Globalstar-G1	48	8	7800	52						4
4	Globalstar-G2	24	8	7800	52						5
31	GLONASS	24	3	25508	64.8						2
5	Gonets	12	6	7790	82.58						3
30	GPS	24	6	26558	55						1
16	Hawkeye-i41	30	5	6928	40.5						3
23	Hawkeye-i98	24	4	6878	97.6						3
259	ICEYE-X	30	3	6941	97.7						3
6	Iridium-NEXT	66	6	7158	86.4						9
22	Jilin-1	300	30	6918	97.5						6
18	KLEOS	80	4	6903	97.5						4
21	NuSat	200	2	6848	97.3	0.0001	10 years	20/06/2016	1/1/2020	1/1/2030	4
260	Orb	70	1	14371	0.841	0.0186	10 years	6/25/2013	6/25/2013	1/1/2300	3
7	OneWeb	648	12	7578	87.9	0.0001	10 years	2/27/2019	6/1/2023	1/1/2300	31

(b) condition not expected to be the driving one

Example of cumulative collision probability assessment in a Galileo-like orbit for two values of cross-sectional area (MASTER reference population)



Orbital clearance: how to


Tools available:
e.g. ESA's DRAMA already distributed with a **python wrapper** to facilitate the execution of probabilistic assessments

Intention to make available some basic scripts while the analysis is not available in the DRAMA GUI

DRAMA

Home Downloads FAQ Known Issues Development Team

The aim of the DRAMA tool suite as a whole is to enable space programs to assess their compliance with international requirements (e.g. ISO-24113) related to space debris, providing current mitigation measures that represent best practice. This suite accompanies ESA's Space Debris Mitigation Guidelines Handbook, which provides the necessary support and processes for the verification of these requirements. The DRAMA tool suite supports this aim by providing a software model that enables an assessment of mitigation strategies for the operational and disposal phases of a mission, including the debris risk posed to the mission and the effectiveness of an end-of-life strategy.



The current version of DRAMA is: 3.1.0

Each of the software tools has been designed to provide a fast, well-founded assessment of a user-defined mission and provides a response to international requirements related to space debris.

These five tools are:

pyDRAMA

Welcome to the documentation of DRAMA's python package!

Welcome to the documentation of DRAMA's python package!

DRAMA (Debris Risk Assessment and Mitigation Analysis) is a comprehensive tool for the compliance analysis of a space mission with space debris mitigation standards. For a given space mission, DRAMA allows analysis of:

- Debris and meteoroid impact flux levels (at user-defined size regimes)
- Collision avoidance manoeuvre frequencies for a given spacecraft and a project-specific accepted risk level
- Re-orbit and de-orbit fuel requirements for a given initial orbit and disposal scenario
- Geometric cross-section computations
- Re-entry survival predictions for a given object of user-defined components
- The associated risk on ground for at the resulting impact ground swath

This library serves as an interface to the DRAMA modules from python. It further extends the functionality of DRAMA by adding support for parametric and stochastic analyses.

Program Files (x86) > DRAMA-3.1.0 > TOOLS

- ARES
- CROC
- CSTATE
- MIDAS
- OSCAR
- python_package**
- SARA
- components_database.xml
- material_database.xml
- propulsion_database.dat
- subsystems_database.xml

Tools

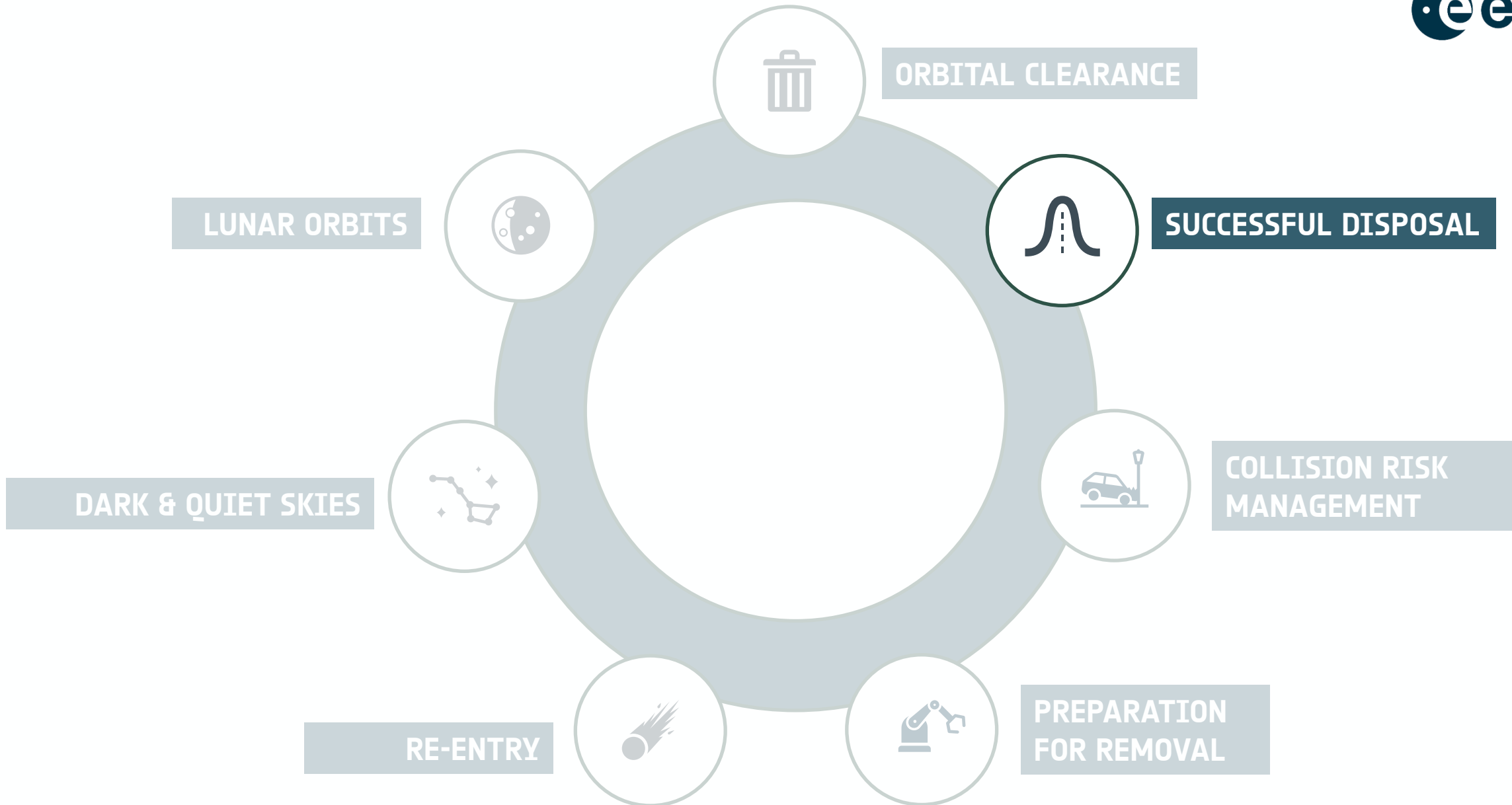


<https://sdup.esoc.esa.int/drama/>

Scripts



<https://debris-forum.sdo.esoc.esa.int/> 38



Probability of successful disposal

novelty level



5.4.1.1.a



The overall probability of successful disposal of a spacecraft or launch vehicle orbital stage in Earth orbit shall be kept above **0,9** through to end of life, including the contributions from system reliability **and** from collisions with space debris or meteoroids preventing the successful disposal.



Probability of successful disposal

novelty level



5.4.1.1.a

The overall probability of successful disposal of a spacecraft or launch vehicle orbital stage in Earth orbit shall be kept above **0,9** through to end of life, including the contributions from system reliability **and** from collisions with space debris or meteoroids preventing the successful disposal.

5.3.2.2.a

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall include **passivation capabilities**.

5.3.2.2.c

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall be designed to guarantee a probability of **successful passivation** through to the end of life of:

- 1) At least 0,90
- 2) At least 0,95, when operating in the LEO protected region in an orbit with a natural orbital decay duration longer than 25 years



What's new
Passivation capabilities now required also for spacecraft performing controlled re-entry

Passivation success rate with an explicit figure



How to handle the case of controlled re-entry?

We are not asking to demonstrate 90% probability of successful passivation in the contingency case.

Demonstrate that the 90% is achievable in the nominal case e.g. if the spacecraft has a nominal lifetime of 10 years, it should be verified that the components that would be used for passivation have a reliability compatible with the 90% value after 10 years

5.3.2.2.a

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall include **passivation capabilities**.

5.3.2.2.b

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall be **passivated** before the end of life **unless a successful controlled re-entry** is performed.

5.3.2.2.c

A spacecraft or launch vehicle orbital stage operating in Earth orbit shall be designed to guarantee a probability of **successful passivation** through to the end of life of:

- 1) At least 0,90
- 2) At least 0,95, when operating in the LEO protected region in an orbit with a natural orbital decay duration longer than 25 years

Probability of successful disposal

novelty level



Calculation methodology (reliability contribution):

- Identify all the equipment in charge of the disposal functional chain
→ **list of components**
- Identify all the equipment whose failure could prevent the successful disposal (through failure propagation, for instance)
→ **list of components**
- Build the Reliability Block Diagram (RBD)
→ **functional logic** (series / parallel configuration)
- Define the applicable **timeline** for the disposal probability
- Use the failure rate data for the different equipment to compute the disposal probability.

↓ **How to obtain it?** (in order of preference)

1. Manufacturers' data
2. Physics of failures (FIDES, etc.) ----- Training by ESA RAMS experts can be organised
3. Reliability data handbooks
4. In-flight data (only applicable if the number of data is sufficient) ----- Important for developers & operators to collect data on behaviour in orbit
5. Similarity (scaled-down to the mission)



Probability of successful disposal

novelty level



5.4.1.1.a



The overall probability of successful disposal of a spacecraft or launch vehicle orbital stage in Earth orbit shall be kept above **0,9** through to end of life, including the contributions from system reliability **and** from collisions with space debris or meteoroids preventing the successful disposal.



Starting point for the analysis:
Guideline on Small Debris Risk Assessment (MIDAS)



Probability of successful disposal

novelty level



5.4.1.1.a



The overall probability of successful disposal of a spacecraft or launch vehicle orbital stage in Earth orbit shall be kept above **0,9** through to end of life, including the contributions from system reliability **and** from **collisions with space debris or meteoroids** preventing the successful disposal.

HANDBOOK

1. Identify relevant mission **phase**, **trajectory** conditions, and **pointing** scenario
2. Define the **space system design**
3. Identify **critical components** for the disposal implementation
4. Identify **ballistic limit equation** and **failure model** (e.g. perforation) for the critical components
5. Determine the **surface at risk** for each critical component
6. Determine the expected number of collisions causing failure per component
7. Determine the system level **Probability of No Failure**



Included also in
ECSS-U-AS-10C Rev.2 (2024)

Starting point for the analysis:
**Guideline on Small Debris
Risk Assessment (MIDAS)**



Probability of successful disposal

novelty level



5.4.1.1.a



The overall probability of successful disposal of a spacecraft or launch vehicle orbital stage in Earth orbit shall be kept above **0,9** through to end of life, including the contributions from system reliability **and** from collisions with space debris or meteoroids preventing the successful disposal.



Early phases (0-A)

Conservative assessment based on impact rate with 1 cm objects

Indication of the allocation for reliability aspects



Definition phases (B-C)

Assessment with simplified models (e.g. with DRAMA/MIDAS, but also other tools available) that consider the selected shielding and component placement



Later phases (C onwards)

If needed, assessment with refined 3D models (e.g. ESABASE2)
+ updates when a re-estimation of the disposal probability is requested

Example
if the probability of impacts with 1 cm objects over the operational lifetime is 2% (typical value for medium/large satellite in SSO) and the probability of successful disposal requirement is 90%, then the minimum reliability of the disposal items and functions needed for compliance is 91,84%

HANDBOOK

SSO: Sun Synchronous Orbits

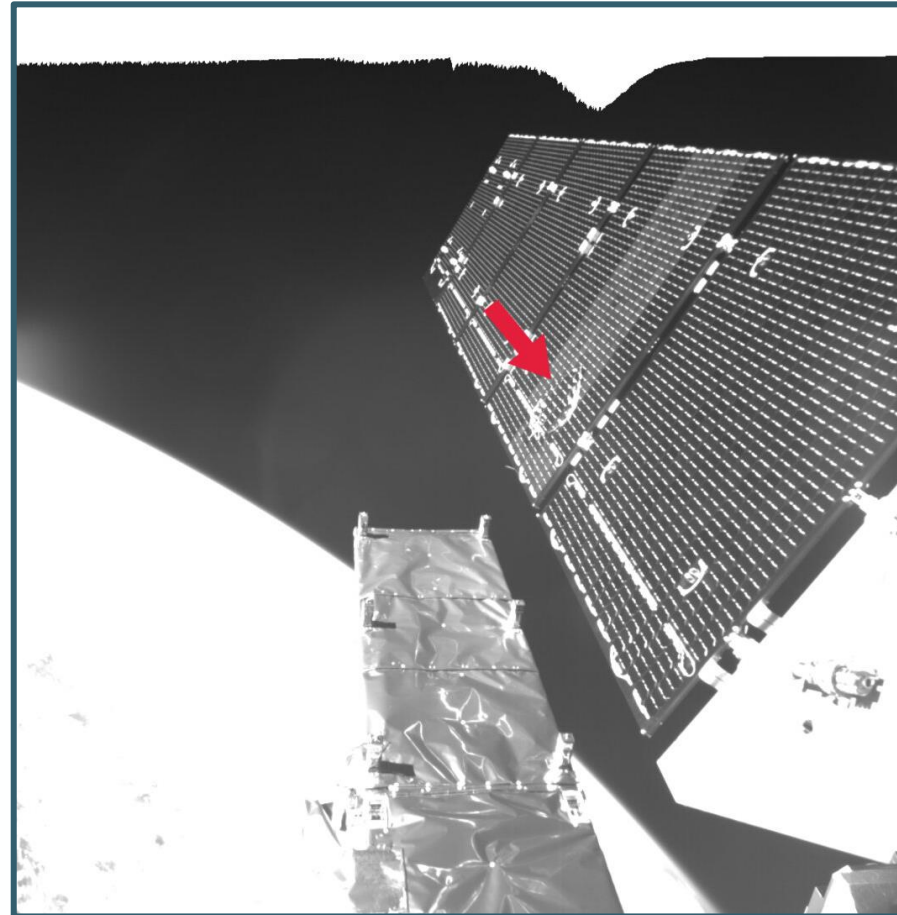


Vulnerability assessment

Damage assessment



H. Krag et al, Acta Astronautica, Vol. 137, 2017



Impact on Sentinel-1A's solar panel (2016)

Debris generation

DISCOSweb ▾ Home Data ▾ API Documentation

Objects

DISCOS ID	Name	SATNO	COSPAR ID ↓
	Sentinel-1A		
39631	Sentinel-1A	39634	2014-016A
41795	Sentinel-1A solar array debris	41798	2014-016B
41796	Sentinel-1A solar array debris	41799	2014-016C
41797	Sentinel-1A solar array debris	41800	2014-016D
41798	Sentinel-1A solar array debris	41801	2014-016E
41799	Sentinel-1A solar array debris	41802	2014-016F
41800	Sentinel-1A solar array debris	41803	2014-016G
41801	Sentinel-1A solar array debris	41804	2014-016H
52651	Sentinel-1A solar array debris	43417	2014-016J

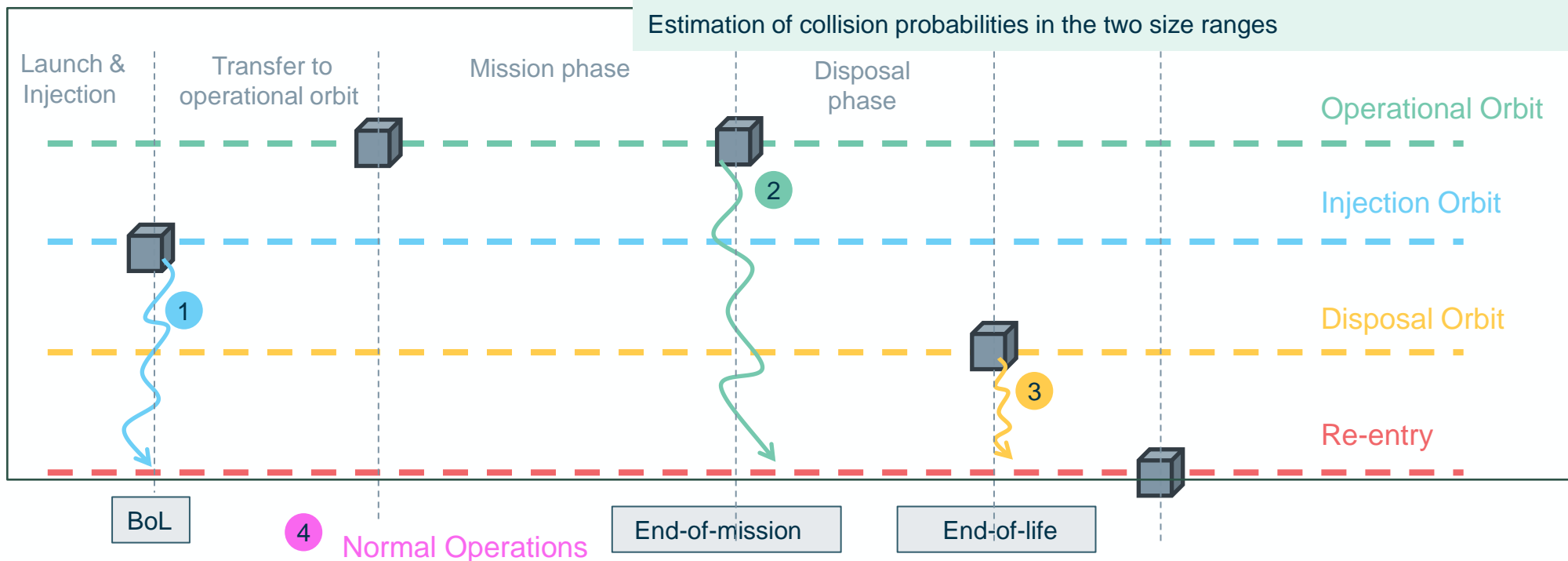
Vulnerability assessment

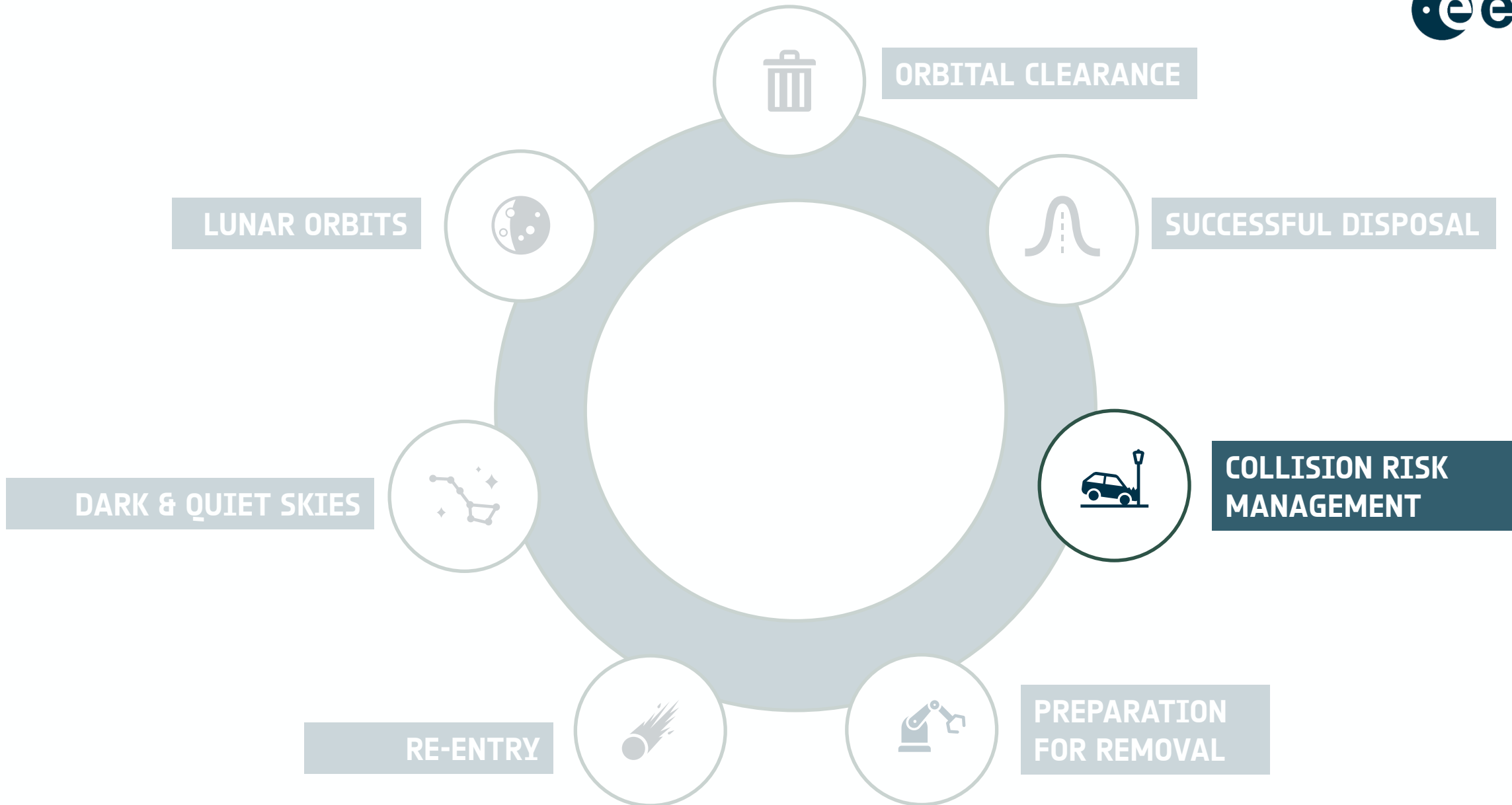


Collision risk assessment during design

The developer of a spacecraft or launch vehicle orbital element operating in Earth orbit shall quantify the probability that space debris or meteoroid impact causes the spacecraft or launch vehicle orbital element to break-up, including:

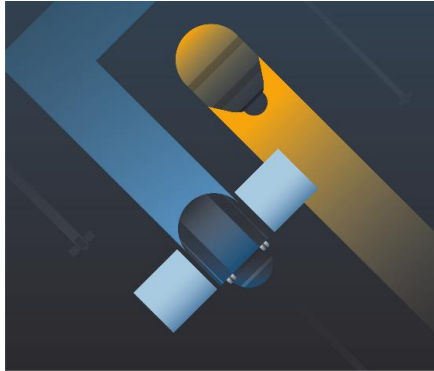
1. Impacts with space debris and meteoroids larger than 1 mm and smaller than 1 cm
2. Impacts with space debris and meteoroids larger than 1 cm
3. A free drift trajectory after orbit injection, end of mission, and disposal, and during normal operations, until re-entry or up to 100 years





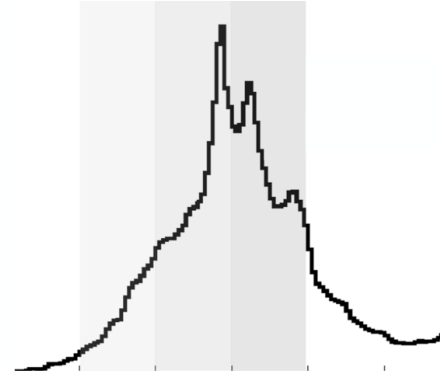
Not having manoeuvre capabilities does not mean that nothing can be done

Manoeuvre capabilities



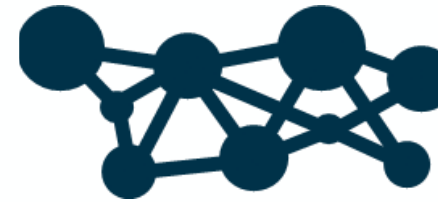
- Reaction threshold
- CAM size
- Timeliness of the reaction

Characterise risk



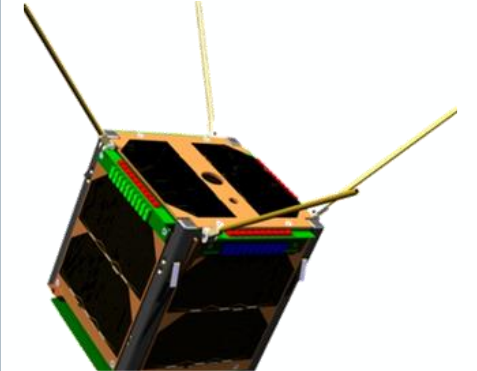
- Assess vulnerability to impacts
- Assess expected number of conjunctions

Ease interactions



- Procedure for contact
- Ephemerides available for distribution using standard formats

Ensure trackability



- Engage with SST data provider
- Facilitate identification

Image credits:
© LEDSAT team

Collision risk management

novelty level 



5.3.3.2.d

During the *design*, the developer of a spacecraft operating in near Earth orbit with a recurrent manoeuvre capability shall quantify the **operational impact** during normal operations due to conjunctions.

5.3.3.2.e

The developer of a spacecraft or launch vehicle orbital element injected into near Earth orbit shall quantify, during normal operations and after end of life until re-entry or up to 100 years:

- 1) The **expected number of conjunctions** at 10^{-4} and 10^{-6} collision probability threshold, and
- 2) The **estimated number of collision avoidance manoeuvres** triggered thereby on other spacecrafts

5.3.3.3.d

The operator of a spacecraft operating in near Earth orbit with a recurrent manoeuvre capability shall perform the assessment of:

- 1) The **resources allocation** for the acceptable collision probability for individual conjunctions and its impact on the mission *design* [...]



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How do we estimate the impact on other spacecrafts?

5.3.3.2.e

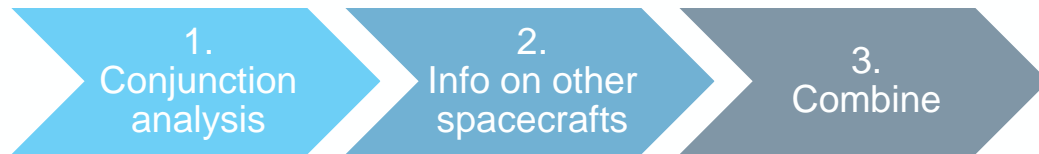
The developer of a spacecraft or launch vehicle orbital element injected into near Earth orbit shall quantify, during normal operations and after end of life until re-entry or up to 100 years:

- 1) The expected number of conjunctions at 10^{-4} and 10^{-6} collision probability threshold, and
- 2) **The estimated number of collision avoidance manoeuvres triggered thereby on other spacecrafts**

Options (not exclusive)

- 1: Use own data from **past operations**
- 2: Simulations

Minimal workflow:



Perform classical analysis with DRAMA/ARES to extract the number of expected conjunctions above a certain threshold

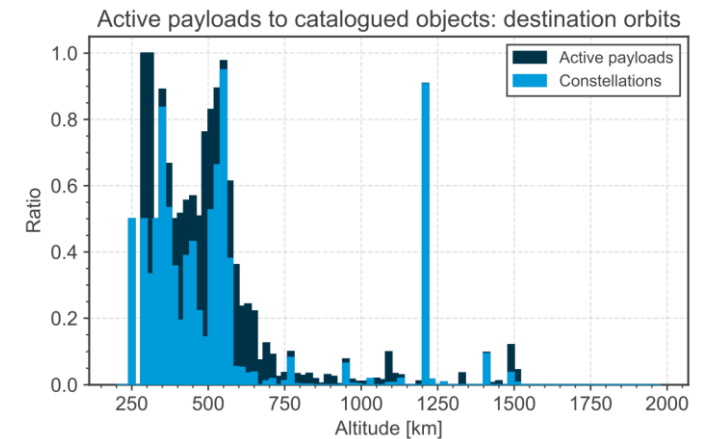
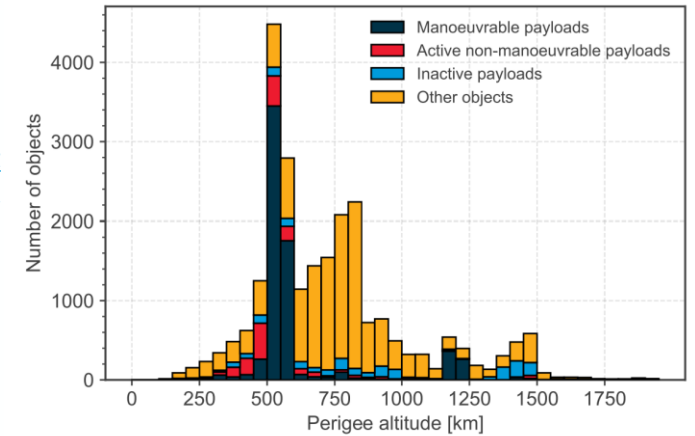
Retrieve the number/share of spacecraft vs total catalogued population

Use the share from the point 2 to scale the results obtained in 1.

2

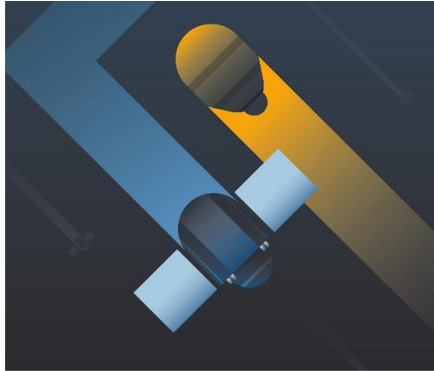
Information available from ESA's Space Environment Report

https://www.sdo.esoc.esa.int/environment_report/Space_Environment_Report_latest.pdf



5.3.3.2.c

Manoeuvre capabilities



- Reaction threshold
- CAM size
- Timeliness of the reaction

A spacecraft operating in near Earth orbit shall have a **recurrent manoeuvre capability** if it satisfies at least one of the following conditions:

- 1) It is operating in the **GEO** protected region
- 2) It is injected into an orbit **crossing** the **LEO** protected region with a natural orbit decay duration longer than **5 years**
- 3) Its **cumulative collision probability** with space objects larger than 1 cm is above **10^{-3}** through to its end of life
- 4) It is part of a **constellation**
- 5) It is performing **close proximity operations**, or **formation flying**

recurrent manoeuvre capability

capability of a spacecraft to perform repeatable manoeuvres on-orbit that can cause a change to the orbit over a limited amount of time

NOTE The repeatability of the manoeuvres implies that multiple manoeuvres of a targeted accuracy can be implemented by a spacecraft.

What about differential drag?

5.3.3.2.c

A spacecraft operating in near Earth orbit shall have a **recurrent manoeuvre capability** if it satisfies at least one of the following conditions:

- 1) It is operating in the **GEO** protected region
- 2) It is injected into an orbit **crossing** the **LEO** protected region with a natural orbit decay duration longer than **5 years**
- 3) Its **cumulative collision probability** with space objects larger than 1 cm is above 10^{-3} through to its end of life
- 4) It is part of a **constellation**
- 5) It is performing **close proximity operations**, or **formation flying**

recurrent manoeuvre capability

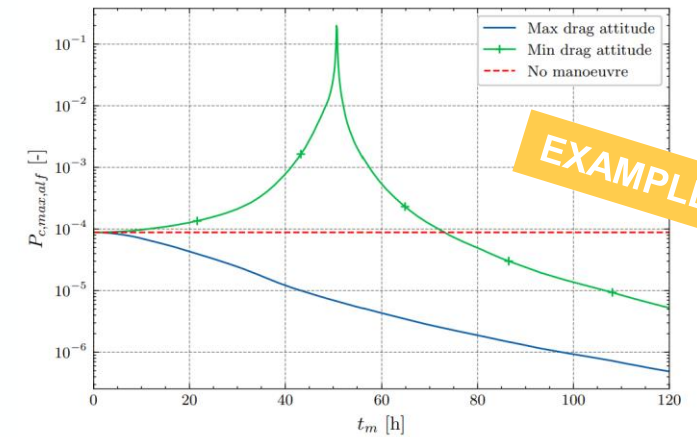
capability of a spacecraft to perform repeatable manoeuvres on-orbit that can cause a change to the orbit over a limited amount of time

NOTE The repeatability of the manoeuvres implies that multiple manoeuvres of a targeted accuracy can be implemented by a spacecraft.

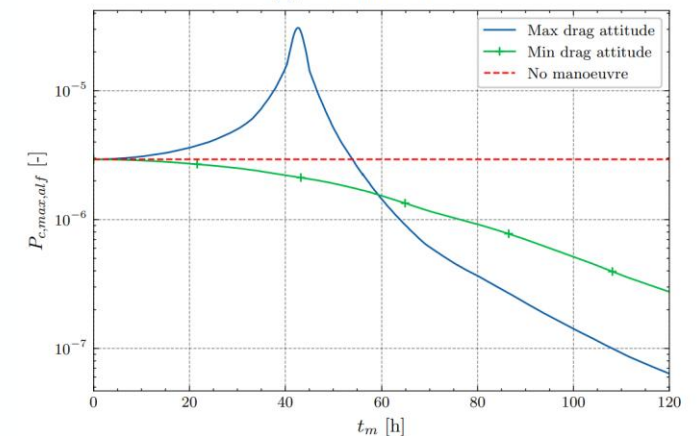
Differential drag is **not compatible** with the requirements.

Request to achieve a **specific risk reduction** in a **limited time**, which cannot be guaranteed in a **robust way** with differential drag

Examples from F. Turco et al, Acta Astronautica, 2023



(a) Encounter A.



(b) Encounter B.

Collision risk management during operations

novelty level



5.3.3.3.a

During normal operations of a spacecraft in near-Earth orbit with a recurrent manoeuvre capability, the acceptable collision probability threshold shall be below 10^{-4} per conjunction.

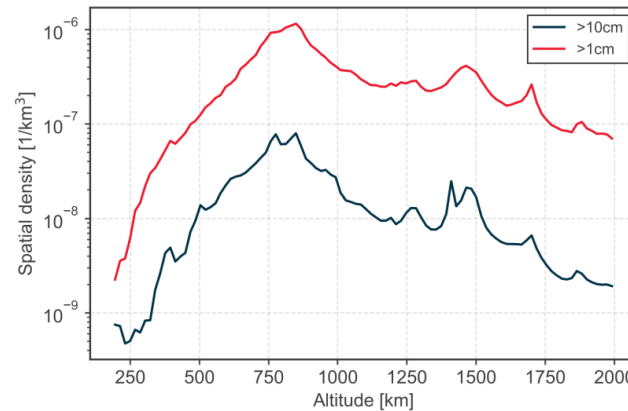
5.3.3.3.i

For a spacecraft operating in near Earth orbit with a recurrent manoeuvre capability, [...] the operator of the spacecraft shall perform collision avoidance manoeuvres to reduce the collision probability by at least **two orders of magnitude** below the threshold.

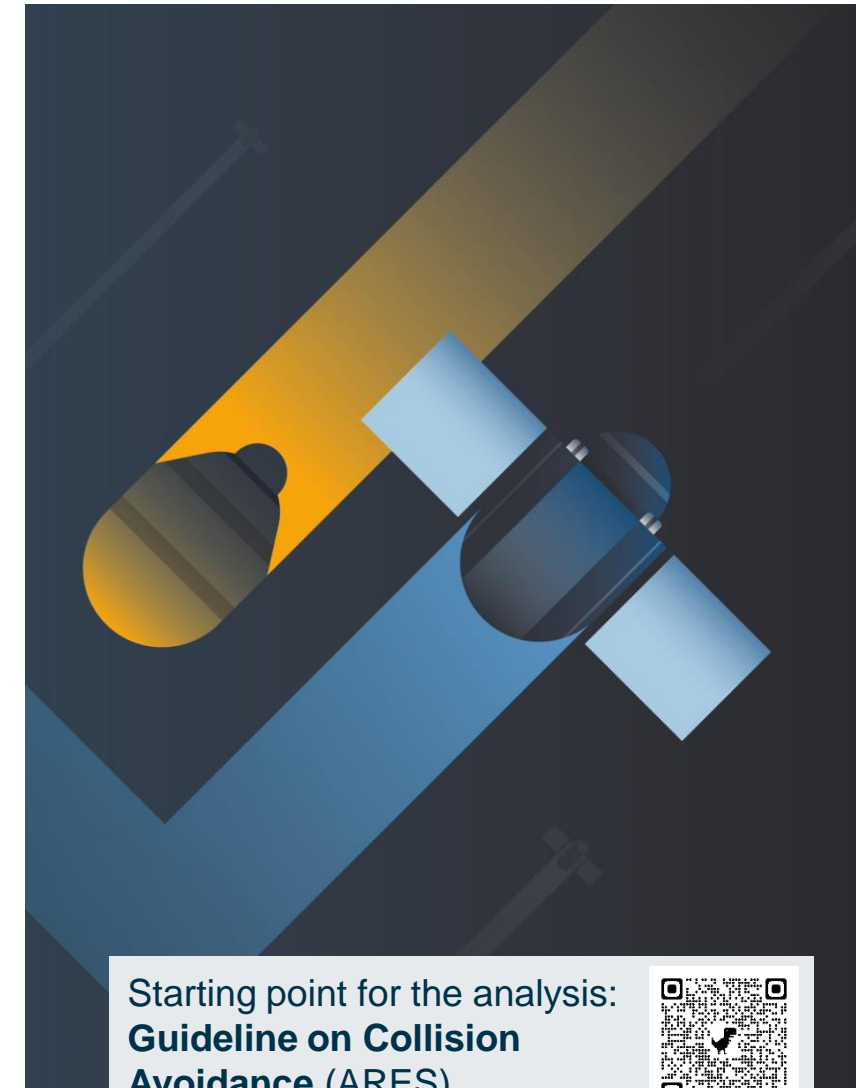
5.3.3.3.b

During the normal operations of a spacecraft in the LEO protected region with a recurrent manoeuvre capability, on an orbit with an average density of space debris larger than 1 cm above 10^{-7} km^{-3} , the acceptable collision probability threshold shall be the lower of the following values: 1) 10^{-4} , and 2) The collision probability value such to **reduce the annual collision probability** by at least **90%** with respect to not performing collision avoidance manoeuvres

These requirements are operational in nature, but have an impact on the **design** (including the **deltav budget**), so they shall be addressed already in early mission design phases



ESA's Space Environment Report



Starting point for the analysis:
Guideline on Collision Avoidance (ARES)



Why a CAM size in terms of risk reduction?

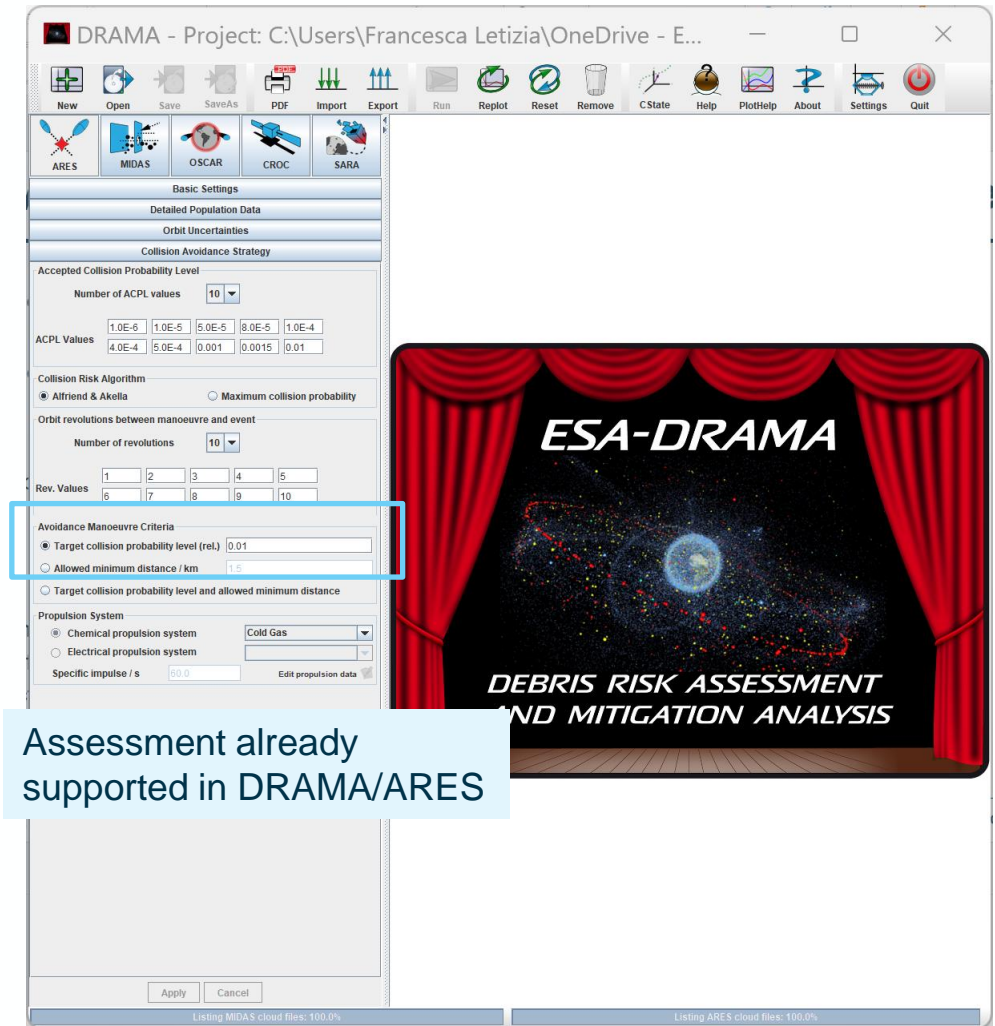
Objectives of a CAM:

- Reduce risk of the event to the background/accepted one
- Avoid that the event needs to be actioned again after the CAM

Collision probability targets better suited to achieve such objectives than separation distances

Example:

Past recommendation of 200m radial separation may not be suitable for low LEO missions (e.g. Aeolus) where the effect of drag is such that the position uncertainty on the chaser is larger



Collision risk management during operations

novelty level



5.3.3.3.g

The space and ground segments associated with spacecraft operating in near Earth orbits shall be designed to have **ephemerides** available for collision avoidance purposes in **less than 1 day** after orbital injection.

5.3.3.3.j

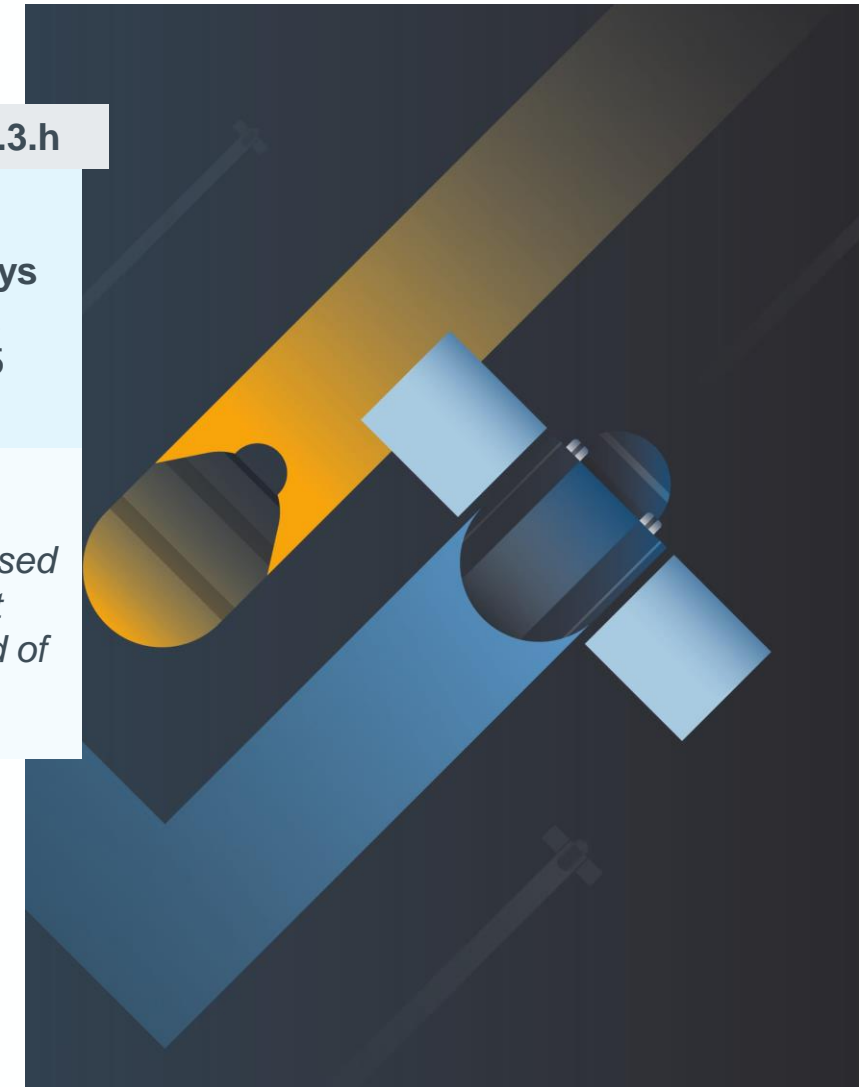
A spacecraft operating in near Earth orbit, after receiving a warning for a conjunction with a collision probability above the threshold during normal operations, shall perform a collision avoidance action, including:

- 1) **Manoeuvres**, if the warning is received up to **12 hours** before the conjunction and the spacecraft is operational
- 2) **Assessment** in less than **4 hours** after the warning
- 3) Actively communicating its status or ephemerides, if unable to perform manoeuvres

5.3.3.3.h

A spacecraft with a recurring manoeuvre capability shall be able to implement a collision avoidance manoeuvre within **2 days** when injected into a near Earth orbit with a natural orbital decay duration longer than 5 years.

It is understood that in case of rideshare launches with no manoeuvre periods imposed by the launcher this cannot happen. In that case, the time will be counted from the end of the no manoeuvre period



Are 24/7 operations required for compliance?

5.3.3.3.j

A spacecraft operating in near Earth orbit, after receiving a warning for a conjunction with a collision probability above the threshold during normal operations, shall perform a collision avoidance action, including:

- 1) **Manoeuvres**, if the warning is received up to **12 hours** before the conjunction and the spacecraft is operational
- 2) **Assessment** in less than **4 hours** after the warning
- 3) Actively communicating its status or ephemerides, if unable to perform manoeuvres

Ephemerides exchange described in 5.3.3.3.m

No, they are not required

- **Assessment** can be performed through the (automatic) processing of a CDM
- In case of **manoeuvres**,
 - The **space segment** shall be able to implement the required separation (to achieve the 2 orders of magnitude reduction of the collision probability) in less than 12 hours (relevant for very low thrust missions)
 - The **ground segment** should target operations with 12 hours coverage/day (this defines the time when warning can be acted on) – aspects such as platform limitations, passes availability, etc. can be discounted for the assessment

Space surveillance and tracking

novelty level



5.3.3.5.a

The developer of a spacecraft or launch vehicle orbital element injected into Earth orbit shall guarantee that it can be **tracked** by a space surveillance segment supporting collision avoidance processes.

5.3.3.5.c

During normal operations, the operator of a spacecraft in Earth orbit shall **quantify the position and velocity accuracy of the combined ground, space, and space surveillance segment** [...]

5.3.3.5.e

The developer and operator of a spacecraft or launch vehicle orbital element injected into Earth orbit shall guarantee that it can be **unambiguously identified** by a space surveillance segment within **1 day after on-orbit injection**.

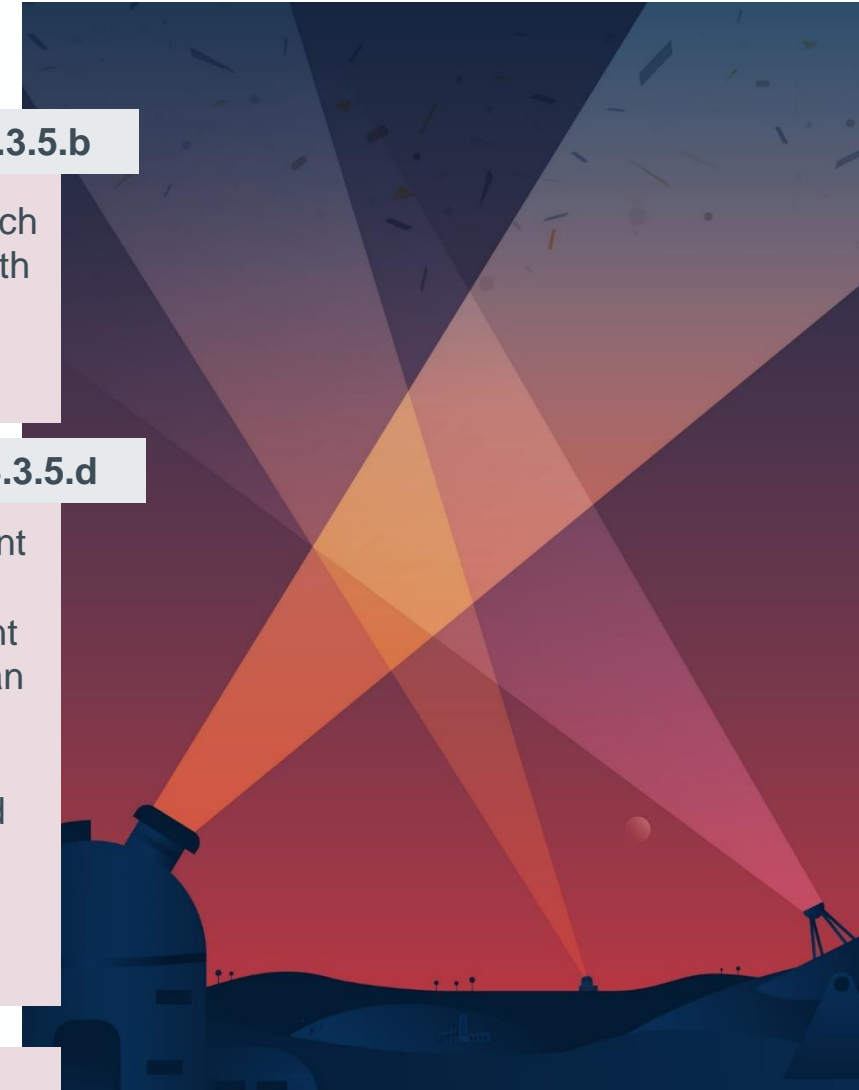
5.3.3.5.b

The ground segment of a spacecraft or launch vehicle orbital stage injected into a near Earth orbit shall include a **space surveillance segment**.

5.3.3.5.d

A spacecraft or launch vehicle orbital element injected into the protected regions shall guarantee that a space surveillance segment supporting collision avoidance processes can achieve a **position accuracy** during normal operations as well as after end of life higher than **100 m** in the **LEO** protected region and higher than **1000 m** in the **GEO** protected region along the orbit determination interval outside of manoeuvre periods.

...



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Need to demonstrate that we are identified in 1 day?

5.3.3.5.e

The developer and operator of a spacecraft or launch vehicle orbital element injected into Earth orbit shall guarantee that it can be **unambiguously identified** by a space surveillance segment within **1 day after on-orbit injection**.

Example: cubesat on a rideshare launch



No, as the actual identification will depend also on the Space Surveillance Segment's processes. Here we are asking about the **capability** i.e. enable a fast identification

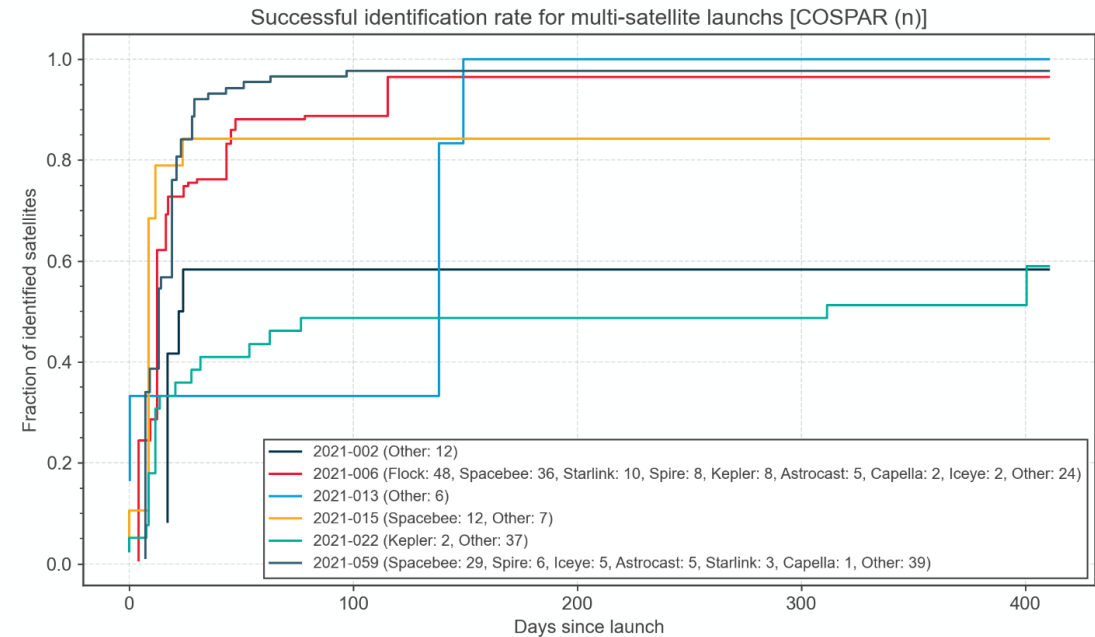
- **Collaborate** with the space surveillance segment and share **predicted launch trajectory** and early operations and manoeuvring **plans**.
- **Inform** surveillance segment early about possible **mislabelling** in the catalogue (e.g. using the TLE).
- Review **launch sequence**, in case of rideshare, to avoid uncoordinated release of spacecraft and cause mislabelling in the catalogue.
- Identify **ground segment capabilities** to share early orbital information derived from telemetry and on-board GNSS data.

TLE: Two-Line elements

Ensure trackability

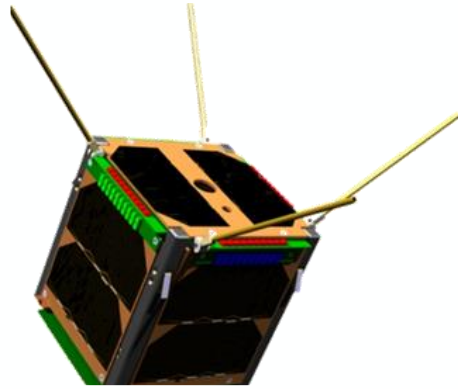
CubeSat Confusion: small satellites, with similar shape, released simultaneously and with lower reliability rates than traditional missions

Delay in identification can result in mission failure and interference with other operators



M. Skinner, CubeSat Confusion: Technical and Regulatory Considerations, 2021 ([Available online](#))

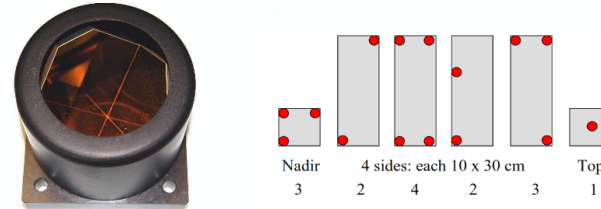
Available technologies



LED

<https://www.s5lab.space/index.php/ledsat-home/>

Passive laser retro-reflector



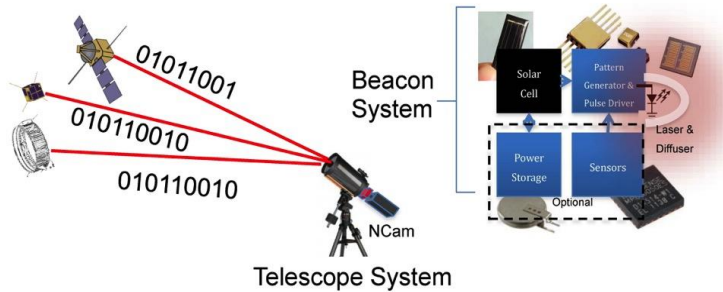
https://www.thorlabs.com/navigation.cfm?guide_id=2539

More information available from NASA, State-of-the-Art of Small Spacecraft Technology



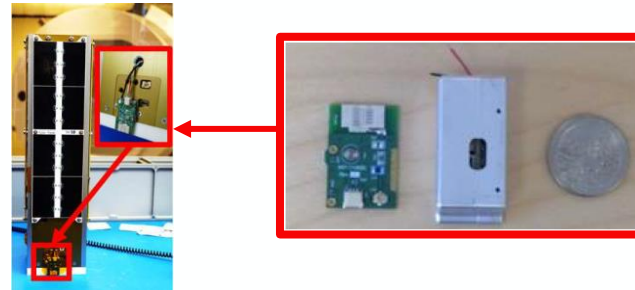
➔ <https://www.nasa.gov/smallsat-institute/sst-soa/identification-and-tracking-systems/>

Modulated laser

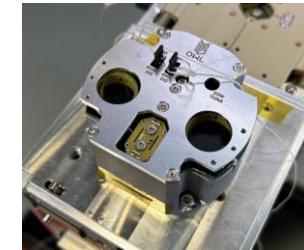


ELROI: A License Plate for Your Satellite
https://amotech.com/TechnicalPapers/2018/Poster/Holmes_Rebecca.pdf

Space transponder



SRI International's CubeSat Identification Tag (CUBIT): System Architecture and Test Results from Two On-Orbit Demonstrations
<https://digitalcommons.usu.edu/cgi/viewcontent.cgi?article=4451&oncontext=smallsat>



Plug and play device equipped with a battery, GNSS tracker, omnidirectional antenna
<https://owl.c3s.space/>

Space surveillance and tracking

novelty level



Providers of SST data for free exist



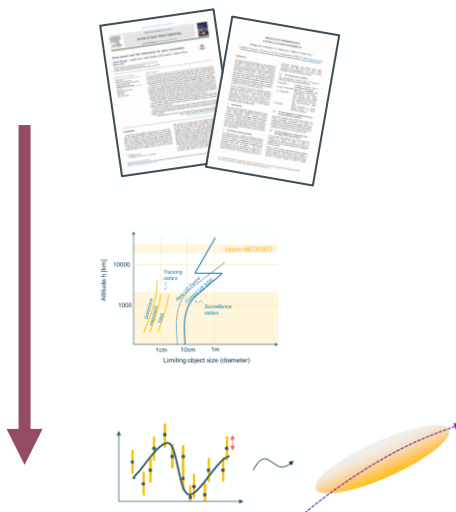
Valuable to register even w/o manoeuvre capabilities



Immediately compliant with many requirements (e.g. probabilistic assessment, daily screening, ...)



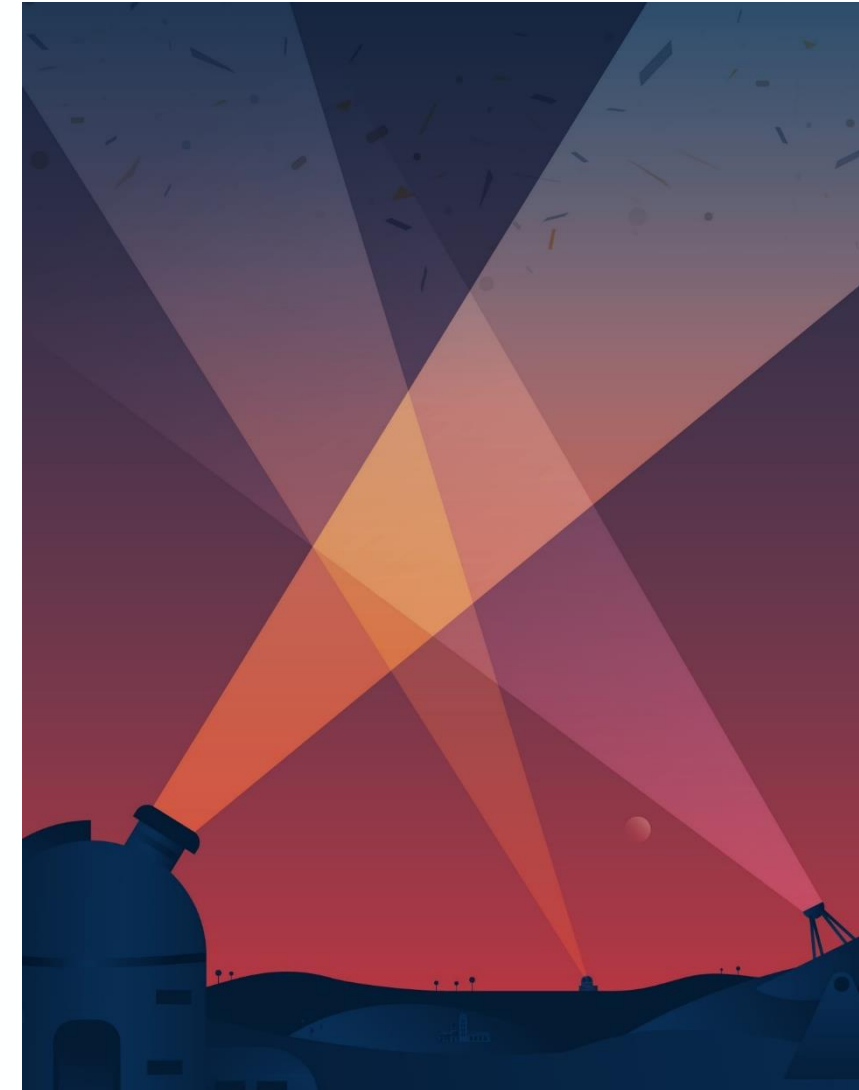
Trackability performance can be assessed with different levels of detail



Declared performance, analysis in public literature, past operational experience
e.g. single values, look-up tables

Trackability curve
included in the updated Handbook

Own simulations
upcoming DRAMA functionality in January 2025



Space surveillance and tracking

novelty level



Providers of SST data for free exist



Valuable to register even w/o manoeuvre capabilities



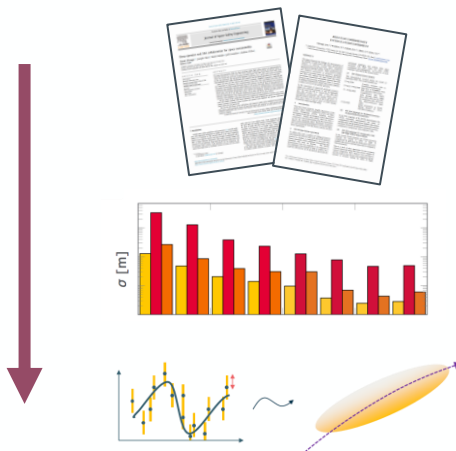
Immediately compliant with many requirements (e.g. probabilistic assessment, daily screening, ...)



Trackability performance can be assessed with different levels of detail



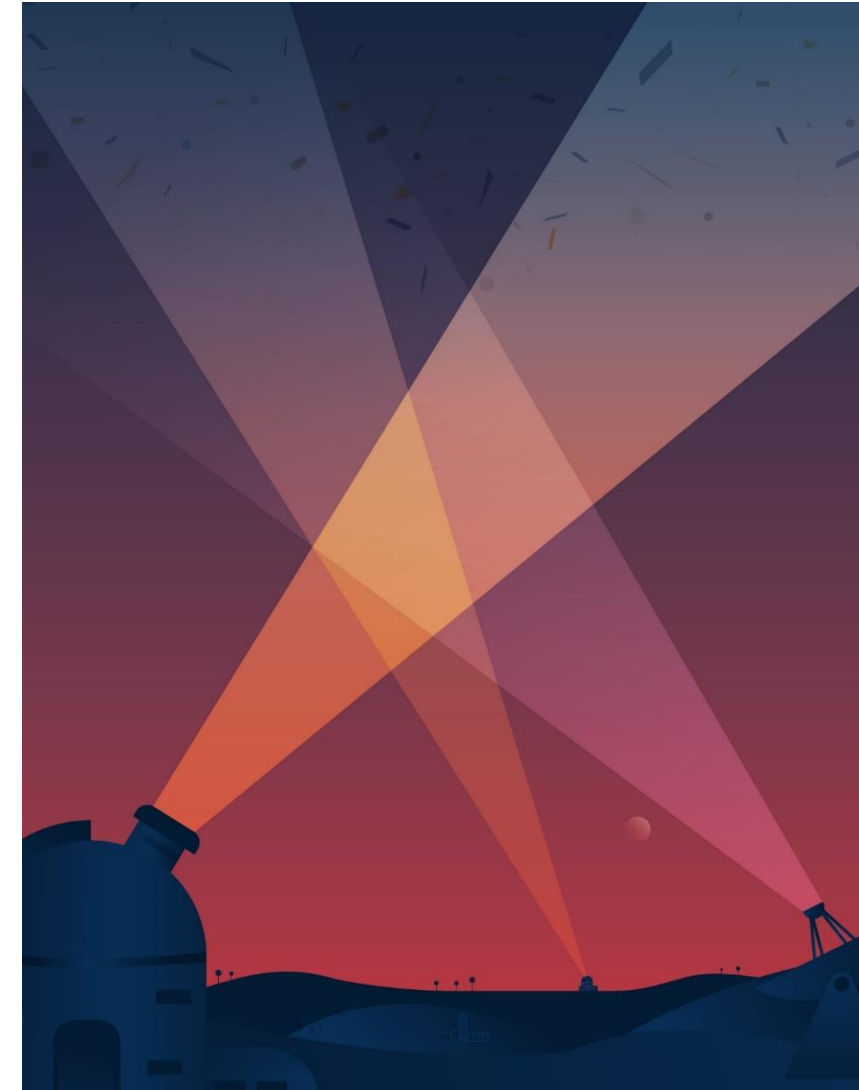
Accuracy performance can be assessed with different levels of detail



Declared performance, analysis in public literature, past operational experience
e.g. single values, look-up tables

ESA's assessment
e.g. based on historical CDMs

Own simulations
upcoming DRAMA functionality in January 2025



Close-proximity operations

novelty level



5.3.3.4.a

The probability of **unintentional contact** during CPO or formation flying in Earth orbit must remain below 10^{-4}

This is the core requirement, serving as the **foundation** for all subsequent requirements, which explains the conditions for its verification

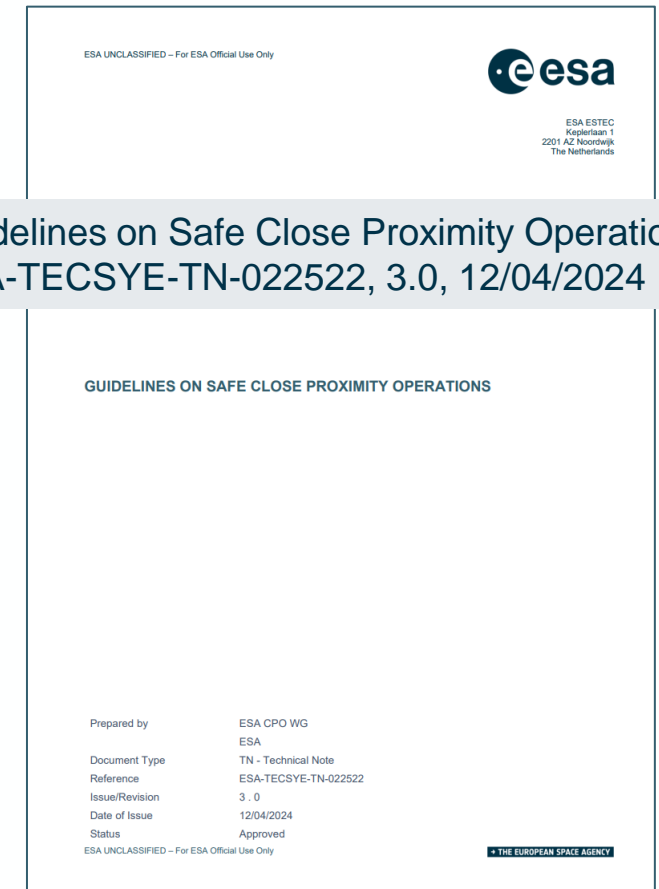
5.3.3.4.b: Quantification of the probability

Verification methodology to assess the probability:

- **CONOPS** detailing decision gates & phase definition
- **RAMS** analysis of all functional chains and units involved accounting for performance uncertainties and environmental perturbations
- Simulation of the nominal/reference **trajectories**

5.3.3.4.c - 5.3.3.4.f: Additional requirements on health monitoring, redundancy, contingency operations, safe trajectories and collision avoidance measures.

Guidelines on Safe Close Proximity Operations, ESA-TECSYE-TN-022522, 3.0, 12/04/2024



CONOPS: CONcept of OPerationS | RAMS: Reliability, Availability, Maintainability, Safety



Close-proximity operations



Early phases (0-A)

Initial collision risk assessment.
Safe trajectory design.



Later phases (B-C)

Detailed design and verification of on-board systems for health monitoring and autonomous collision avoidance
Analysis of RAMS data, integration of redundant systems, and review of failure scenarios.



After production (D onwards)

Real-time collision probability monitoring.
Re-assessment during mission extensions or anomalies.

How close is enough to be considered CPO?

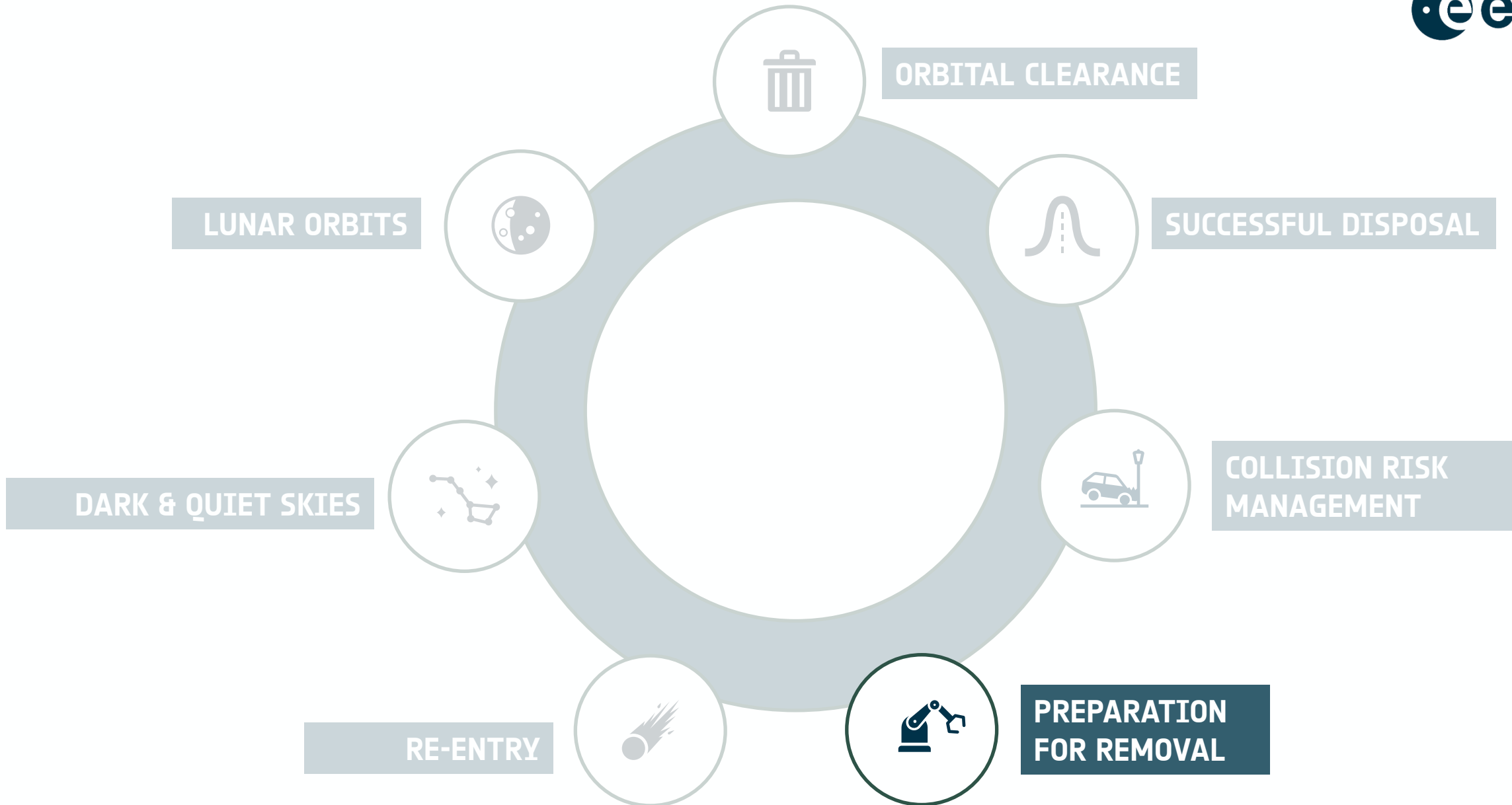
Any mission where the spacecrafts are maintaining a **relative distance** is considered to fall under the category of close proximity operation and formation flying

It is understood that the verification methodology may be significantly different between cases such as

- Active Debris Removal/In-orbit servicing mission
- Satellites with km of separation

For the latter, it can be enough to demonstrate that the time to reach a potential risky conjunction (e.g. after an erroneous manoeuvre) is enough for the ground to react as in the case of collision avoidance manoeuvres with other debris object





Preparation for removal



GEO: always requested

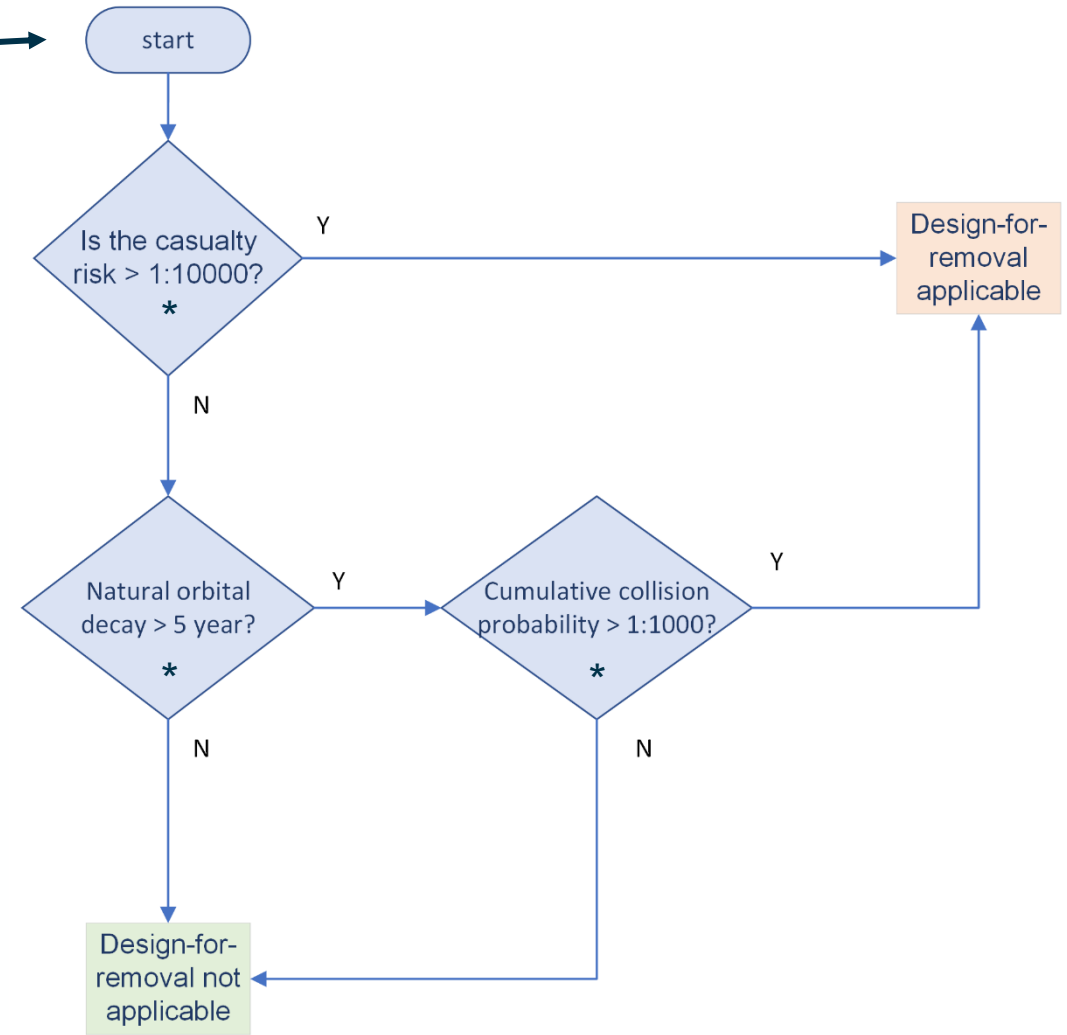
LEO: requested for high-risk objects

The requirements cover several aspects related to Design-for-Removal (D4R)

- Mechanical **interfaces**
- Support to passive **navigation**
- Assessment of long-term **attitude**
- Attitude reconstruction from ground
- Limiting and damping **angular rates**
- **Operations**
- ...



LEO



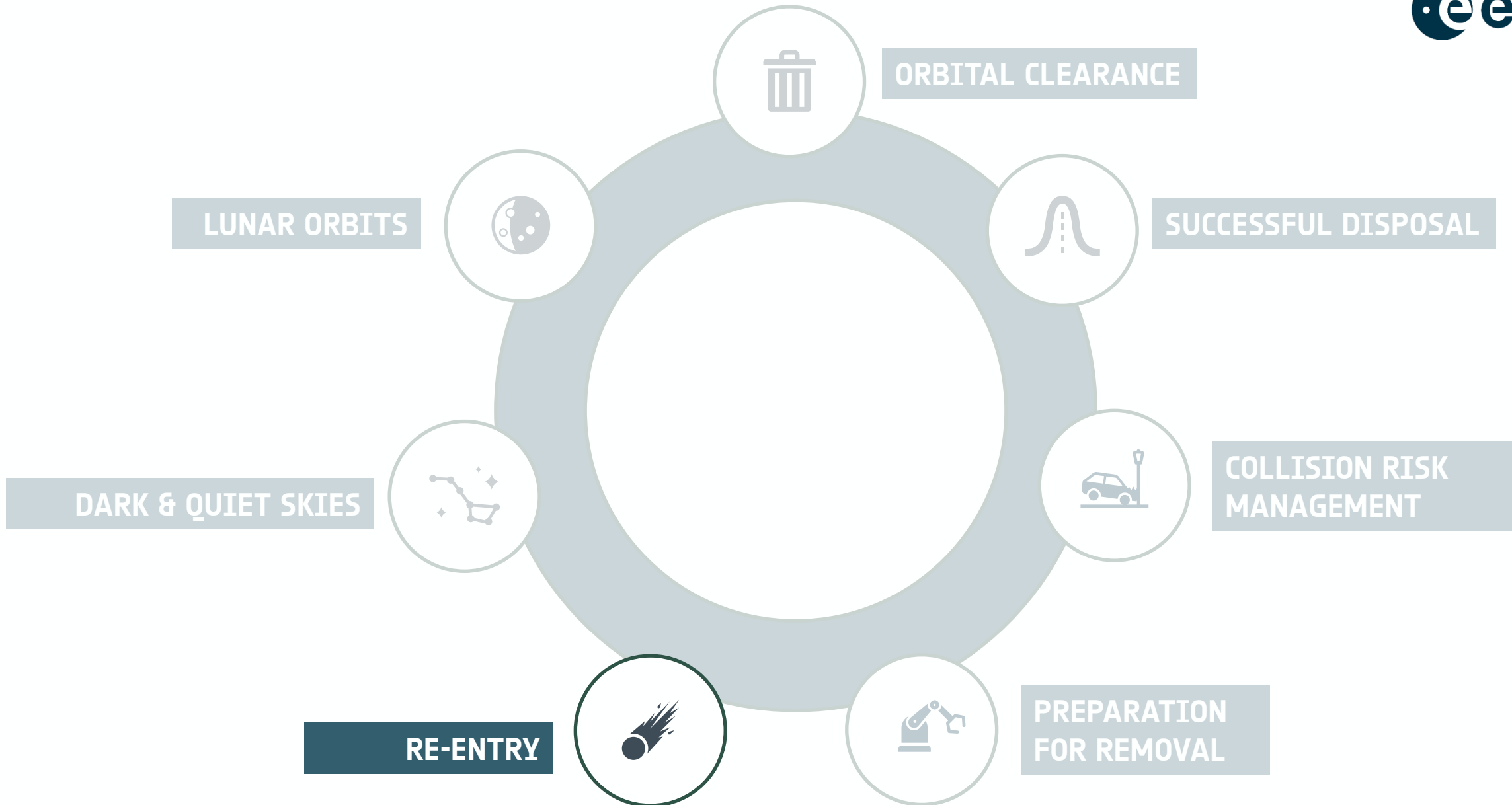
* In case of failure in orbit



Do D4R features make my mission a CPO mission?

Not automatically: the requirements related to Collision risk management for close proximity operations and formation flying (5.3.3.4) do not become applicable only because of the adoption of design-for-removal features





Re-entry

novelty level

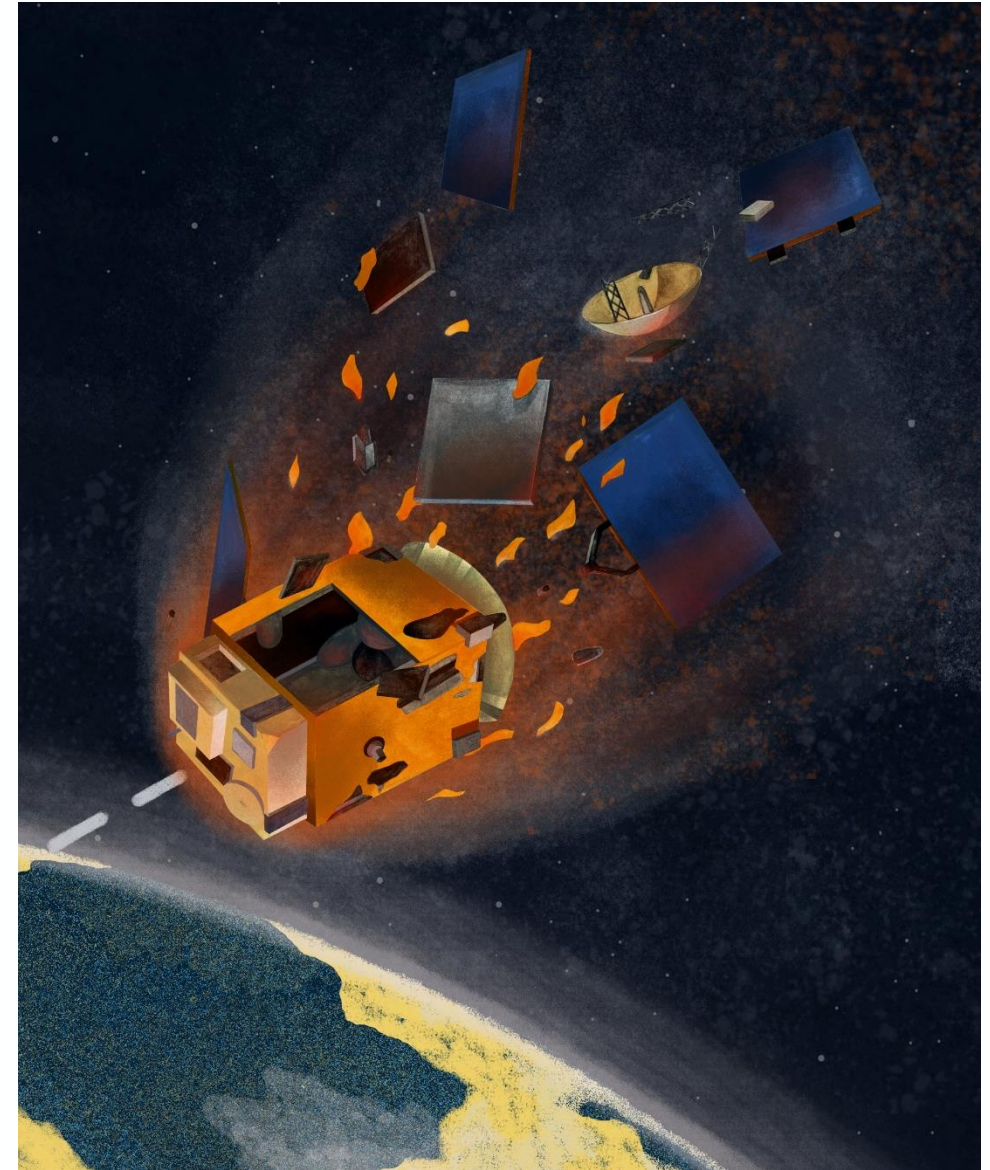


The main requirement has not changed:
re-entry casualty risk $< 10^{-4}$

ESA's Re-entry Safety Requirements (ESSB-ST-U-004)
remain applicable

What's new

- More stringent requirement for **large constellations** (10^{-6})
- Order of **preference** in how to achieve compliance
 1. Design for demise
 2. Controlled re-entry
 3. Any other approach needs approval



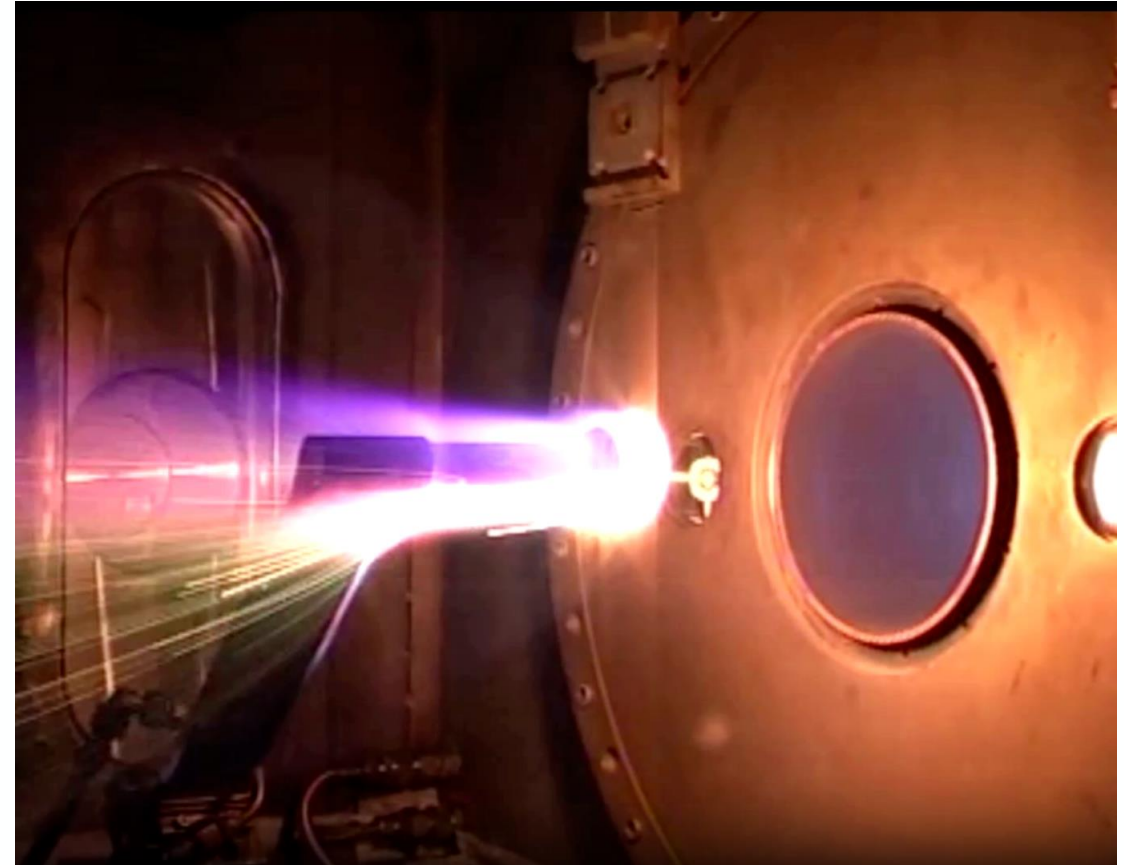
77



What about design-for-containment?

It requires approval by the approving agent (i.e. ESA's technical authority for space debris mitigation)

It won't be accepted without testing given that current simulation tools are not suitable to verify its efficacy and it is considered an approach for which TRL maturation is needed



Re-entry



novelty level

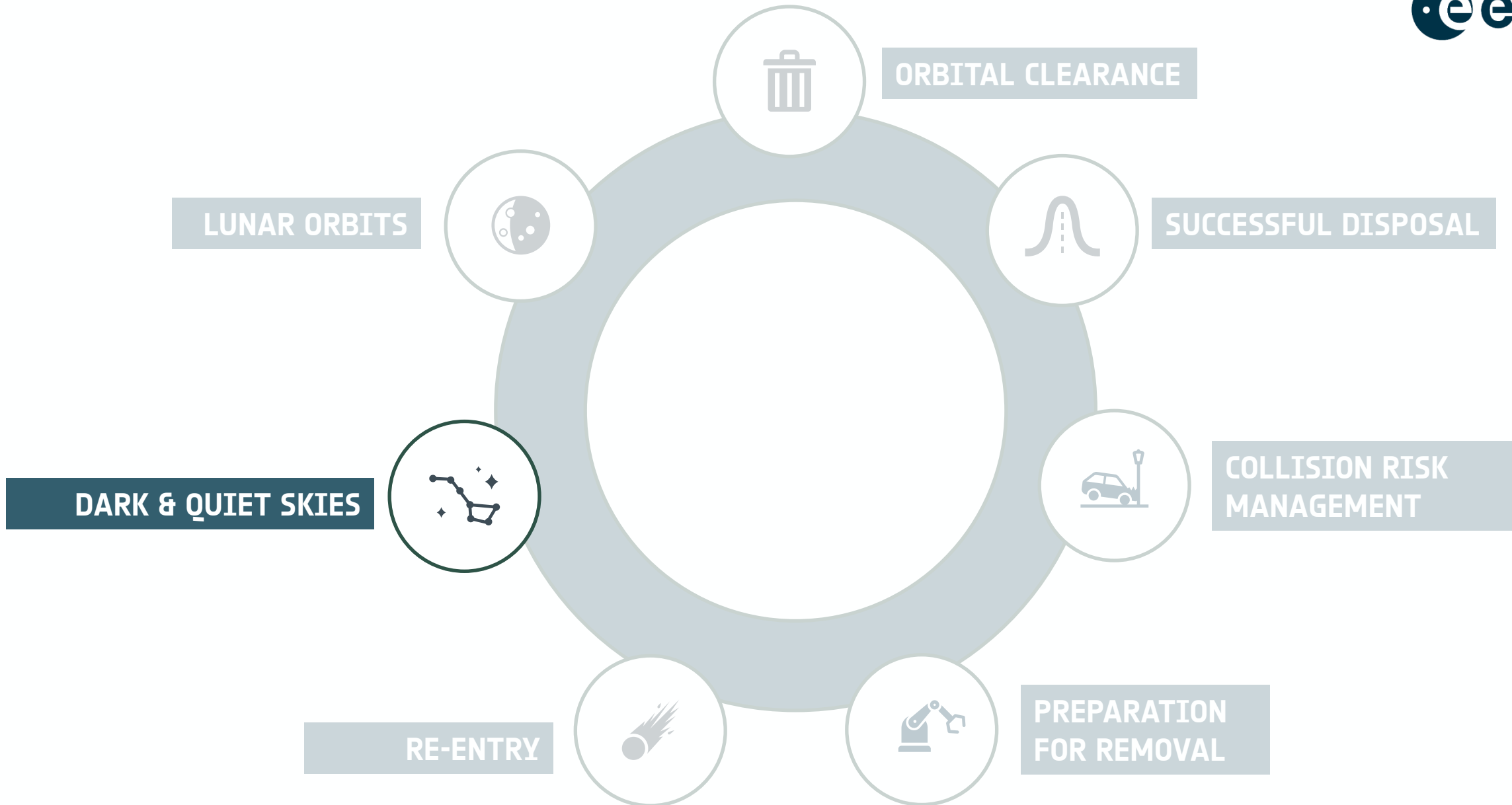


What's new

Explicit request for a **probabilistic assessment** of the casualty risk

- Uncertainty sources to be considered described in ESA Space Debris Mitigation Compliance Verification Guidelines (ESSB-HB-U-002-Issue 2),
- Modelling guidelines in DIVE - Guidelines for Analysing and Testing the Demise of Man-Made Space Objects During Re-entry (ESA-TECSYE-TN-018311)





Dark & Quiet Skies



novelty level



5.6.a

The developer of a spacecraft or launch vehicle orbital element in near Earth orbit shall quantify the visual brightness of the design.



Early phases (0-B)

Assess brightness assuming a combination of diffuse and/or specular reflection for primitive shapes (e.g. sphere, cylinder, flat plate).

Diffusive and specular reflection for surfaces is described using physical or empirical models, e.g. ideal Lambertian, or empirical Phong reflection models

ESA tools available (internally only at the moment) for such assessments



Later phases (B-C)

3D geometrical models describe the overall system using exposed subassemblies with different material properties.

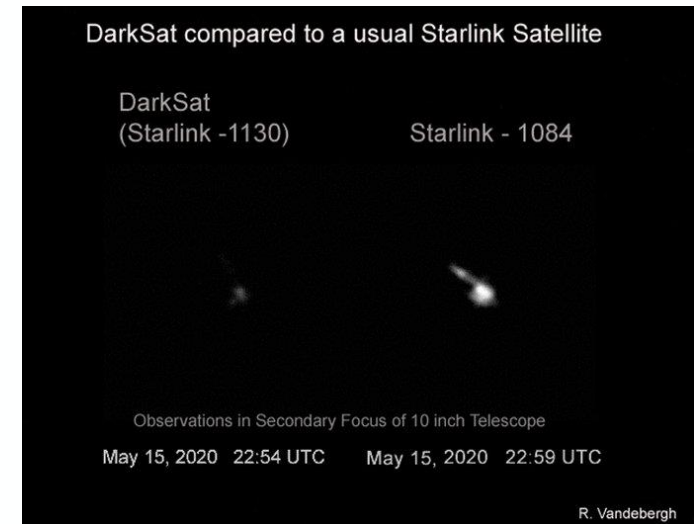
Material properties are described with specular or diffuse reflection models or with more complex bi-directional reflectance distributions (BDRF).

Identify specific conditions that may cause glints / strong reflections



After production (D onwards)

Regularly update the brightness estimate during the qualification phase with measured BDRFs of materials, exposed subassemblies, or the whole system.



DarkSat compared to a usual Starlink Satellite

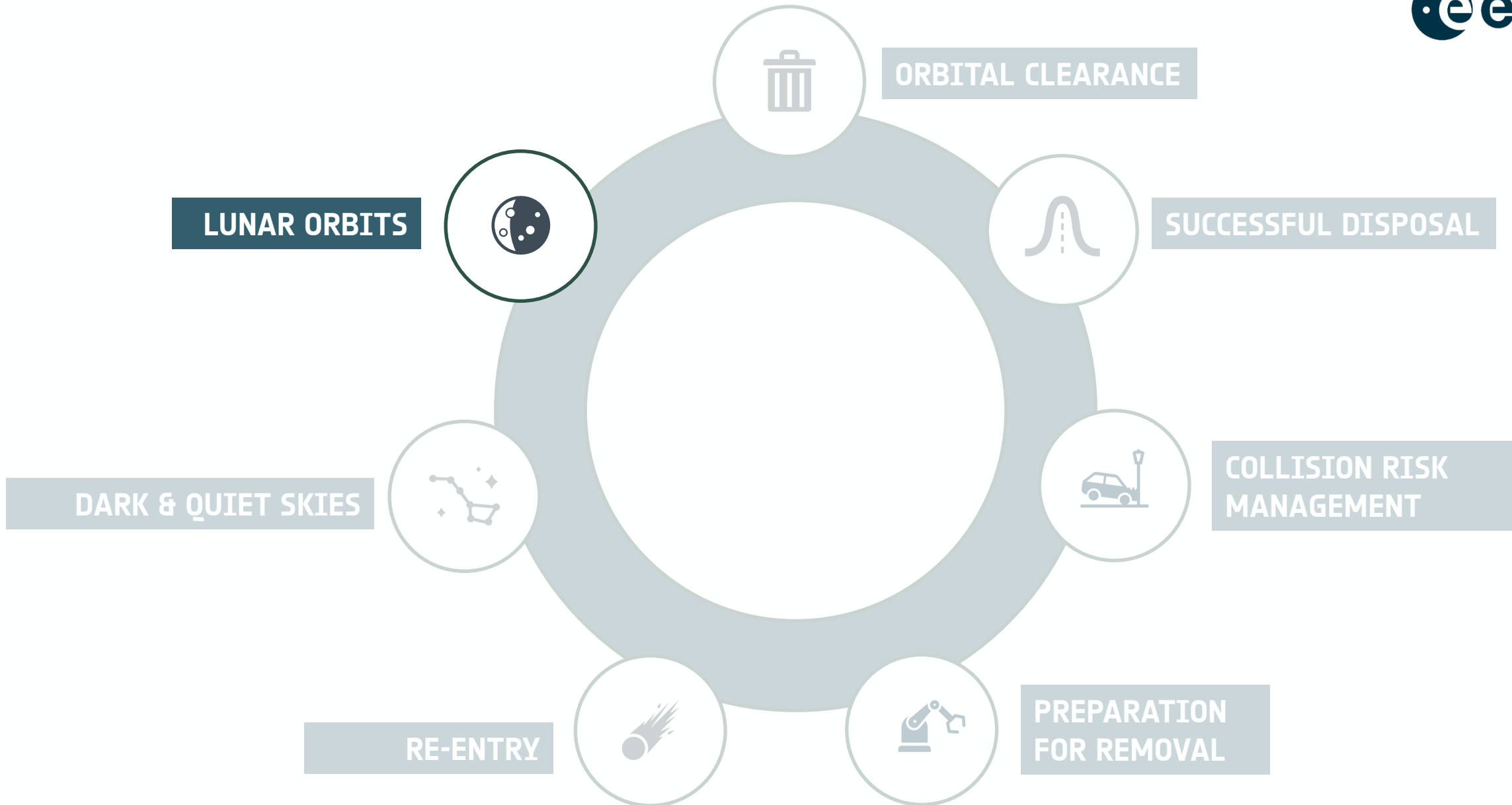
DarkSat (Starlink -1130)

Starlink - 1084

Observations in Secondary Focus of 10 inch Telescope
May 15, 2020 22:54 UTC May 15, 2020 22:59 UTC

R. Vandebergh





Lunar orbits

No intentional **breakup**

No **release** of space debris during normal operations

Space & ground segment designed to have **ephemerides** available for space traffic coordination

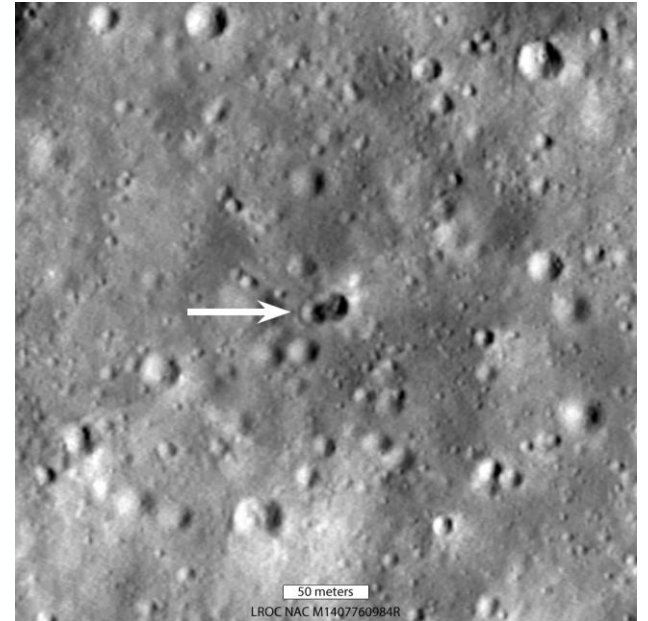
Disposal by one of the following means in order of preference:

1. **Heliocentric** orbit
2. Lunar impact, Earth re-entry, or a Lunar graveyard orbit

The free drift trajectories after disposal of a spacecraft or launch vehicle orbital element in lunar orbit shall be analysed for at least 100 years to evaluate:

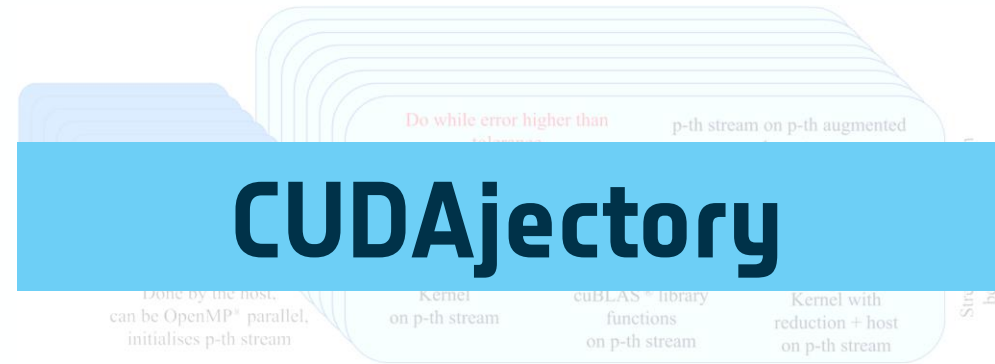
1. Probability of **Earth re-entry** and its associated impact area
2. Probability of **Lunar impact** and its associated impact area

Double crater created by the impact of a rocket body on the Moon in March 2022.
Credits: NASA/Goddard/Arizona State University



Lunar orbits - tools

For the propagation of lunar and libration point orbits, the following tools are recommended.
The tools are available in ESA member states through the <https://gitlab.space-codev.org/> website.



Application

long term propagation of lunar orbits,
e.g. to assess the variation of the orbital elements
of the lunar graveyard orbit

Application

parallel computation of large numbers of orbital states
e.g. long-term Earth re-entry risk analysis for spacecraft
in libration point orbits

Policy



Requirements



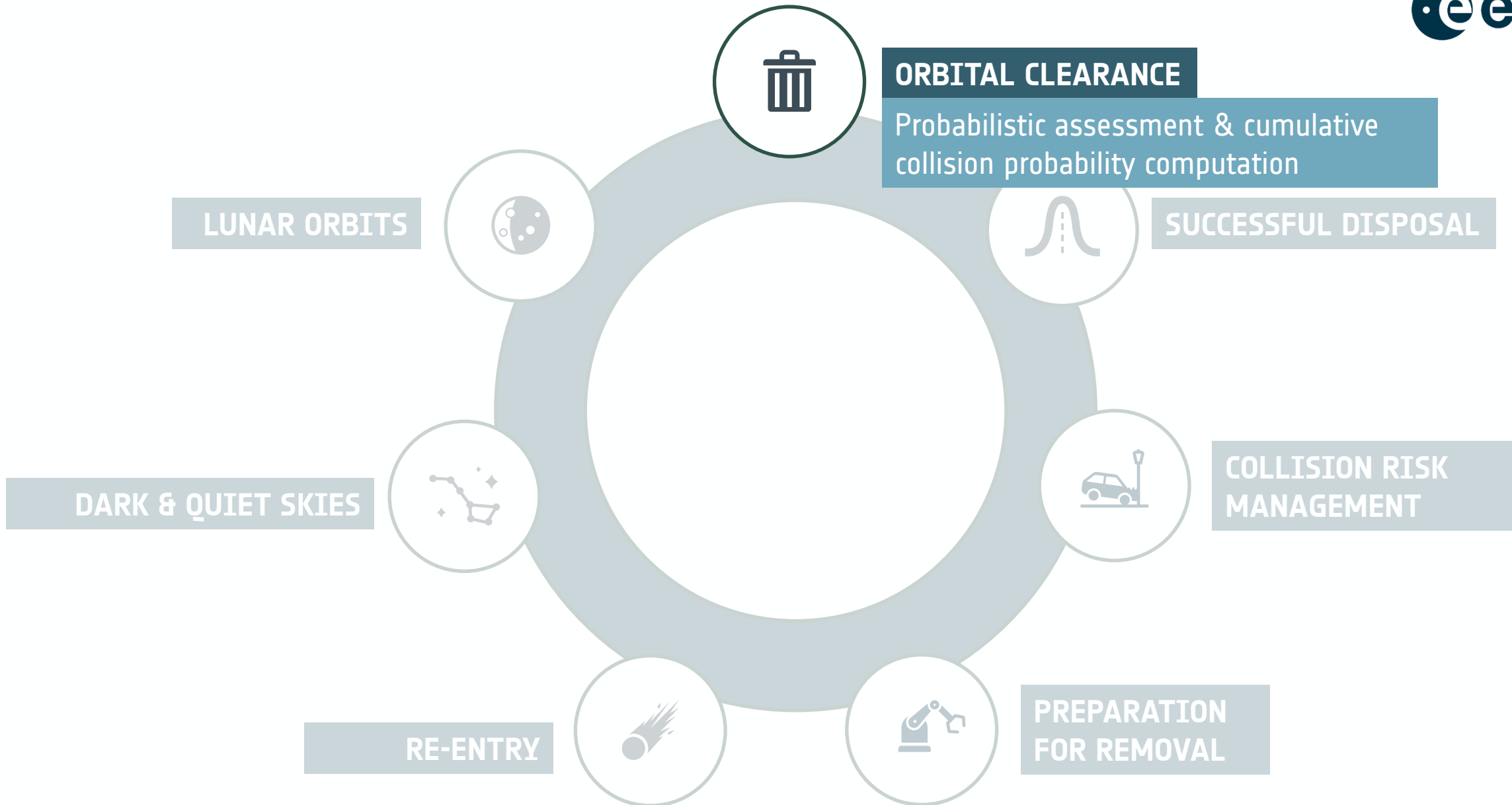
Handbook



Tools



space.debris.mitigation@esa.int



5.4.2.3.a

LEO protected region clearance

The orbit clearance of a spacecraft or launch vehicle orbital element from the LEO protected region shall satisfy both following conditions:

- 1) the **orbit lifetime** is less than 5 years [...]
- 2) the **cumulative collision probability** from its end of life until re-entry with space objects larger than 1 cm is below 10^{-3}

6.2

Verification and validation requirements

- f) The orbit lifetime of a space object shall be assessed **probabilistically**, including at least the variability by moving the starting point through a **full solar cycle** [...]
- g) For the orbit lifetime assessment, [...] the **50th percentile** for orbit with eccentricity below 0,3 at end of life [...]

Helper scripts available to support verification for orbital clearance and cumulative collision probability requirements

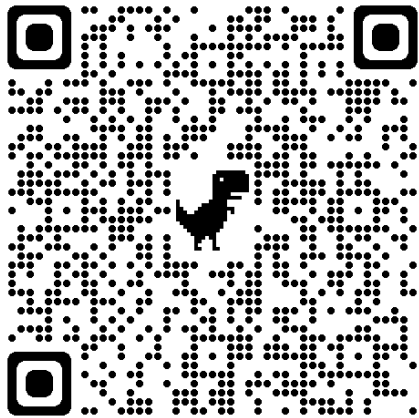
Computation of:

- Disposal trajectory for different **target lifetimes** and **disposal epochs** (aid probabilistic assessment)
- Associated **cumulative collision probability**

Orbital lifetime and cumulative collision probability



Where?



Space Debris Forum ▾ Home

Topics
My Posts
More
Categories
In-situ detection
Site Feedback
Uncategorized
All categories
Tags
master
drama
dmf
ares
in-situ
All tags
Messages
Inbox
DMs

Proof of concept script for cumulative collision probability computation

drama, ares, oscar

Philippe Meyers 17m 4 Oct

DISCLAIMER:
This script is intended as a proof of concept, not a complete verification tool. It is provided "as is", without implied warranty, without implied commitment to the accuracy of the results, and without commitment to support. It is only compatible with DRAMA version 3.1.0.

Cumulative Collision Probability Calculation

This script provides proof of concept on how to use the DRAMA Python package to calculate the cumulative collision probability of a given spacecraft, to check compliance with ESA's latest [Space Debris Mitigation Requirements](#). Specifically requirement 5.4.2.3a.2. This is done using the OSCAR and ARES tools in sequence. OSCAR is used to propagate the trajectory and can be used to verify compliance with 5.4.2.3a.1. Based on this propagation, ARES is used to calculate the annual collision probability for different orbital states along the propagated trajectory. The resulting probabilities are then accumulated to give a final collision probability value.

The results are written to a .res file in .csv format and some basic plots are generated.

The following files are provided:

- CCollProb.py contains class definitions that handle all the computations
- utils.py contains various functions for parsing input and output files
- run_CCo11.py is a sample program which runs a set of analyses using the previous modules
- example.py is a plaintext example input file for run_CCo11.py, based on an OSCAR oscar.inp input file format.
- requirements.py lists the required Python modules required for the script

[CCollProb.py](#) (28.8 KB)
[utils.py](#) (6.8 KB)
[run_CCo11.py](#) (5.3 KB)
[example.py](#) (5.4 KB)
[requirements.py](#) (195 Bytes)

1 / 1
4 Oct
17m ago

Example

<https://debris-forum.sdo.esoc.esa.int/>



pyDRAMA

Search docs

CONTENTS:

- Installation
- Getting started
- Known issues

Module Reference

- ARES**
- MIDAS
- OSCAR
- SARA

Examples

Developer Module Reference

```
drama.ares.run(config=None, dependent_variables=[], project=None, save_output_dirs=None, parallel=True, ncpus=None, timeout=None, keep_output_files='summary', spell_check=True, **kwargs)
```

Runs (parametric) ARES analysis and return the results.

- Parameters:
- **config** (dict or list) –
The (parametric) ARES run configuration. If a dictionary is provided it must be of the following format (lists are used for parametric analyses):

```
{  
  'epoch': datetime or list,  
  'sma': float or list,  
  'ecc': float or list,  
  'inc': float or list,  
  'raan': float or list,  
  'aop': float or list,  
  'spacecraft_radius': float or list,  
  'mass': float or list,  
  'functionality': int or list,  
  'particle_size_min': float or list,  
  'particle_size_max': float or list,  
  'EMR_switch': int or list,  
  'uncertainty_type': int or list,  
  'uncertainty_along': float or list,  
  'uncertainty_cross': float or list,  
  'uncertainty_radial': float or list,  
  'lead_time': float or list,  
}
```

OSCAR for disposal trajectory computation

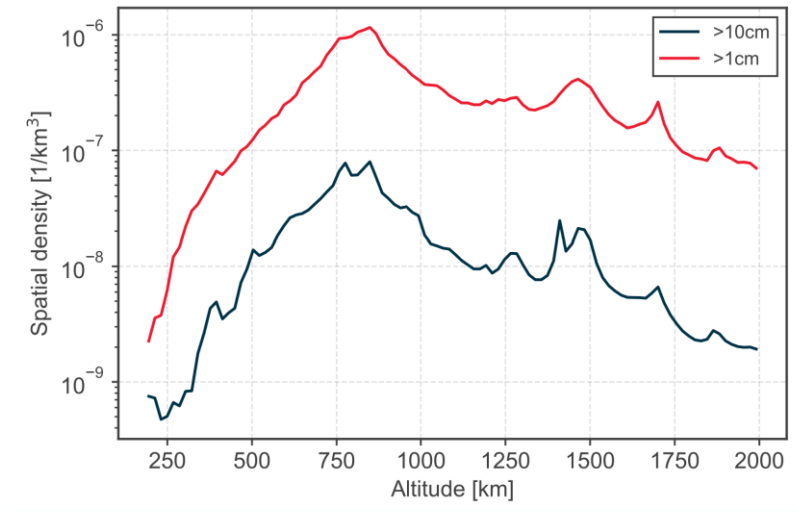
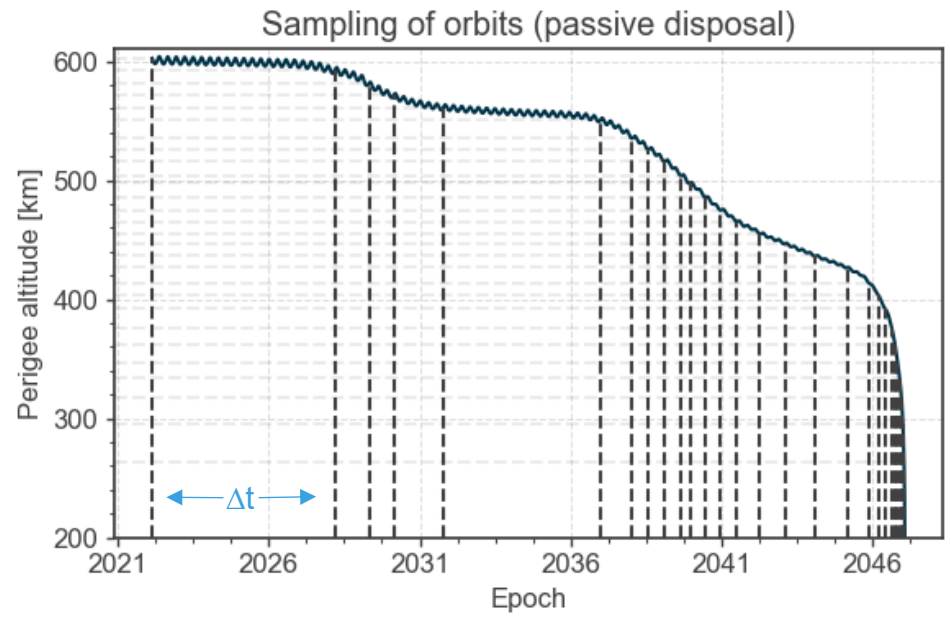
ARES for cumulative collision probability computation

https://sdup.esoc.esa.int/drama/python_package_docs/index.html

Space Debris User Portal (esa.int) · Tools · DRAMA

Cumulative collision probability computation

1. OSCAR for disposal trajectory computation
2. Discretise trajectory: steps of 10 km in perigee altitude (LEO)




ESA's Space Environment Report

1 cm calibrated population (no forecast)

3. ARES annual collision probability (ACP) over each slice
4. Scale to slice duration (Δt) and aggregate probabilities

Orbital clearance: script inputs

- OSCAR input file (from DRAMA GUI or template)

Spacecraft parameters	<ul style="list-style-type: none">• Mass• Cross-sectional area <div data-bbox="1128 425 1695 549" style="border: 1px solid blue; padding: 5px; display: inline-block;"> Including appendages e.g. solar panels</div>
Disposal options	<ul style="list-style-type: none">• Free drift or delayed de-orbit• Target lifetime configurable e.g. [1.5, 3, 5] years in script
Begin date	<ul style="list-style-type: none">• End of operation epoch• Varied forward over solar cycle (yearly steps)
Initial orbit	<ul style="list-style-type: none">• Starting orbit of disposal
Solar activity scenario	<ul style="list-style-type: none">• May be performed with different solar activity models

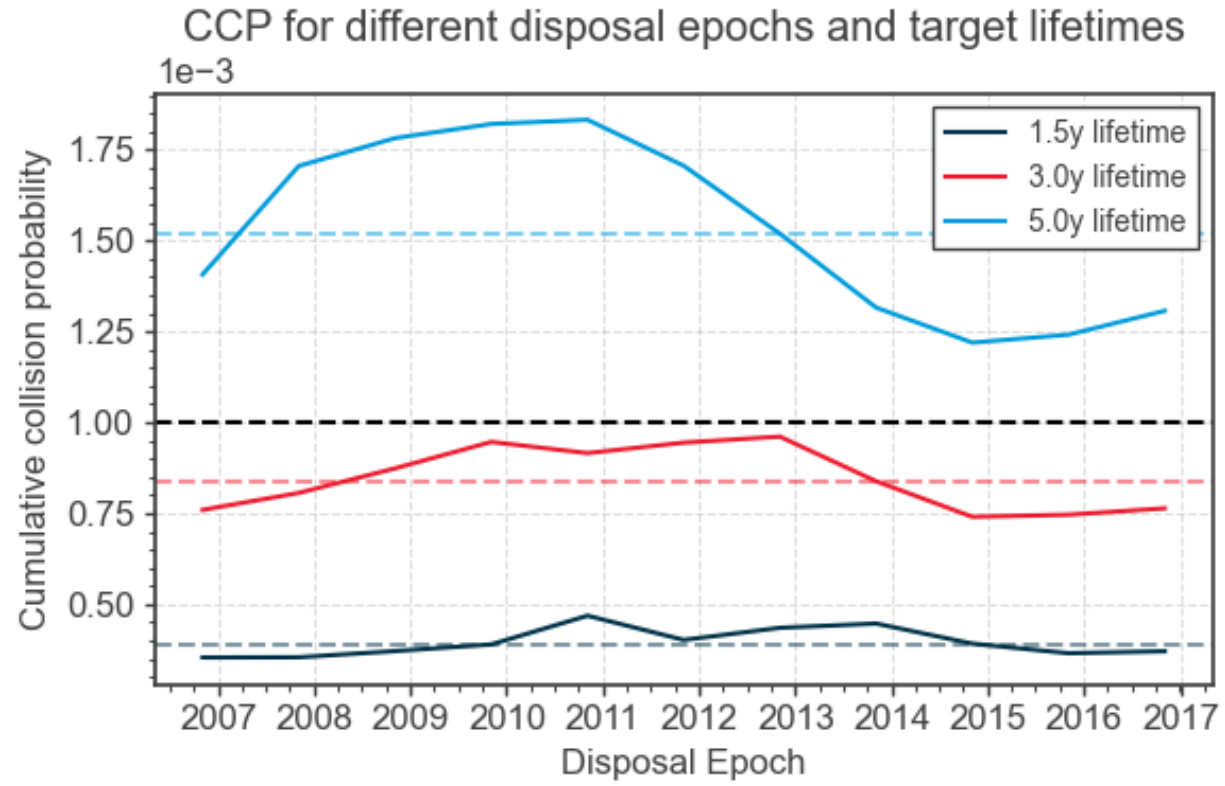
- Runs in a parallelised fashion

Verification and validation requirements

e) [...] The cumulative collision probability is computed considering the complete space object geometry, **including appendages**, unless it is demonstrated that specific appendages can be hit by objects larger than 1 cm without generating space debris.

6.2

Orbital clearance: script outputs

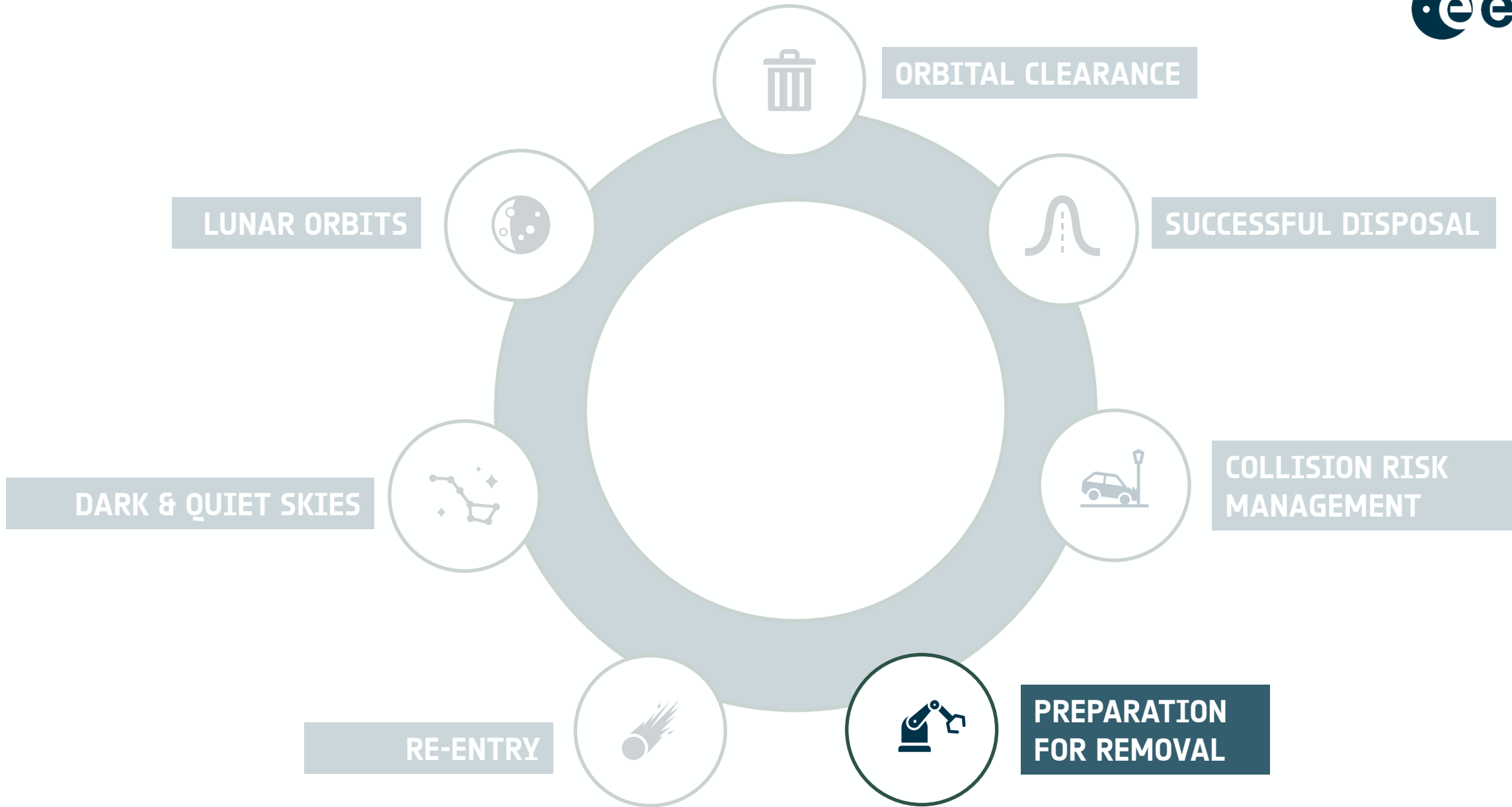


- 5-year lifetime would not be compliant with cumulative probability requirement
- Median value of sampled trajectories (or trajectory closest to median computed lifetime)

Vary disposal epoch over solar cycle →

CCP: Cumulative Collision Probability



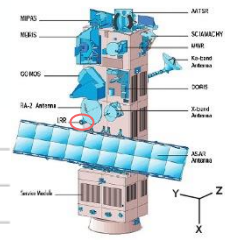
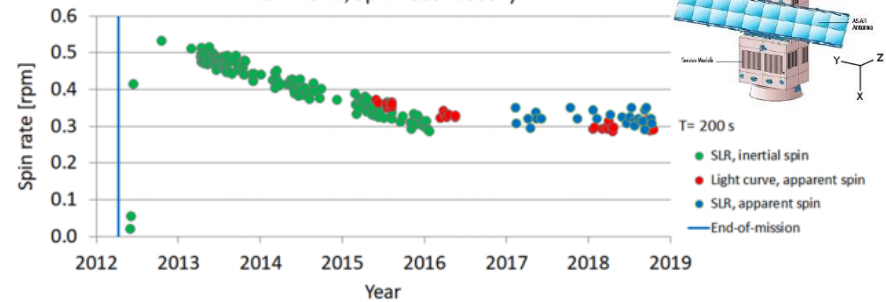


Why Design-for-Removal is needed?

Active Debris Removal (ADR) is challenging, but crucial to maintain a sustainable orbital environment

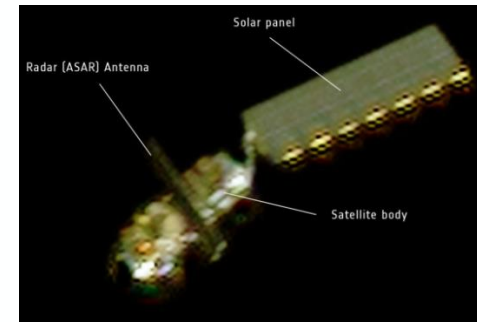
Debris object spin

ENVISAT, spin rate history

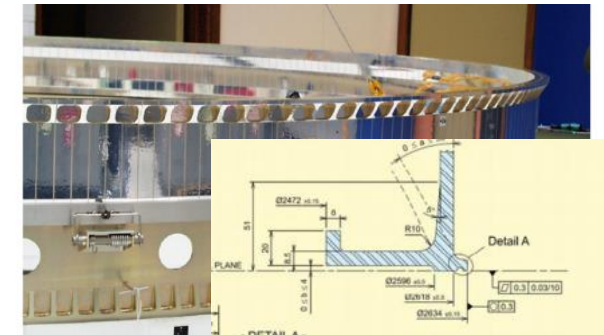


ENVISAT Retroreflector

Debris object not designed for capture



Missing capture interfaces



To enable ADR, we need to prepare the satellites to be removed → Design for Removal (D4R)

D4R implies dedicated modifications to cover certain **functions**, in order to ease removal by external servicer and decrease associated risks and costs

The most optimal approach is to find a **standard D4R solution (or standard D4R interface)** for all missions → only one servicer design

What is a standard D4R interface?

A standard D4R solution or interface shall cover different functions:

Capture

Relative navigation for rendezvous

Attitude reconstruction from ground

LEO

Detumbling

LEO

Cooperative

- The satellite is operational but unable to perform the end-of-life functions with respect to removal from orbit.

Uncooperative

- The satellite is non-operational (either completely or with respect to attitude control) and tumbling.

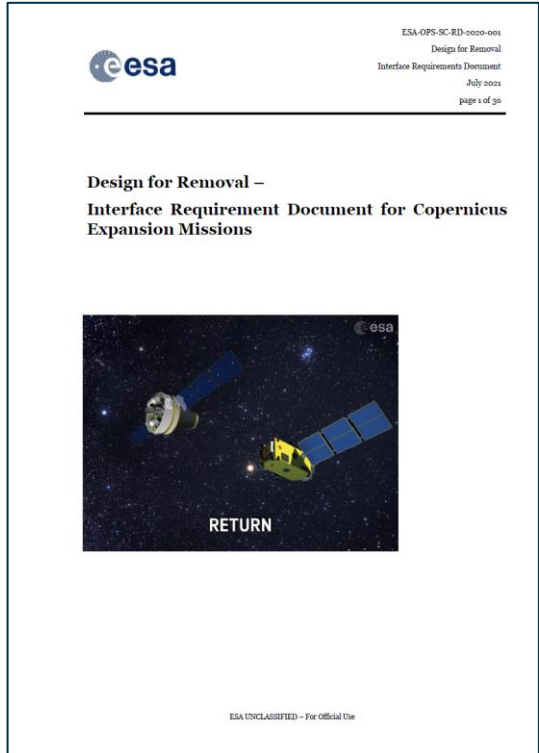
For **cooperative scenario** and prepared targets, it is assumed the target:

- Is prepared for capture (e.g. dedicated mechanical capture interface, rendezvous markers / navigation supports implemented)
- Can provide telemetry to the mission control centre of the debris removal service provider
- Capable to perform attitude control
- Will not hinder the capture process (e.g. thrust during the final moment before capture).

For **uncooperative scenario** and prepared targets, it is assumed the target is:

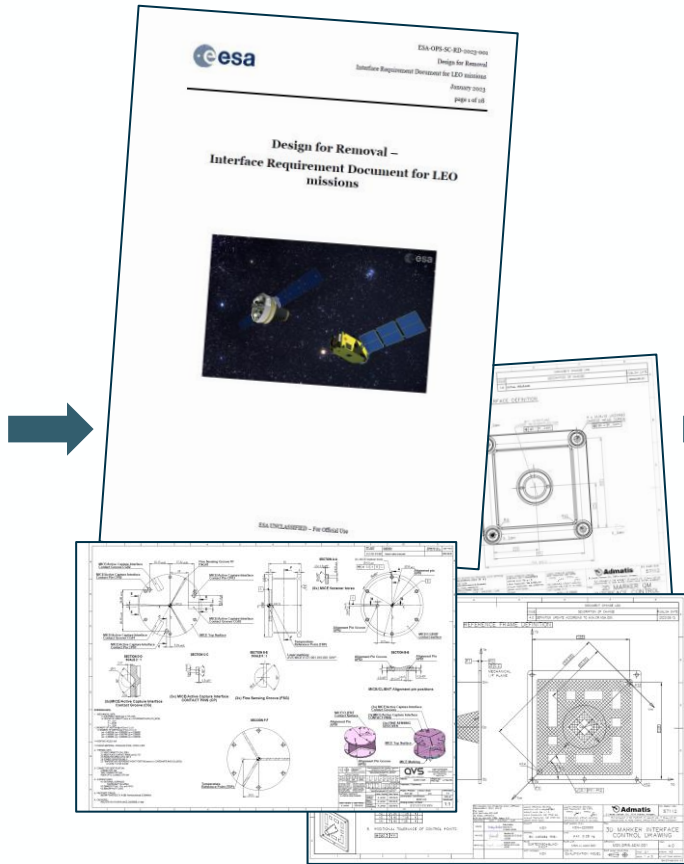
- Prepared for capture (e.g. dedicated mechanical capture interface, rendezvous markers / navigation supports implemented)
- Unable to provide telemetry on the status, all information on target status based on observations from ground
- Characterisation of tumbling motion shall be done in orbit by the chaser.
- Unable to perform attitude control

D4R Interface Requirements Document



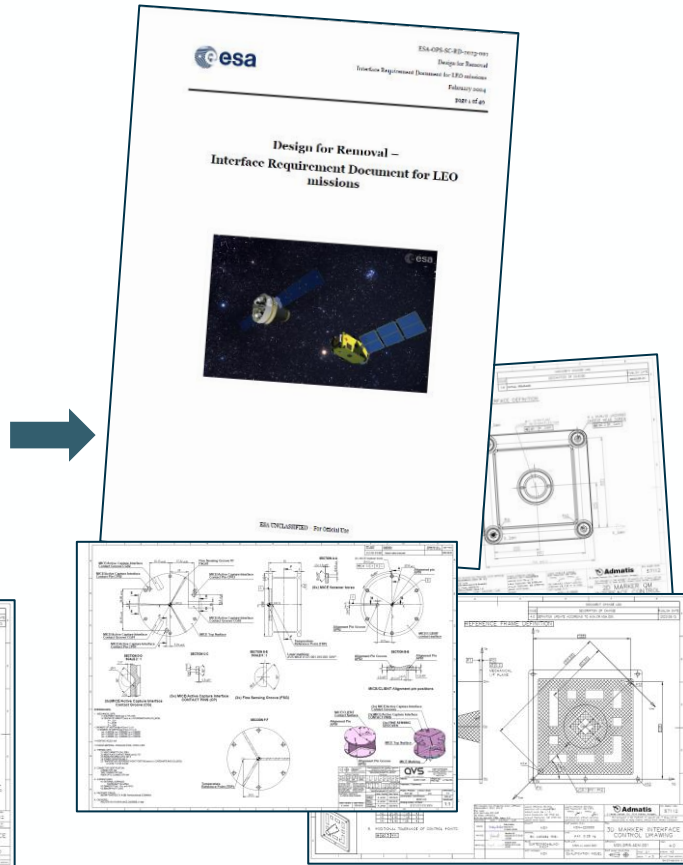
First D4R IRD for Copernicus Expansion Missions released in 2020

Applicable for Copernicus only



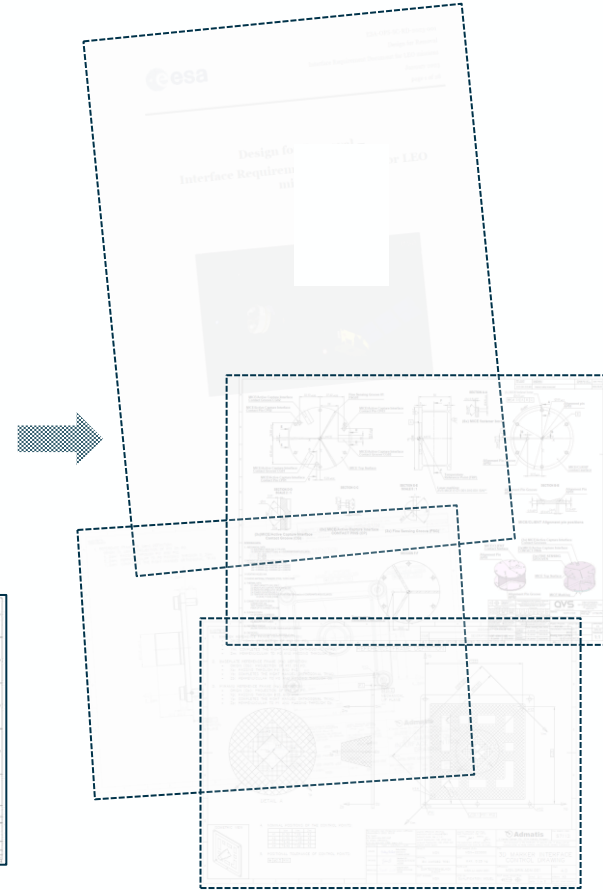
First D4R IRD for LEO missions released in 2023
MICE, 2D marker and 3D marker ICDs

Applicable for LEO missions performing a controlled re-entry



Second D4R IRD for LEO missions released in 2024
MICE, 2D marker and 3D marker ICDs

Applicable for LEO missions performing controlled or uncontrolled re-entry



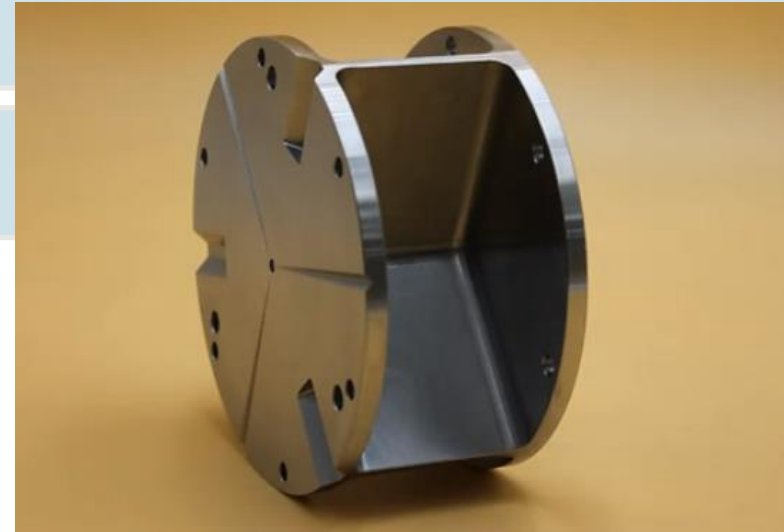
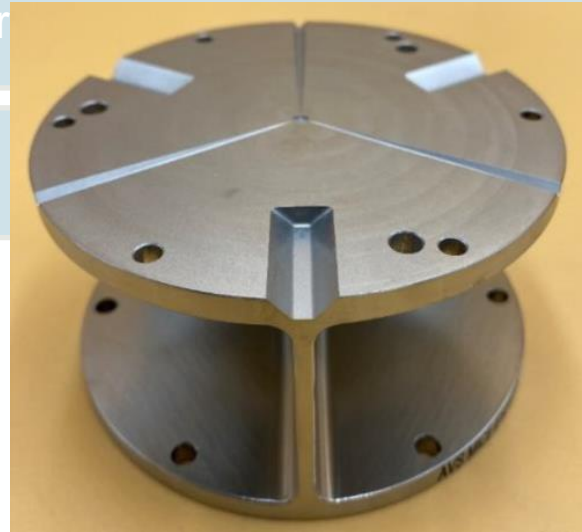
Future D4R IRD data-package releases for other applications

Capture

Relative navigation for rendezvous

Attitude reconstruction from ground

Detumbling



MICE – Mechanical Interface for Capture at EOL

D4R Technologies – Relative Navigation and attitude reconstruction

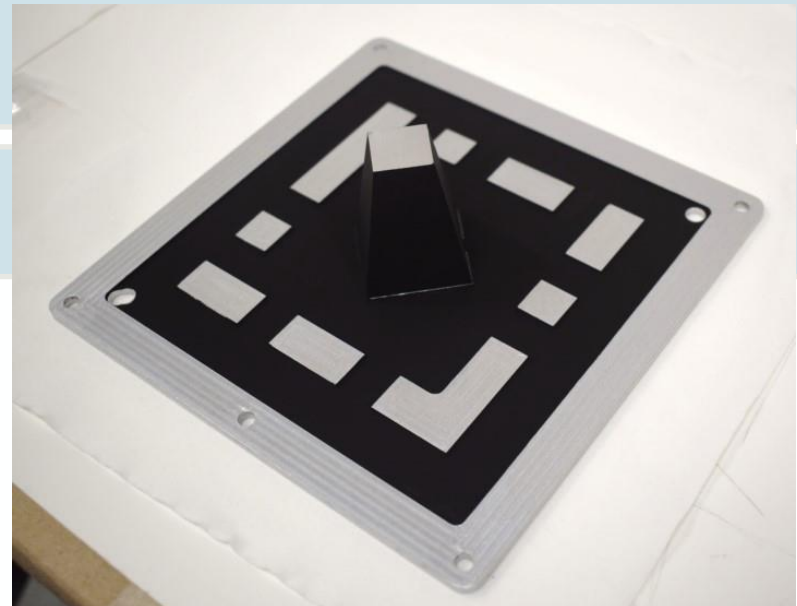
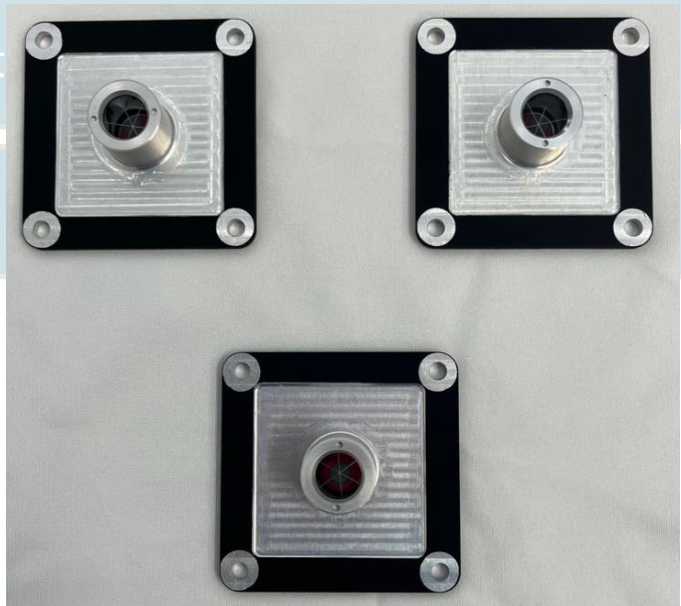


Capture

Relative navigation for rendezvous

Attitude reconstruction

Detumbling



MSN – Markers to Support Navigation



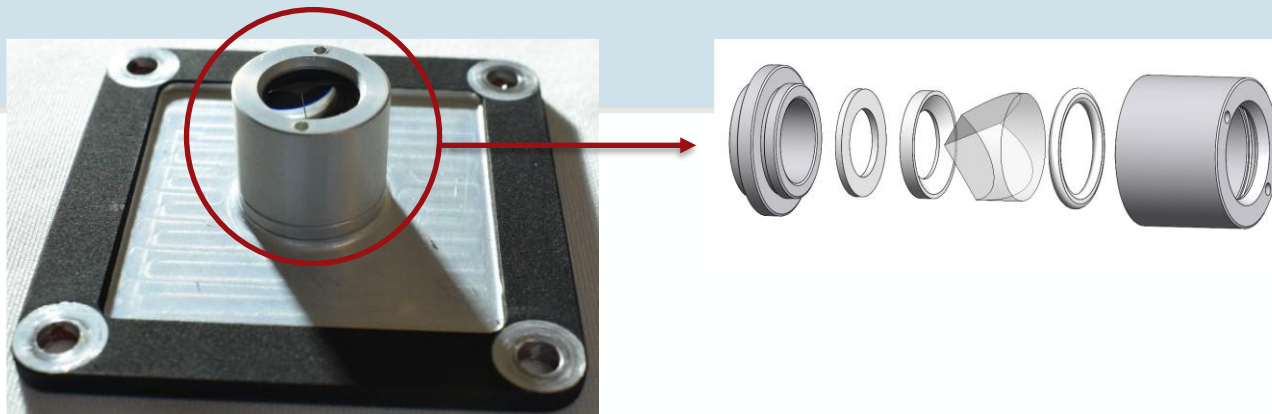
D4R Technologies – Relative Navigation and attitude reconstruction

Capture

Relative navigation for rendezvous

Attitude reconstruction from ground

Detumbling



LRRs – Laser Retro-Reflectors (embedded on 2D Markers)

D4R Technology – Detumbling



Capture

Relative navigation for rendezvous

Attitude reconstruction from ground

Detumbling



Short-circuited magnetorquers



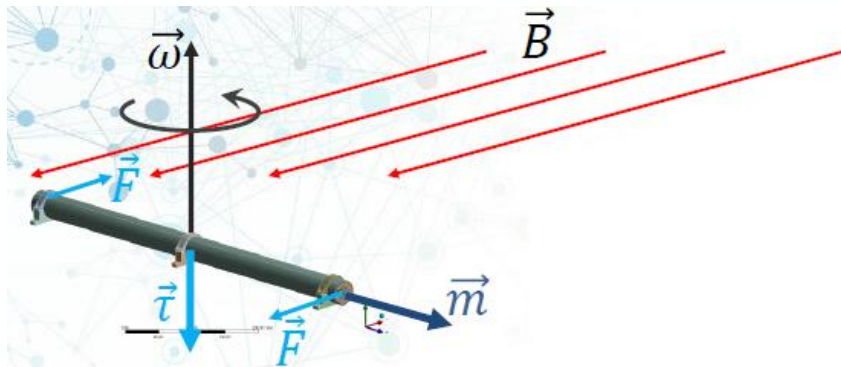
Stabilisation of tumbling motion

Short-circuited magnetorquer

Patent Reference:
213130EP TE/BD

Idea: a short-circuited magnetorquer can still produce a torque helping detumbling...

1. a rotating satellite in LEO sees a time-dependent magnetic field created inside the magnetorquer
2. the magnetic flux variation produces an electromotive force at the magnetorquer terminals
3. an induced current is generated on the coil wire
4. resulting in the magnetorquer magnetic moment and generated torque
5. the dissipation of rotational kinetic energy is achieved through Joule effect inside the magnetorquer



Magnetic moment induced by changes in magnetic flux



Proof of concept of short-circuit triggering system (left)
and short-circuited magnetorquer (right)

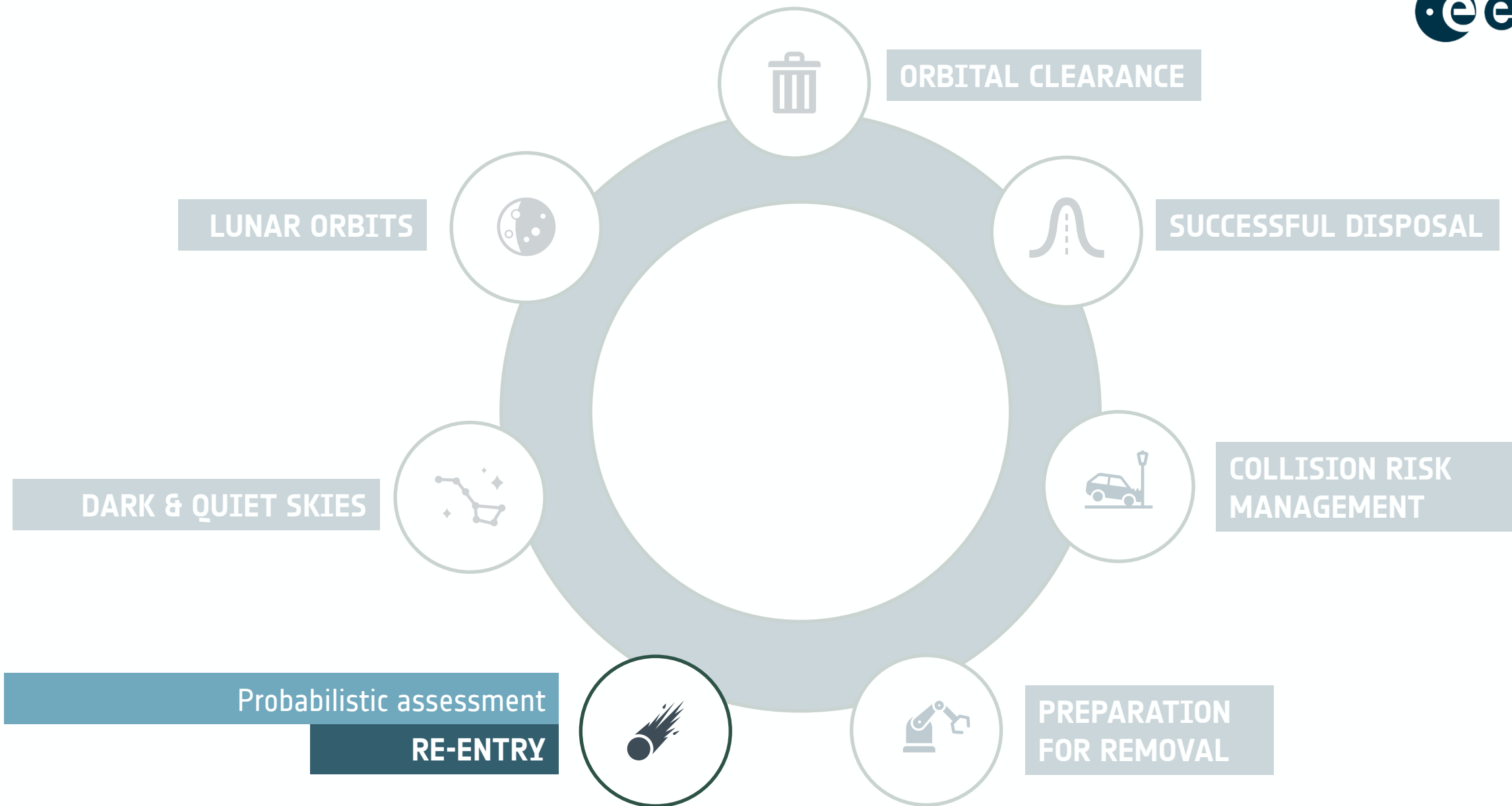
How can we design for the cooperative scenario?

...given that no service is currently readily available in LEO?

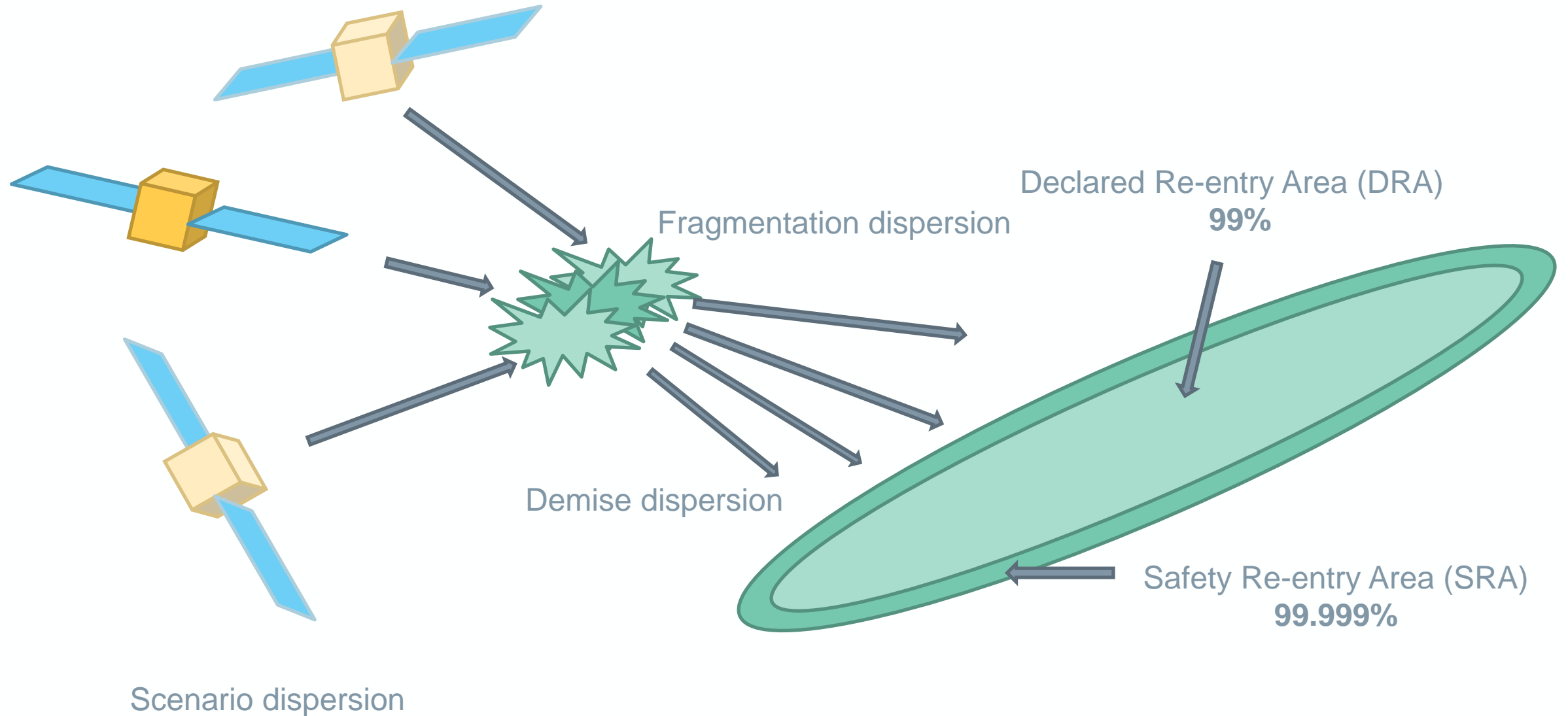
We understand that this is a gradual process, so a first step is to design a Safe Mode compatible with capture i.e.

- stable angular rates
- prevention of AOCS from reacting against capture
- orientation of appendages to ensure access to the mechanical capture interface

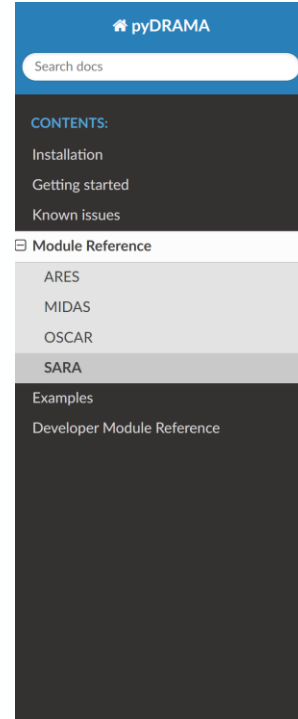
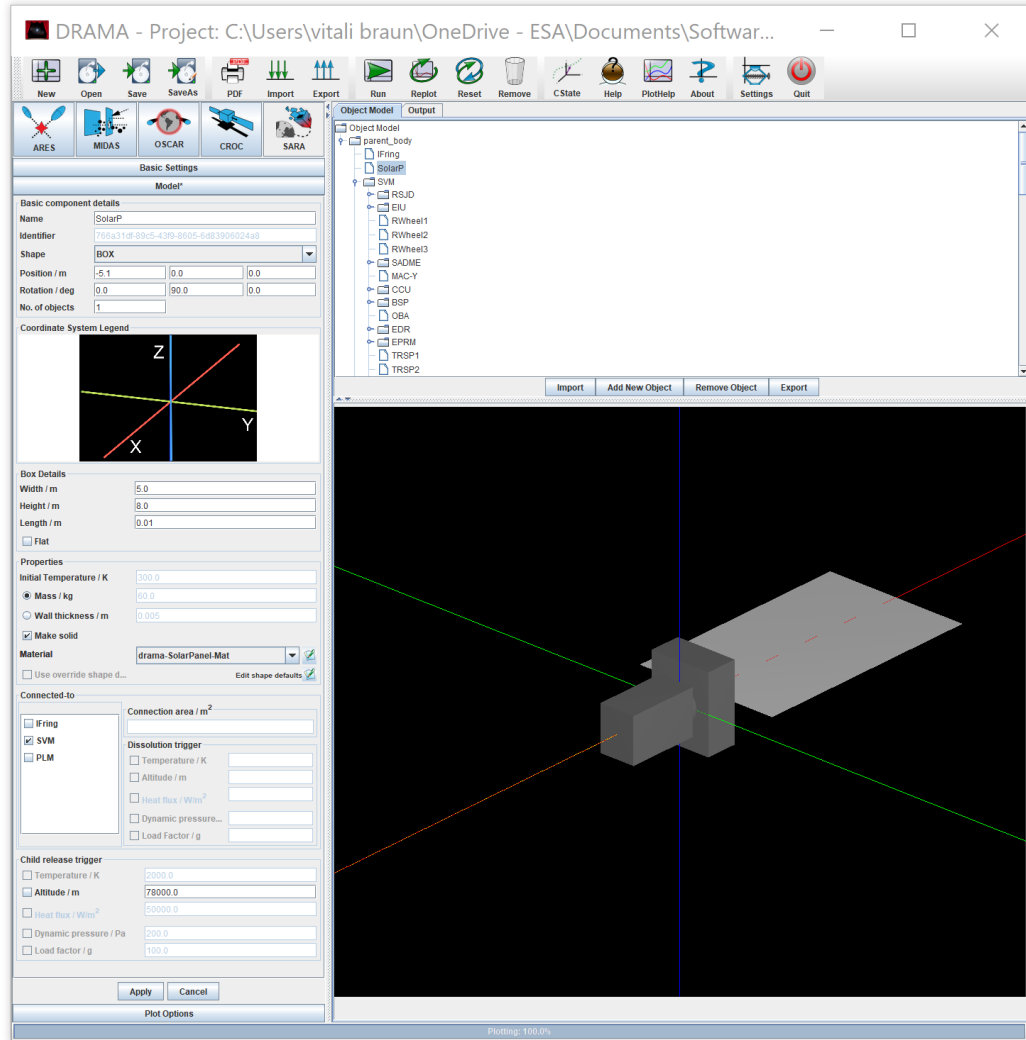




Probabilistic Assessment of Re-entry Risk



DRAMA 3.1.0 and Python Package



```
drama.sara.run(config=None, dependent_variables=[], project=None, save_output_dirs=None, parallel=True, ncpus=None, model=None, timeout=None, keep_output_files='summary', spell_check=True, create_fig=False, **kwargs)
```

Runs (parametric) SARA analysis and return the results.

Parameters:

- **config** (dict or list) – The (parametric) SARA run configuration. If a dictionary is provided it must be of the following format (lists are used for parametric analyses):

```
{
  'runMode' : str
  'coord' : str
  'epoch' : datetime or list,
  'e1' : float or list,
  'e2' : float or list,
  'e3' : float or list,
  'e4' : float or list,
  'e5' : float or list,
  'e6' : float or list,
}
```

Alternatively, **config** can also be a list of config dictionaries, or any iterable. Each config dictionary in this case describes one run and thus can not contain any list to expand.

- **dependent_variables** (list of lists of str) – Describe which parameters depend on each other in a parametric analysis. Each list of parameters defines one dependency. See the example below for details.
- **project** (str) – Path to DRAMA project to use as baseline (directory or exported project). If **None** the default project is used.
- **save_output_dirs** – Save the output directories of all runs to this directory. Each run will have its own numbered directory. The path to it is stored in **output_dir** in each run's config. If **None** the output directories will be deleted.

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- 📁 Topics
- 👤 My Posts
- ⋮ More
- ▾ Categories ✎
- 🟣 In-situ detection
- 🟡 Site Feedback
- 🟢 Uncategorized
- ☰ All categories
- ▾ Tags ✎
- 👉 dmf
- 👉 master
- 👉 drama
- 👉 in-situ
- ☰ All tags

Example Scripts for Performing Monte Carlo Analyses using SARA



Daniele Bella

May '23

May 2023

Calculating the SRA and DRA (Safety and Declared Reentry Areas) for a mission, as well as the on-ground casualty risk, is an important part of a controlled reentry's safety analysis. One of the ways that it can be computed is through the use of a Monte Carlo simulation.

Though the DRAMA GUI provides a "Monte Carlo Analysis" mode, this is in reality a parametric analysis, without randomised parameters. However, it is possible to use DRAMA for "true" randomised Monte Carlo analyses using the DRAMA python package and some scripting. In order to show how this could be performed, and how each of the major parameters of a SARA run can be randomised, we created a set of example scripts. These were designed to be used as a reference and/or starting point during the development of more complex and comprehensive calculations; they are thus heavily commented and feature simplified algorithms, for the sake of understandability. They can and should be expanded upon based on the needs of your analysis, in order to encompass other parameters or to make use of more rigorous but more complex methods.

In fact, if you have any suggestions for improvements, or want to share your experience in tailoring them to a mission's needs, don't hesitate to reply to this post! Everyone can then learn from it, and in future it even helps us provide better examples and tools.

What the example scripts cover

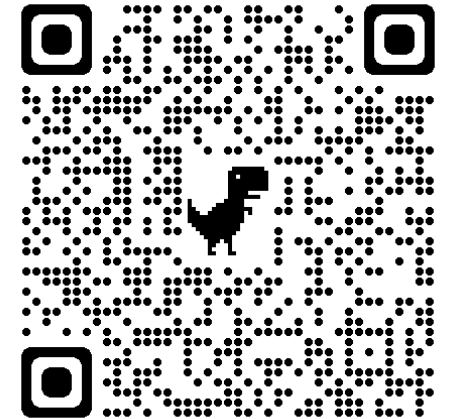
- Opening a nominal example SARA project
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- Compiling these inputs into the format required for SARA
- Running SARA in a parallel fashion for each case
- Parsing the results, calculating the overall casualty risk
- Using the location of the fragments, using a simplified and conservative algorithm to calculate the SRA and DRA

These are all the necessary files:

- 📄 [SARA_MC_script.py](#) (10.3 KB)
- 📄 [SARA_MC_helpers.py](#) (20.0 KB)
- 📄 [example_project.dpz](#) (3.8 MB)

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```
222 if __name__ == "__main__":
223     # Load the base model
224     base_model = sara.get_model(project=PROJECT)
225     # Load the base config
226     base_config = sara.get_basic_config(project=PROJECT)
227
228     # Generate the list of randomised configs, models and project_paths
229     configs = create_config_from_burn(
230         base_config, START_ORBIT_STATE, DELTA_V, n=NUM_RUNS
231     )
232     models = randomise_model(base_model, n=NUM_RUNS)
233     project_paths = randomise_project_xml(PROJECT, n=NUM_RUNS)
234
235     # Get inputs in the correct format for multiprocessing
236     func_inputs = []
237     for i in range(NUM_RUNS):
238         func_inputs.append([models[i], configs[i], project_paths[i], i])
239
240     print("Created config, running SARA...")
241     with Pool(NCPUS) as p:
242         p.starmap(run_sara, func_inputs)
243
244     # Parse the result
245     parsed_reentry_result = parse_reentry_results_xml("output")
246     parsed_risk_result = parse_risk_results_xml("output")
247
248     # We now have the locations of every single fragment! We can use this however we like.
249     # For example, we could use it to calculate the SRA and DRA from the impacts. Here is a
250     # very simplified function
251     ra_df = calc_reentry_area(parsed_reentry_result, [0.99, 0.9999])
252
253     # Calculate the total 2D casualty risk for the whole simulation
254     tot_casualty_risk = 1 - np.prod(
255         1 - parsed_risk_result["totalCasualty2D"] / NUM_RUNS
256     )
257     print(f"The computed casualty risk is {tot_casualty_risk}")
258
259     ## Plot the data
260     SRA_boundary = ra_df[ra_df["Threshold"] == 0.99]
261     SRA_boundary = pd.concat([SRA_boundary, SRA_boundary])
```

➤ Load nominal model and conditions from DRAMA project

➤ **Create N runs with independently randomised parameters**

1. Randomise orbit and final burn
2. Randomise the SARA model properties
3. Randomise material properties

➤ Run SARA in a parallelised fashion

➤ Parse outputs

➤ Calculate SRA and DRA

➤ Calculate Overall (averaged) casualty risk

➤ Plots

1. Initial conditions in stochastic simulations

Example scenario uncertainties available in ESSB-HB-U-002:

Table D-1: Approach for initial conditions for stochastic simulations

Re-entry type	Orbit type	Initial Conditions	Uncertainties
Uncontrolled	Decaying circular orbit	Altitude: 130 km x 130 km Semi-major axis: 6501 km	Argument of perigee with uniform distribution across an
Uncontrolled	Targeted circular orbit		
Controlled	Targeted circular orbit		
Uncontrolled or controlled	Highly eccentric or interplanetary		

D.2.2.1 Uncertainties for nominal controlled or off-nominal uncontrolled re-entry

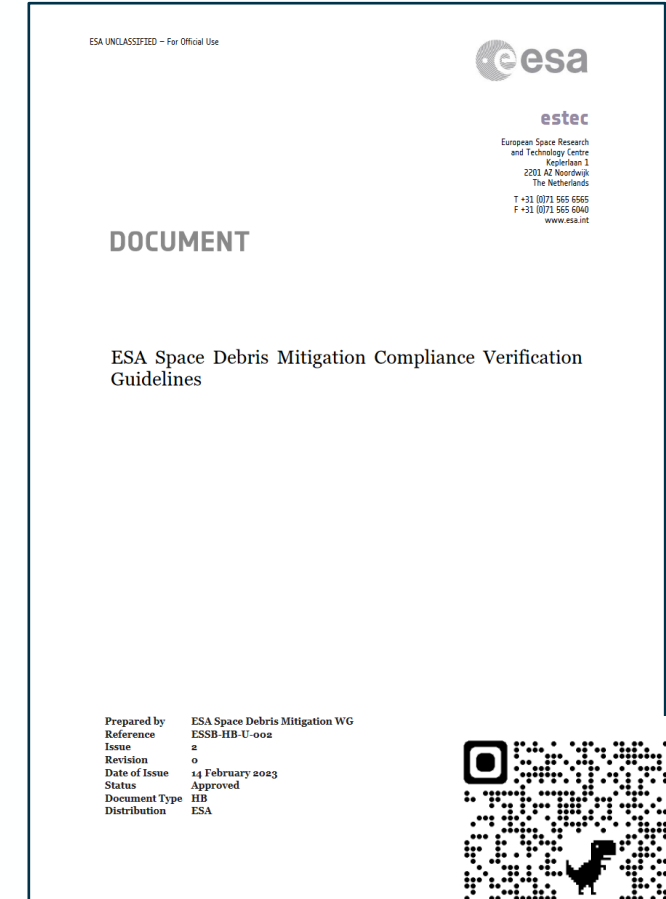
The re-entry casualty risk analysis is performed for each relevant mission scenario with sufficient confidence to cover all re-entry uncertainties:

- Nominal case, e.g. controlled or uncontrolled re-entry.
- Off-nominal cases, e.g. degraded controlled re-entry and uncontrolled re-entry due to failures prior to enter the nominal case.

The uncertainties for the nominal and off-nominal cases are identified and taken into account depending on the space system design and operations.

For example, the following dispersion parameters have been considered for the ESA ATV controlled re-entries:

- Position at last boost ignition: ± 3 km
- Burn Start Time: ± 5 s
- Delta-v realisation dispersion: Gaussian, 1σ (e.g. ± 5 %)



...but should be tailored to your mission

1. Initial conditions in stochastic simulations

```
110 # Position uncertainty
111 #####
112
113 # Create random unit directions to have noise be in
114 dir_array = np.random.uniform(low=-1, high=1, size=(n, 3))
115 dir_array_norm = np.linalg.norm(dir_array, axis=1)
116 dir_array = dir_array / np.tile(dir_array_norm, (3, 1)).T
117
118 # Scale this random direction by a random scale
119 pos_scale_arr = np.random.uniform(low=0, high=pos_uncert, size=(n))
120 pos_noise_arr = dir_array * np.tile(pos_scale_arr, (3, 1)).T
121
122 # Manoeuvre uncertainty
123 #####
124
125 # Apply uncertainty to the delta-V scale
126 delta_v_thrust_scale = np.random.uniform(
127     low=1 + thrust_uncert_bounds[0], high=1 + thrust_uncert_bounds[1], size=(n)
128 )
129 delta_v_scale = np.random.normal(1, delta_v_sigma, size=(n))
130
131 # Calculate randomisation of delta-V direction; creating a new coordinate system to be able
132 # to apply random angles
133
134 # Need any vector that isn't collinear with the delta-v vector, and not ill-conditioned
135 # coord_const_vec = [1, 0, 0] if all(np.cross([1, 0, 0], delta_v)) == 0 else [0, 1, 0]
136 coord_const_vec = np.zeros((3))
137 coord_const_vec[np.argmax(np.abs(delta_v))] = 1
138
139 # Generate unit vectors of coordinate system
140 delta_v_arr = np.array(delta_v)
141 x_vec = np.expand_dims(
142     np.cross(coord_const_vec, delta_v_arr)
143     / np.linalg.norm(np.cross(coord_const_vec, delta_v_arr)),
144     -1,
145 )
146 y_vec = np.expand_dims(
147     np.cross(x_vec[:, 0], delta_v_arr)
148     / np.linalg.norm(np.cross(coord_const_vec, delta_v_arr)),
149     -1,
150 )
151 z_vec = np.expand_dims(delta_v_arr / np.linalg.norm(delta_v_arr), -1)
```

Example script uses **ATV example** from the handbook

- Position dispersion (uniform)
- Delta-v dispersion (Gaussian)
- Randomised angle deviations for thrust vector

Set of initial conditions can come from **mission analysis**

```
153 # Generate random angles to rotate the thrust by
154 angle_rots = np.deg2rad(np.random.normal(0, delta_v_angle_sigma, size=(n, 2)))
155 angle_vectors = (
156     x_vec @ np.expand_dims(np.sin(angle_rots[:, 0]) * np.cos(angle_rots[:, 1]), 0)
157     + y_vec @ np.expand_dims(np.sin(angle_rots[:, 0]) * np.sin(angle_rots[:, 1]), 0)
158     + z_vec @ np.expand_dims(np.cos(angle_rots[:, 0]), 0)
159 )
160
161 delta_v_randomised = (
162     angle_vectors * delta_v_scale * delta_v_thrust_scale * np.linalg.norm(delta_v)
163 ).T
```

1. Nominal Initial conditions: script input

Note: Script does not use the initial conditions present in the DRAMA project

```
75 PROJECT = "example_project.dpz"
76 NUM_RUNS = 100
77 NCPUS = 2
78
79 # Initial orbital state, at but before the final burn. Cartesian elements ECI 2000:
80 # [x, y, z, dx/dt, dy/dt, dz/dt], units in km and km/s
81 START_ORBIT_STATE = [
82     6472.6,
83     491.8,
84     -58.0,
85     -0.5766527384119823,
86     7.719100561002604,
87     1.3687058837186878,
88 ]
89
90 # Delta V to apply, same coordinate system:
91 # [dx/dt, dy/dt, dz/dt], km/s
92 DELTA_V = [0.00365274, -0.04910056, -0.00870588]
```

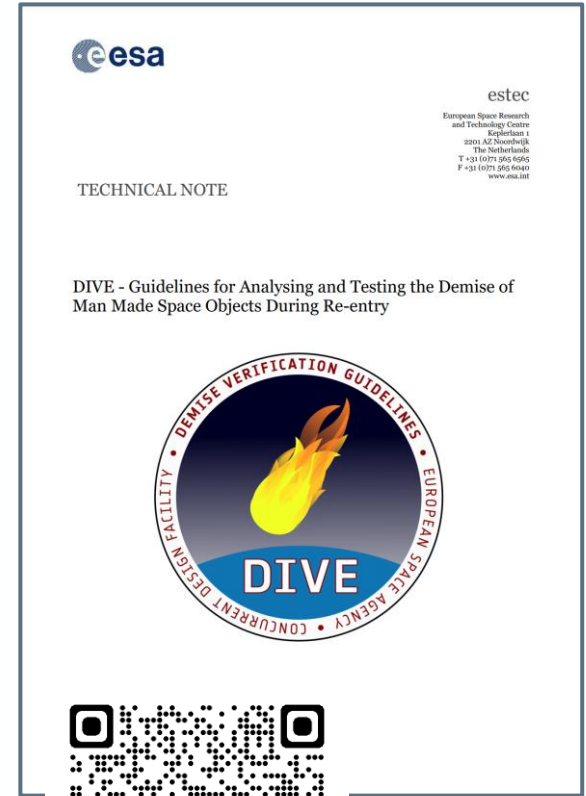
➤ Set Initial nominal state (before burn)

➤ Applied (nominal) delta-v of final burn

2. Model dispersions (DIVE – ESA-TECSYE-TN-018311)

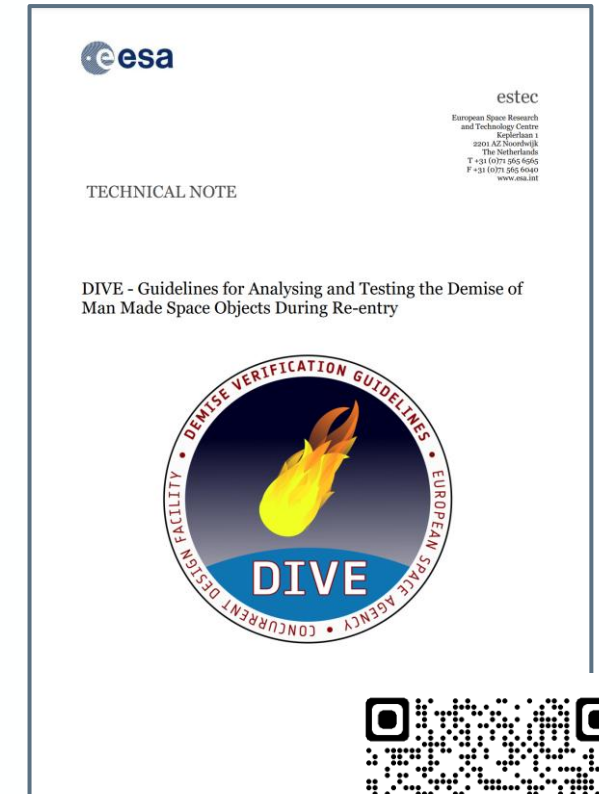
```
232 num_el = len(orig_model.el)
233 num_cn = len(orig_model.cn)
234 num_inc = len(orig_model.inc)
235
236 # Elements
237 #####
238
239 # Global aerodynamic scaling (drag and heat flux), due to density uncertainty
240 glob_drag_factor = np.random.normal(loc=1, scale=glob_drag_unc_sigma, size=(n))
241 glob_heat_factor = np.random.normal(loc=1, scale=glob_heat_unc, size=(n))
242
243 # Individual element drag offset
244 drag_factor = np.random.uniform(1 - drag_unc, 1 + drag_unc, size=(n, num_el))
245 heat_factor = np.random.uniform(1 - heat_unc, 1 + heat_unc, size=(n, num_el))
246
247 # Mass uncertainty
248 mass_factor = np.random.normal(loc=1, scale=mass_unc_sigma, size=(n, num_el))
249
250 # Connectors
251 #####
252
253 height_offset_cn = np.random.uniform(
254     -height_unc_cn, height_unc_cn, size=(n, num_cn)
255 )
256 temp_offset_cn = np.random.uniform(-temp_unc_cn, temp_unc_cn, size=(n, num_cn))
257 pres_factor_cn = np.random.uniform(
258     1 - pres_unc_cn, 1 + pres_unc_cn, size=(n, num_cn)
259 )
260
261 # Inclusions
262 #####
263 height_factor_inc = np.random.normal(
264     loc=1, scale=height_unc_inc_sigma, size=(n, num_inc)
265 )
```

- Object-wise global drag and mass uncertainty
- Connectors breakup altitude uncertainty (also pressure, temperature)
- Inclusions breakup altitude uncertainty



3. Material dispersions (DIVE – ESA-TECSYE-TN-018311)

```
349 # Generate the random numbers for the MC run
350 alloy_melt_offset = np.random.uniform(
351     -alloy_melt_unc, alloy_melt_unc, size=(n, num_materials)
352 )
353 oxidised_emissivity_factor = np.random.triangular(
354     left=1 - oxidised_emissivity_unc_factor,
355     mode=1,
356     right=1 + oxidised_emissivity_unc_factor,
357     size=(n, num_materials),
358 )
359 heat_cap_factor = np.random.normal(
360     loc=1, scale=heat_cap_sigma, size=(n, num_materials)
361 )
362 latent_melt_factor = np.random.normal(
363     loc=1, scale=latent_melt_sigma, size=(n, num_materials)
364 )
```



ESSB-HB-U-002: Appendix M.2

The Monte Carlo analysis should be executed until **convergence of the percentiles**, and not solely be based on a maximum number of samples.

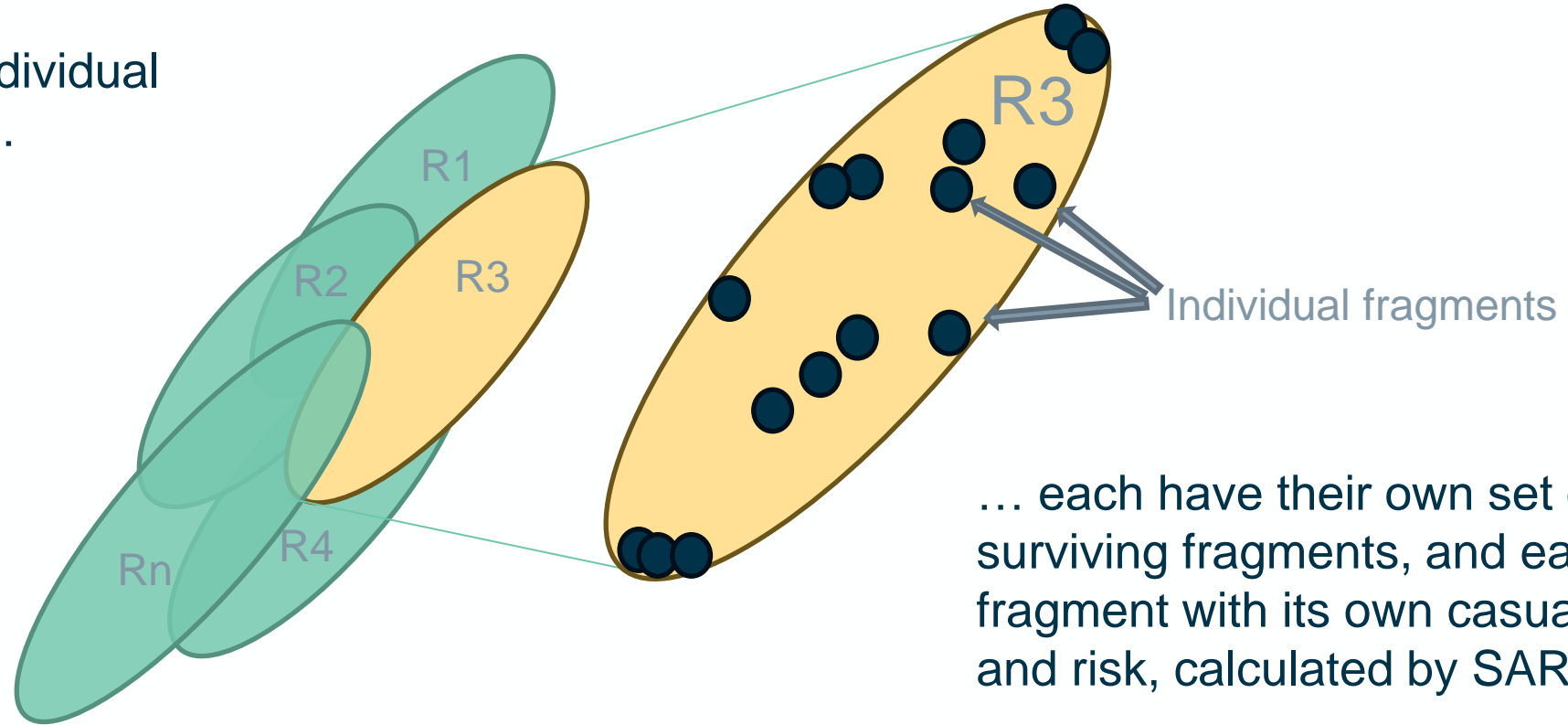
Example Criteria

- *The 95% confidence interval in the mean value of the total landed mass is within 2.5% of the current value.*
- *The 95% confidence interval in the mean value of the number of landed fragments is within 5% of the current value.*
- *The 95% confidence interval in the mean value of the landed mass of each individual component is within either 0.2kg or 10% of the current estimate for all components which land in 1% of simulations.*

The recommended minimum number of runs is **2000**.

Then run SARA... and analyse the results

We now have the individual results of each run...



... each have their own set of surviving fragments, and each fragment with its own casualty area and risk, calculated by SARA

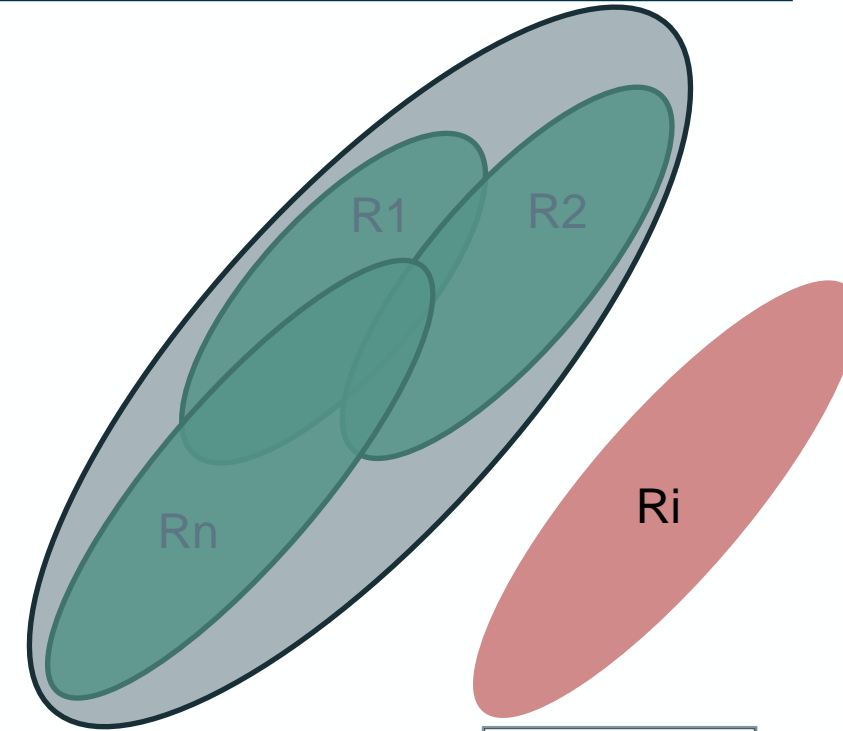
Calculating the total (averaged) risk from here is very straightforward

```
253 # Calculate the total 2D casualty risk for the whole simulation
254 tot_casualty_risk = 1 - np.prod(
255     1 - parsed_risk_result["totalCasualty2D"] / NUM_RUNS
256 )
```

D.2.13 Declared Re-entry Area (DRA) and Safety Re-entry Area (SRA)

The Declared Re-entry Area (DRA) and the Safety Re-entry Area (SRA) are computed following several simulation runs (Monte Carlo), which are based on the dispersions of the relevant variables to cover all uncertainties of the model (see section D.2.2), where the amount of runs yield stable confidence intervals (see Figure D-7):

- a. The Declared Re-entry Area (DRA) delimits the area where the debris are enclosed with a probability of 99% given the delivery accuracy.
- b. The Safety Re-entry Area (SRA) delimits the area where the debris are enclosed with a probability of 99,999% given the delivery accuracy.

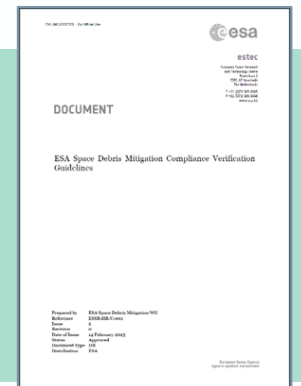
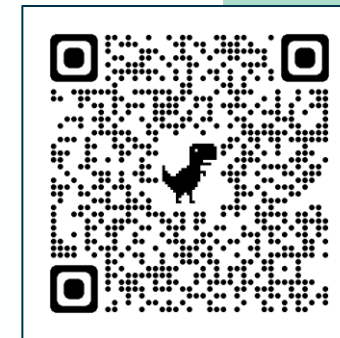


Optimisation Problem - many ways of calculating this

Important Note:

- 99/99.999% of **runs**
- **NOT** 99/99.999% of the **fragments**

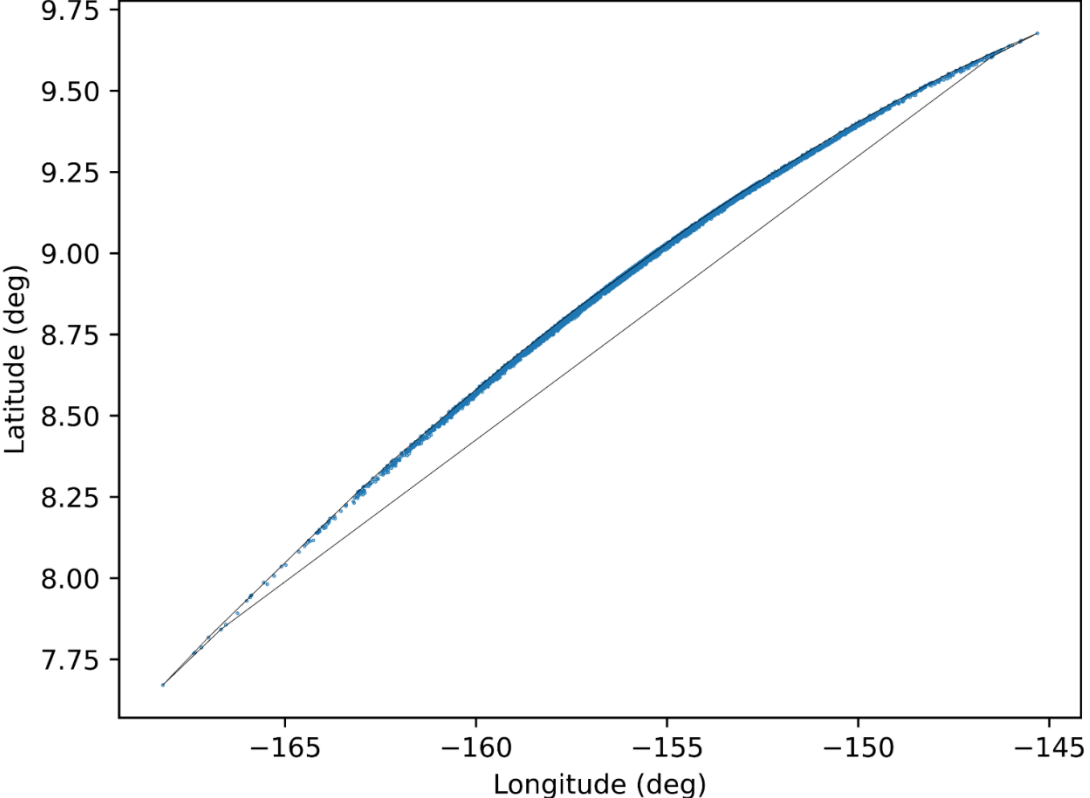
Not respecting this can lead to certain components being systematically excluded



Convex hull approach used

```
95 def calc_reentry_area(  
96     objects_df: pd.DataFrame, thresh_list: List[float] = [0.99]  
97 ) -> pd.DataFrame:  
98     """Example of what you can do once you have all the impacting fragments. This function  
99     calculates the reentry area (convex hull) that includes a certain percentage of the runs.  
100  
101     This will NOT give anything near the optimum result, and is just meant as an example; better  
102     algorithms should be implemented in practice.  
103  
104     :param objects_df: Dataframe containing the final properties of the impacting objects, as  
105     returned by parse_reentry_results_xml()  
106     :type objects_df: pd.DataFrame  
107     :param thresh_list: List of threshold percentages for which to calculate the reentry area,  
108     defaults to [0.99]  
109     :type thresh_list: List[float], optional  
110     :return: Dataframe containing the latitude and longitude of the vertices of the reentry areas  
111     for each threshold  
112     :rtype: pd.DataFrame  
113     """  
114     pts_df = objects_df[["longitude", "latitude", "run"]].copy(deep=True)  
115  
116     # Convert the location of fragments to cartesian coordinates in order to get rid of discontinuities  
117     x, y, z = EarthLocation.from_geodetic(  
118         lon=pts_df["longitude"], lat=pts_df["latitude"]  
119     ).to_geocentric()  
120     pts_df["x"], pts_df["y"], pts_df["z"] = (x.value, y.value, z.value)  
121  
122     run_ids = pd.unique(pts_df["run"])  
123     runs_df = pd.DataFrame(columns=["Run", "x", "y", "z", "pts_index"])  
124     for i, run in enumerate(run_ids):  
125         # Find the mean latitude and longitude of each run  
126         run_points = pts_df[pts_df["run"] == run]  
127         mean_point = EarthLocation.from_geocentric(  
128             run_points["x"].sum() * u.m,  
129             run_points["y"].sum() * u.m,  
130             run_points["z"].sum() * u.m,  
131         ).to_geodetic()  
132         mean_point = EarthLocation.from_geodetic(lon=mean_point.lon, lat=mean_point.lat)
```

Example Monte-Carlo Results and SRA (n = 100)



- 📁 Topics
- 👤 My Posts
- ⋮ More
- ▾ Categories ✎
- 🟣 In-situ detection
- 🟡 Site Feedback
- 🟢 Uncategorized
- ☰ All categories
- ▾ Tags ✎
- 👉 dmf
- 👉 master
- 👉 drama
- 👉 in-situ
- ☰ All tags

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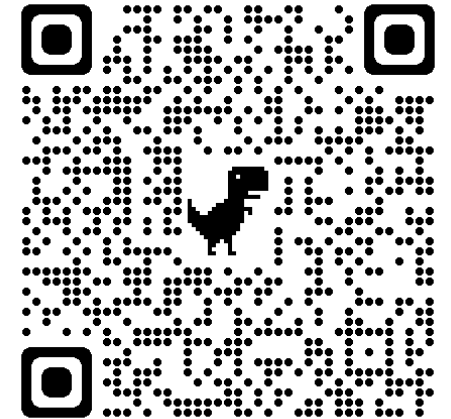
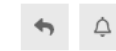
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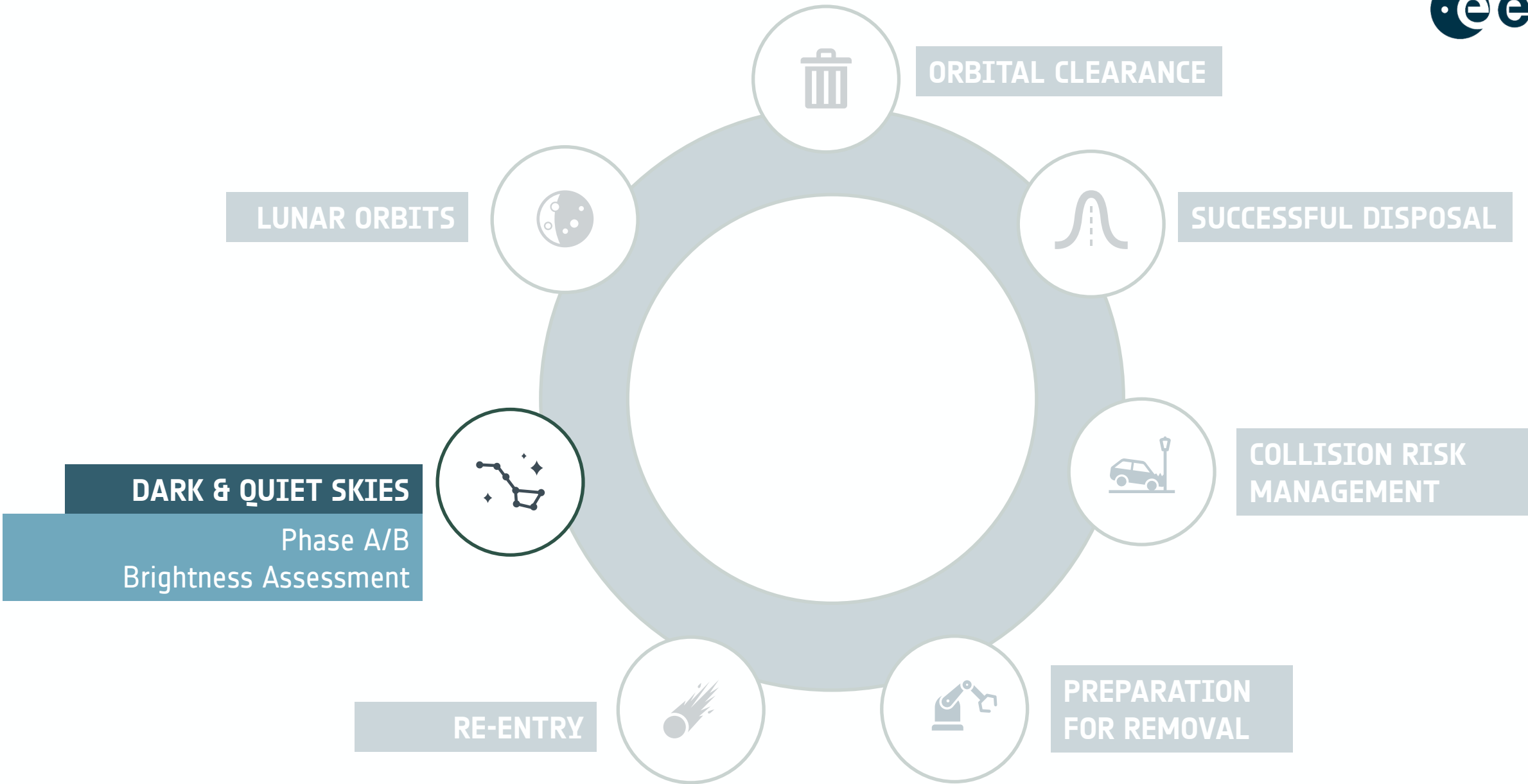
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Phase A/B Requirements– Visual Brightness

ESSB-ST-U-007 Issue 1 5.6.a

The developer of a spacecraft or launch vehicle orbital element in near Earth orbit shall quantify the **visual** brightness of the design.



Early phases (0-B)

Assess brightness assuming a combination of diffuse and/or specular reflection for **primitive shapes** (e.g. **sphere**, cylinder, flat plate).

Diffusive and specular reflection for surfaces is described using physical or empirical models, e.g. ideal **Lambertian**, or empirical Phong reflection models

ESA Space Debris Mitigation Compliance Verification Guidelines

The apparent magnitude of a satellite can be computed from the irradiance ratio of the satellite with respect to the solar illumination irradiance E_{sun} and the apparent magnitude of the Sun m_{Sun} at Earth distance.

$$m_{sat} = m_{sun} - 2.5 \log \left(\frac{E_{sat}}{E_{sun}} \right) + x\chi$$

Satellite Brightness

Atmospheric Extinction

Need to determine:

1. Geometric set-up
2. Reflectance model
3. Atmospheric extinction

1. Geometric Set-Up

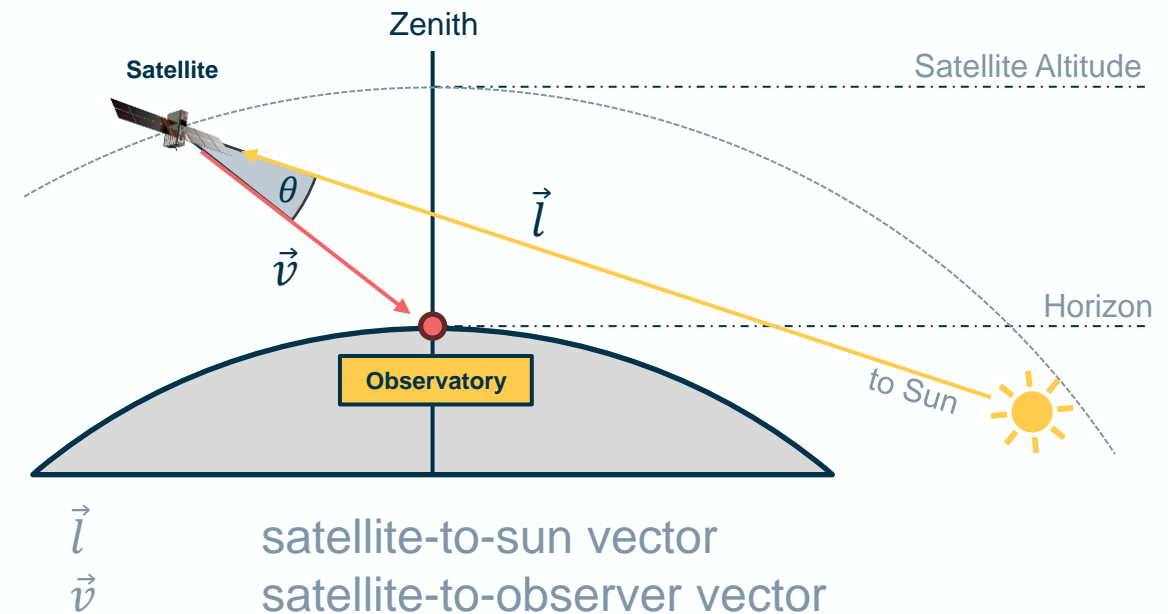
The geometric set-up of the **satellite**, the **Sun**, and an **observer** is required. These are used to construct:

- The sun-to-satellite vector \vec{l}
- The satellite-to-observer vector \vec{v}

The angle between these vectors is the phase angle θ (see following slides).

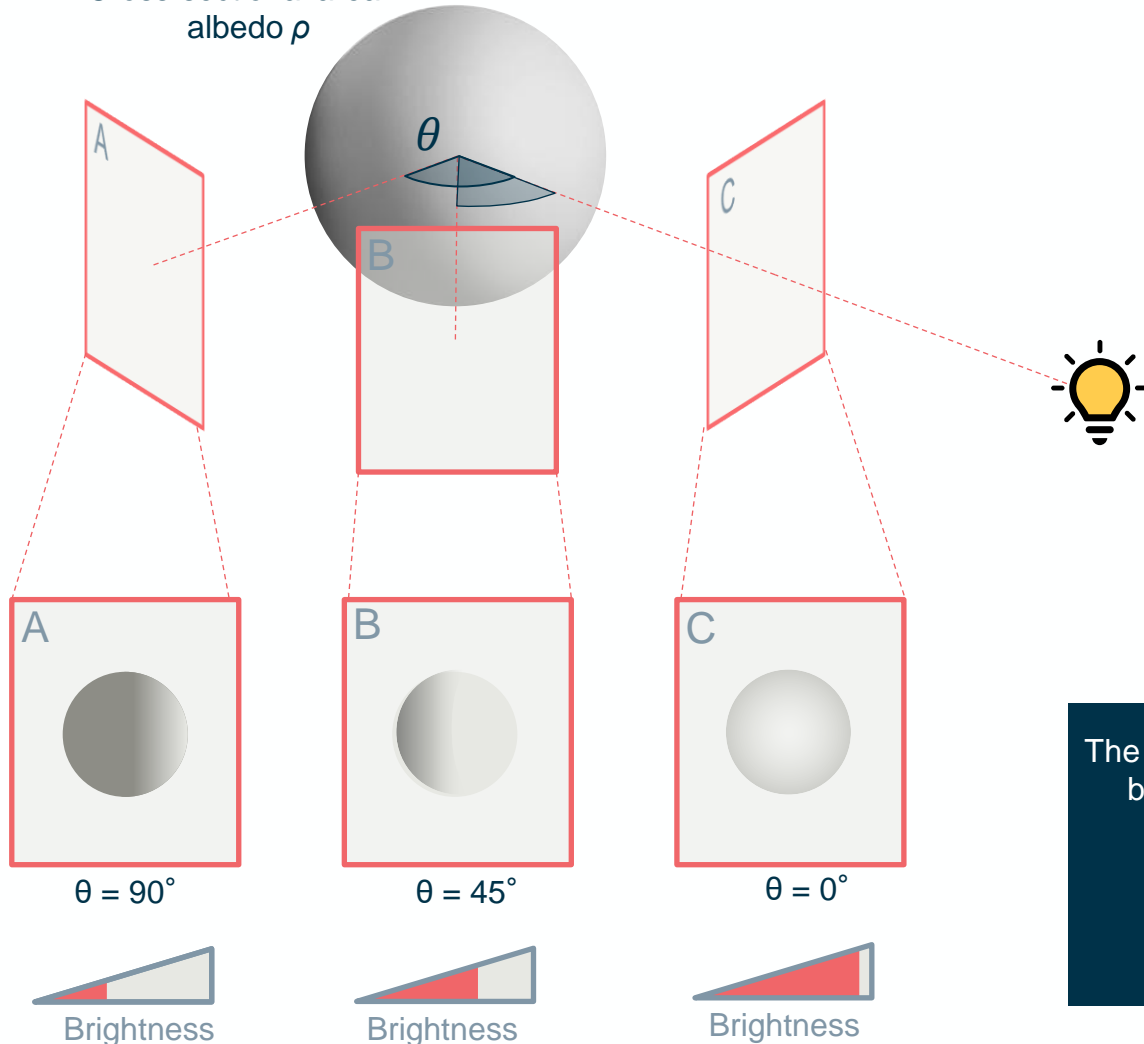
The vector to zenith from the observer is also required to calculate airmass (see following slides).

The brightness will be at a maximum when θ is closest to 0° and $|\vec{v}|$ is minimised, subject to the constraint that the satellite is not in eclipse.



2. Simple Reflectance Model – Lambertian Sphere

Cross-sectional area A
albedo ρ



Lambertian reflectance is the property that defines an ideal diffusely reflecting surface. The apparent brightness of a Lambertian surface to an observer is the same regardless of the observer's angle of view. For an illuminated **Lambertian sphere**, the **observed brightness only varies with phase angle θ** .

$$E_{sat} = E_{sun} \frac{f_r(\vec{l}, \vec{v})}{d^2}$$

$$f_r(\vec{l}, \vec{v}) = \rho A \frac{1}{\pi} (\sin \theta + (\pi - \theta) \cos \theta)$$

The phase angle θ is the angle between illumination and observation vectors

$$\theta = \cos^{-1} \frac{\vec{l} \cdot \vec{v}}{\|\vec{l}\| \|\vec{v}\|}$$

$0^\circ \leq \theta \leq 180^\circ$

- E_{sat} satellite emission
- E_{sun} Solar illumination irradiance
- d distance from observer-satellite
- ρ geometric albedo
- θ phase angle
- A cross-sectional area
- \vec{l} satellite-to-sun vector
- \vec{v} satellite-to-observer vector

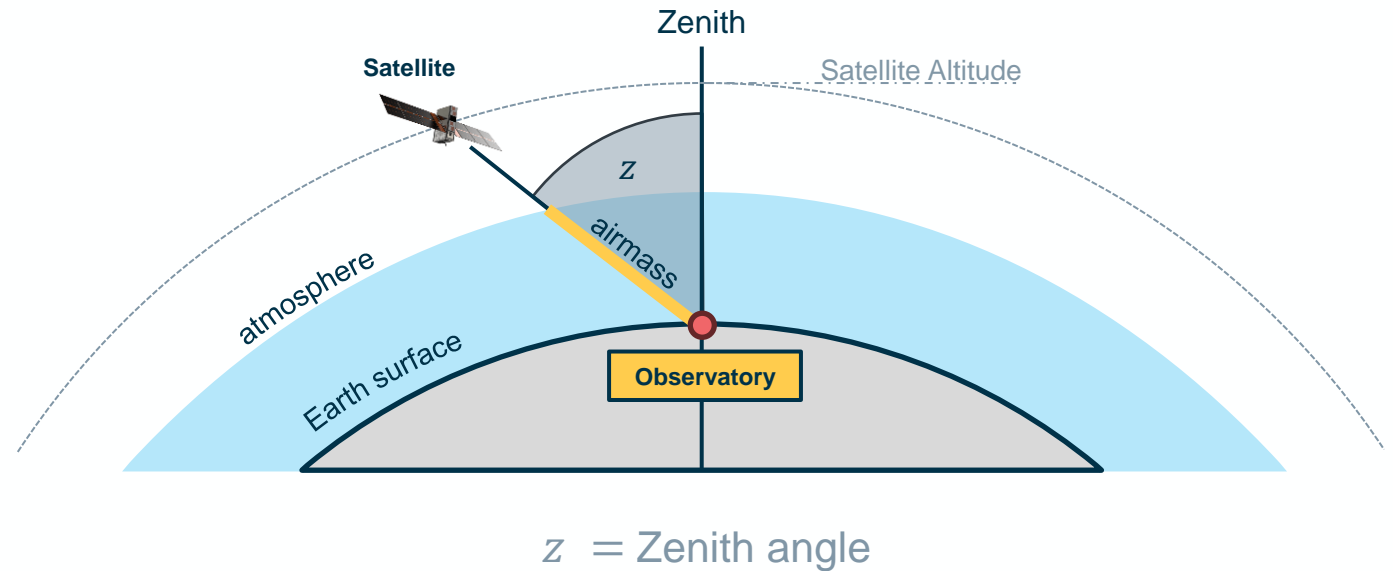
3. Modelling Extinction

Some light is absorbed and scattered by the atmosphere, reducing the brightness of a satellite when viewed from ground. This is referred to as extinction.

$$\text{Extinction} = x\chi = \frac{0.12}{\cos z}$$

$\chi = 1/\cos z$ is the airmass, which is the quantity of atmosphere crossed by the observed light, normalized to zenith.

$x \approx 0.12$ mag/airmass is a typical value at visible wavelengths¹



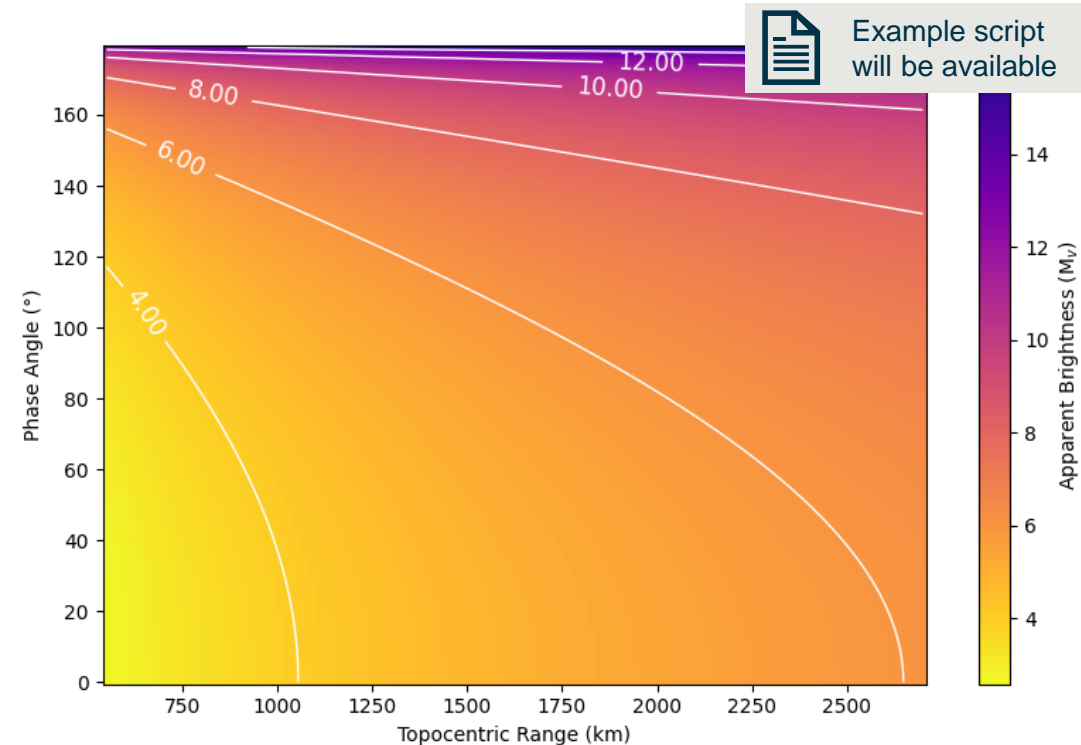
¹ Patat, F., et al. "Optical atmospheric extinction over Cerro Paranal." Astronomy & Astrophysics 527 (2011): A91.

Assessment Steps

With a simple Lambertian sphere as a reflectance model and a defined geometrical set-up the brightness can be calculated by hand using the equations given or implemented in a script.

Modelling Process:

1. Estimate satellite cross-sectional area
 - Can use e.g. DRAMA CROC
2. Estimate/assume geometric albedo
3. Calculate geometries
 - Satellite position
 - Observatory position
 - Sun position
4. Calculate phase angle θ
5. Calculate satellite brightness
6. Calculate extinction
7. Calculate final magnitude
8. Document results



Results for a satellite with cross-sectional area 7m^2 and **assumed** geometric albedo of 0.25. Satellite in circular orbit at an altitude of 550km, with corresponding minimum and maximum topocentric ranges.

Next steps

NOW



Question time



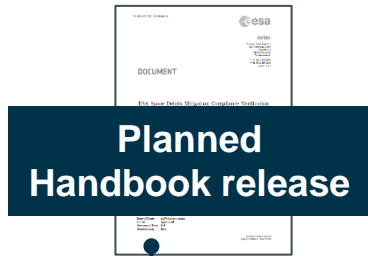
Questions that could not be answered now will be followed up



Dedicated clarification sessions can be requested



Clean Space Days



Planned Handbook release



DRAMA and MASTER population release

October 2024

November 2024

December 2024

January 2025

February 2025

March 2025

April 2025



Policy



Requirements



Handbook



Tools



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